

[RESTRICTED]



Hong Kong Housing Authority

**AGREEMENT NO. CB20210448 -
Term Engineering Consultancy Services for
New Territories East Region (2021-2023)**

Proposed Public Housing Development Site at Po Shek Wu Road

**Sewerage Impact Assessment (SIA)
Report (Issue 6.0)**

SEWERAGE IMPACT ASSESSMENT

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LIST OF ABBREVIATIONS

<u>Abbreviation</u>	<u>Full title</u>
ADWF	Average Dry Weather Flow
DSD	Drainage Services Department
DCC	Day Care Centre
EPD	Environmental Protection Department
GESF	Guidelines for Estimating Sewage Flows for Sewage Infrastructure Planning
HD	Housing Department
HKHA	Hong Kong Housing Authority
HKPSG	Hong Kong Planning Standard and Guidelines
HCS	Home Care Services
OZP	Outline Zoning Plan
SIA	Sewerage Impact Assessment
UFF	Unit Flow Factor
WSP	WSP (Asia) Limited

1. INTRODUCTION

1.1 General

1.1.1 WSP (Asia) Ltd (WSP) had been commissioned by HKHA, under Term Engineering Consultancy Services for New Area (2021-2023), to carry out the civil engineering consultancy services in respect of SIA for the proposed public housing site at Po Shek Wu Road (hereafter referred to as “the Site” or “the Proposed Development”).

1.2 Background

1.2.1 The Site is located at the northwest of Sheung Shui Town Centre. It is bounded by San Wan Road and Po Shek Wu Road, opposite to Shek Wu Hui Jockey Club Playground. It is zoned for “Other Use” (“OU”) and as temporary bus depot under Short Term Tenancy (STT). The Site is for Subsidised Sale Flats (SSF) Development. It comprises of about 1904 Flats and is envisaged to be complete by Year 2029/30. The site is zoned “Residential (Group A)5. The Site location plan is in **Appendix A**.

1.2.2 Existing sewerage provision is available along San Wan Road. There are two trunk sewers with size DN1800 that were laid along San Wan Road conveying sewage to Shek Wu Hui Sewage Treatment Works (SWHSTW). The sewerage layout plans of the existing sewerage system are in **Appendix A**.

1.2.3 The sewage from the Site will be discharged to the existing sewerage system in San Wan Road. Based on the original development parameters provided by HKHA, JACOBS has prepared and submitted the SIA (Report Ref. R/3509/016 Revision 0), which was approved by EPD and DSD.

1.2.4 Subsequent to the approval of original SIA, HKHA advised that there would be some changes of key development parameters for Po Shek Wu Road. An updated SIA would therefore be required.

1.3 Objective

1.3.1 The purpose of this SIA is to update the key development parameters and assess the impact to the existing sewers for the additional flow generated. In general, the design principle and assumption will follow the approved SIA. Mitigation measures to the existing sewerage system including modification or upgrading works will be recommended if necessary.

The scope of the assessment includes:

- Estimate the sewage generated from the proposed development;
- Assess the capacity of the existing sewerage systems downstream to the Site;
- Analyse the impact to the existing sewerage systems downstream to the Site subjected to the discharge due to the proposed development; and
- Propose mitigation measures (i.e. Modification or upgrading works), if any.

1.4 Structure of this Report

1.4.1 This SIA report contains the following sections in addition to this introduction:

Section 2 Introduces the general information of the Site.

Section 3 Discusses the methodology and design parameters for the SIA.

Section 4 Presents the sewage flow of existing development and capacity checking of the existing sewage system.

Section 5 Presents the proposed sewerage discharge points and capacity checking of the sewage system.

Section 6 Proposes mitigation measures of the Site.

Section 7 Summarizes the results, conclusions and recommendation of the SIA.

2. PROJECT INFORMATION

2.1 Existing Project Information

2.1.1 According to the information provided by HKHA, the Site consists of the followings:

HA-funded Items:

- a) two blocks (Block A and Block B) with 40 and 41 domestic storeys respectively and with an intermediate refuge floor, providing a total of 1 904 flats;
- b) a four-storey podium with shops of approximately 1 800m² internal floor area (IFA), ancillary carpark for private cars and motorcycles, loading/unloading (L/UL) bays, building services plant rooms and a landscaped garden at its roof;
- c) a six-classroom kindergarten;
- d) a post office;
- e) a district management office and a management office for this PHD;
- f) associated ancillary facilities and external works, including open parking spaces for bicycles;
- g) a footbridge No. 1 (FB1) connecting the development and Sheung Shui Areas 4 & 30 Site 2 (SSS2); and
- h) a footbridge No. 2 (FB2) connecting the development and Po Shek Wu Estate (PSWE) across the East Rail.

Government-funded Items (welfare facilities):

- a) a 100-place Child Care Centre (CCC);
- b) a 100-place Residential Care Home for the Elderly (RCHE);
- c) a main base of Short-term Food Assistance Service Team (STFAST);
- d) one team of Home Care Services (HCS) for Frail Elderly Persons; and
- e) public footbridge – a footbridge No. 3 (FB3) with lift tower and staircase along San Wan Road connecting to the existing footbridge network leading to Sheung Shui MTR Station to be handed over to the Transport Department (TD) and the Highways Department (HyD) for management and maintenance, with agreement with TD and HyD obtained.

3. METHODOLOGY AND DESIGN PARAMETERS FOR SEWERAGE IMPACT ASSESSMENT

3.1 Methodology

Assessment Approach

3.1.1 The following approach and methodology have been adopted in this sewerage impact assessment:-

- Carry out the desktop study to collect the relevant information for the assessment;
- Investigate and review the existing and planned sewerage networks and determine the sewage flow generated from the existing development; and
- Determine the potential sewage arising from the proposed development.

3.1.2 For the existing sewers and proposed sewers design, Colebrook-White equation has been used to assess the hydraulic performance.

Collection Information

3.1.3 Desktop study has been undertaken to collect the relevant information for the assessment. The relevant information collected is summarised below:

- Planned Sewerage Layout in the vicinity of the proposed Development; and
- Sewage flow generation from the existing buildings.

Design Standards, Guidelines and Reference

3.1.4 The sewage flow generated from the proposed development is based on the following standards, guidelines and reference for the sewerage and sewage treatment design:-

- Sewerage Manual Part 1 – Key Planning Issues and Gravity Collection System, Third Edition, May 2013 published by DSD;
- Sewerage Manual Part 2 – Pumping Stations and Rising Mains, Second Edition, May 2013 published by DSD;
- Guidelines for Estimating Sewage Flows for Sewage Infrastructure Planning (GESF) published by EPD; and
- Commercial and Industrial Floor Space Utilization Survey published by PlanD.

Hydraulic Analysis

3.1.5 The hydraulic conditions of the proposed **sewage system** are designed with spreadsheet calculations. The full-bore flow shall be taken as the design capacity of a sewer. The capacity for gravity sewers is assessed using the Colebrook–White equation.

$$V = -\sqrt{(8gDs)} \log \left(\frac{k_s}{3.7D} + \frac{2.51v}{D\sqrt{(2gDs)}} \right)$$

3.2 Basic Design Parameters

Unit Flow Factors

- 3.2.1 The Unit Flow Factors (UFF) for Domestic Flow and Commercial and Institutional Flow have been adopted in accordance with Table T-1, Table T-2 and Table T-3 of the GESF. The category of the components and the Unit Flow Factors adopted in the assessment are indicated in **Table 3.2.1** below.

Table 3.2.1 – Unit Flow Factors for Domestic and Commercial Flow

Component	Category/ Use	UFF (m ³ /person/day)
Domestic Flow	Public Rental / Private housing (R1)	0.19
	Private housing (R2)	0.27
	Private housing (R3)	0.37
	Modern village	0.27
	Temporary and non-domestic	0.15
Commercial Flow ^(Note)	J1 Manufacturing (North District)	0.63
	J3 Transport, Storage & Communication	0.18
	J4 Wholesale & Retail	0.28
	J6 Finance, Insurance, Real Estate & Business Services	0.08
	J10 Restaurants & Hotels	1.58
	J11 Community, Social & Personal Services	0.28

Note: The unit flow factor of commercial employee 0.08 m³/h/d is added into the Commercial Flow Factor.

- 3.2.2 According to the information from HKHA, the Site is seeking the relaxation of the maximum total PR from 7.0 to 7.5 which exceeds the maximum plot ratio residential density zone R2 for New Territories (5). Thus, the Site is assumed to be equivalent to R1 housing and the unit flow factor of the resident adopted in the Site is 0.270m³/person/day. For commercial flow of the Site, several categories will be applied for the estimation. Please refer to **Appendix D** for more details.
- 3.2.3 An extra 10% population will be applied to the total sewage generation of the Site.
- 3.2.4 The Catchment Inflow Factors (P_{cif}) cater for the net overall ingress of water or wastewater to the sewage system. They are catchment-dependent and applicable to major sewerage facilities of a catchment. They are not applicable to new catchments which are deemed to be free from misconnections and pipe defects. Therefore, the P_{cif} are not applicable in estimating the total flows from the new development areas.
- 3.2.5 For the existing sewage system in North District, P_{cif} of 1.0 will be adopted in accordance with Table T-4 of the GESF.

Table 3.2.5 - Catchment Inflow Factors, P_{cif}

Catchment	Catchment Inflow Factor, P_{cif}
Central, North Point, Sandy Bay, Wan Chai, Wah Fu, Stanley, Cental Kowloon, Yuen Long, San Wai, North District, Tai Po, North Lantau, Mui Wo	1.00
Chai Wan, Tuen Mun, Kwai Chung, Tsing Yi, East Kowloon	1.10
Sha Tin	1.15
Tseung Kwan O	1.20
Shau Kei Wan	1.25
Aberdeen, Ap Lei Chau, Sai Kung, North West Kowloon	1.30
Cheung Chau, Shek O	1.50

3.2.6 The average sewage flow, $Q_{average}$, is as follows:

$$Q_{average} = (Q_{domestic} + Q_{commercial} + Q_{other}) \times P_{cif}$$

Peaking Factors

3.2.7 Peaking factors cater for seasonal / diurnal fluctuation and normal amount of infiltration and inflow. The peaking factors shall be in accordance with Table T-5 of GESF and are shown in the **Table 3.2.7**.

Table 3.2.7 – Peaking Factors for Various Population Ranges

Population Range	Peaking Factor (including Stormwater allowance) for facility with existing upstream sewerage	Peaking Factor (excluding Stormwater allowance) for facility with new upstream sewerage
(a) For sewers		
<1,000	8	6
1,000 – 5,000	6	5
5,000 – 10,000	5	4
10,000 – 50,000	4	3
>50,000	Max (7.3/ $N^{0.15}$, 2.4)	Max (6/ $N^{0.175}$, 1.6)
(b) Sewage Treatment Works, Preliminary Treatment Works and Pumping Stations		
<10,000	4	3
10,000 – 25,000	3.5	2.5
25,000 – 50,000	3	2
>50,000	Max (3.9/ $N^{0.065}$, 2.4)	Max (2.6/ $N^{0.065}$, 1.6)

Notes: N is the contributing population in thousands.

3.2.8 Peaking factors (including stormwater allowance) used in this report are usually applied to design sewerage facilities receiving flow from new upstream **sewage systems** which rarely has misconnections and defects for infiltration.

3.2.9 The peak sewage flow, Q_{peak} , is calculated as follows:

$$Q_{peak} = Q_{average} \times P$$

Where $Q_{average}$ is the average sewage flow and,

P is the peaking factor

Material

3.2.10 The roughness coefficient for newly concrete sewers used for Colebrook-White (k_s) is based on values provided in the Table 5 of DSD Sewerage Manual Part 1 2013. The roughness coefficient for existing concrete sewer used for Colebrook-White (k_s) is based on values calculated by the trial-and-error basis. Details refer to **Appendix C. Table 3.2.10** summarized the roughness coefficients for the sewerage design.

Table 3.2.10 – Roughness Coefficients for Sewerage Design

Material	Roughness Coefficients, k_s
Concrete (DSD Sewerage Manual)	3.0 mm
Concrete (Trial-and-error Basis)	3.1mm

3.3 Design Assumptions for Existing System Capacity Estimation

3.3.1 An extra 10% population will be applied to the total sewage generation of the Site.

3.3.2 All of the non-domestic facilities will be assumed to be operated by the time when the construction is completed.

3.3.3 Teachers in the kindergarten will be assumed to be community service (J11) employees. Each classroom will hold 1 class with 30 students on average.

3.3.4 The car park staff will be classified to be transport, storage (J3) employees. The worker density of transport will be adopted for the car park.

3.3.5 Since manhole FMH1004664 locates at the most upstream of a pipe section and the original depot will be demolished, the base flow of pipe section between manhole FMH1004664 and manhole FMH1004662 will be assumed to be 0 before the completion of the Site.

3.3.6 Peak wet weather baseline flows of concerned sewer sections were provided by EPD and no adjustment factors on the data are required.

3.3.7 All existing peak flows provided by DSD has been multiplied by catchment inflow factor P_{CIF} and peak factor P . No further factor is required to be imposed on the data provided.

3.3.8 Sewers at downstream of the scope are considered to have sufficient spare capacity for the new development.

3.3.9 Kinematic viscosity of sewage is assumed to be equal to the kinematic viscosity of water. (i.e. $1 \cdot 10^{-6} \text{ m}^2/\text{s}$).

3.4 Other Design Considerations

3.4.1 The existing drainage plans (Plan nos.: 3-SW-6A-2, 3-SW-6A-4, 3-SW-6B-1, 3-SW-6B-3, 3-SW-1C-4 and 3-SW-1C-4) were obtained from the Drainage Services Department (DSD) in September 2016 to gather the background information on existing sewerage system in the vicinity of the Sites. The sewerage layout of the above plans have been redrawn and illustrated in Appendix A.

3.4.2 All capacity and projected peak flows under ultimate scenarios illustrated in Appendix E were obtained from EPD in November 2016 to gather the existing condition of the sewerage system in the vicinity of the Site.

3.4.3 Based on the DSD drainage plans, there is an existing manhole (FMH1004664) connected to a DN225 sewer located inside the Site boundary. This section can be modified into a terminal manhole connect to the existing sewerage system from the Site. The sewage flow generated from the Site will be conveyed to the SWHSTW by a DN1800 existing sewage main trunk along San Wan Road.

3.4.4 There is planned expansion works at the Shek Wu Hui Sewage Treatment Works (SWHSTW) to increase its capacity for meeting the projected district demand. HD had agreed with EPD that sewage arising from the proposed housing development at Sheung Shui Area 30 and Po Shek Wu Road sites could be accommodated by the SWHSTW.

3.4.5 There are several planning developments from the upstream sewerage and will discharge to the sewerage treatment works via the existing 1800dia main trunk. The sewerage flow from the planning developments have been provided by EPD (refer to the **Appendix G**) and the amount will be included into the assessment.

4. CAPACITY AND ADEQUACY ASSESSMENT

4.1 Introduction

4.1.1 In this assessment, the following flow scenario will be presented: -

- 1) Condition of the existing sewerage system after the construction of the proposed development with all sewage generated from the proposed development is discharged to FMH1004664 by using the existing sewer FWD1005561

4.2 Sewage Discharge Estimation

4.2.1 Population

This SIA divides all population into three cohorts: domestic, transport, storage (J3), commercial (J11) employees and students. The average household size and total domestic population of the two blocks are given by HKHA, whereas the population of the commercial employees is estimated according to the usage ratio in “Commercial and Industrial Floor Space Utilization Survey” conducted by Planning Department.

4.2.2 Flow Generation

Sewage generation in this SIA is estimated by unit flow generation stated in GESF. Each population cohort has a unique unit flow factor listed Table T-1 and Table T-2 in GESF. After retrieving the unit flow of each cohort, total discharge flow generation can be calculated by multiplying the unit flow to the corresponding population.

4.2.3 Peak Factor

From GESF, peaking factor P is determined by contributing population. In this report, peak factor of the flow generated from the Site follows Table T-5 (including stormwater allowance) of GESF, which P=5 are adopted for the SIA.

4.2.4 Estimated Sewerage Discharge Flow

Table 4.2.4 summarized the sewerage discharge flow from the Site after the completion. The details breakdown could refer to **Appendix D**.

Table 4.2.4 – Estimated Sewerage Discharge Flow from the Site

Categories	Item	UFF (m ³ /day)
Domestic Flow	Public Residential Building Block:	1583.8
Commercial and Institutional Flow	Retail	23.5
	Kindergarten	17.0
	Post office	5.0
	A district management office and A management office for the Site	7.0
	Associated ancillary facilities and external works, including open parking spaces for bicycles;	52.6
	A 100-place Child Care Centre (CCC);	28.3
	A 100-place Residential Care Home for the Elderly (RCHE);	34.1
	A main base of Short-term Food Assistance Service Team (STFAST);	1.4
Home Care Services (HCS) for Frail Elderly Persons	25.2	
Total		1778.0

4.3 Capacity Checking for the Existing Sewerage System

4.3.1 Capacity Calculation

The baseline sewage flow and full-bore capacity of the existing gravity sewers in the vicinity of the proposed development were given by EPD in **Appendix B** and used as baseline information in the assessment. The baseline sewage flow was estimated using computer hydraulic modelling taking into account the sewage flow from the existing and planned developments in the catchment. However, for proposed sewers and sewers with missing data, capacity should be clarified. The capacity of the existing drainage pipes were estimated by Colebrook-White equation stated in the Section 3.1.5.

For the hydraulic pipeline roughness k_s , from **Section 5.2.1** of Sewerage Manual, published by DSD, the roughness of slimed sewers shall be adopted from Table 5 in the manual. Assume all sewers are concrete sewers, the k_s value of the sewer will then be estimated by trial and error basis based on the manhole data provided by EPD, and the value with minimal error along the main trunk (i.e. 0.0031m) will be adopted in this report. The detail estimation is shown in **Appendix C** in this report.

4.3.2 Utilization Rate

In the context of computer hydraulic modelling, the utilization rate of gravity sewer is defined as the running water depth divided by the sewer diameter. A sewer section is under surcharge if its utilization rate is greater than 1. In this assignment, the estimated sewage flow from the proposed development calculated in **Appendix D** is added to the baseline sewage flow provided by EPD shown in **Appendix B** to project the ultimate flow of concerned sewer sections illustrated in **Appendix E**. The projected flow is then compared against the full-bore capacity. The sewer is expected to have sufficient capacity if its projected flow is lower than the full-bore capacity. **Table 4.3.2a** summarized existing condition of the existing sewerage networks. **Table 4.3.2b** summarized the result of the assessment under Scenario 1. Detail of the result refer to the **Appendix E**.

Table 4.3.2a – Existing Utilization Rate of Existing Sewerage System before the Development (Including other Planning Developments)

Sewers Between Manholes		Utilization
US MH	DS MH	(%)
FMH1004664	FMH1004663	31.1
FMH1004663	FMH1004662	25.8
FMH1004662	FMH1004661	47.1
FMH1004661	FMH1004660	48.8
FMH1004660	FMH1004659	N/A
FMH1004659	FMH1004658	N/A
FMH1004658	FMH1004657	61.9
FMH1004657	FMH1004629	39.3
FMH1004629	FMH1004030	47.9
FMH1004030	FMH1004031	68.6

Table 4.3.2b – Utilization Rate of Existing Sewerage System after the Development

Sewers Between Manholes		Utilization
US MH	DS MH	(%)
FMH1004664	FMH1004663	180.8
FMH1004663	FMH1004662	151.3
FMH1004662	FMH1004661	59.9
FMH1004661	FMH1004660	62.0
FMH1004660	FMH1004659	N/A
FMH1004659	FMH1004658	N/A
FMH1004658	FMH1004657	78.6
FMH1004657	FMH1004629	50.0
FMH1004629	FMH1004030	59.3
FMH1004030	FMH1004031	84.9

5. SEWERAGE IMPACT ASSESSMENT

- 5.1.1 Under Scenario 1 in Section 4.1.1, the estimated peak flow in the sewer sections between manholes FMH1004664 and FMH1004662 exceed 100% of full-bore capacity. There is significant sewerage impact of the existing sewerage system. Mitigation measures for the existing sewerage system are needed.
- 5.1.2 Apart from the sewer FWD1005561 between the manhole FMH1004664 and FMH1004662, the downstream sewerage systems are capable to cater the increased sewerage flow from the Site after the completion.
- 5.1.3 The full-bore capacity of the DN1800 sewer section between manholes FMH1004651 and FMH1004650 is lower than other DN1800 sewer sections in the vicinity due to gentle gradient.
- 5.1.4 Sewer sections from manhole FMH1004660 to FMH1004658 are at level according to the Drainage Record. Hence, the full-bore capacity could not be determined by the Colebrook-White equation. Computer hydraulic modelling indicated that the baseline utilization rate of the sewer sections ranges from 62 to 63% under previous submission. Although the sewerage flow from the Site have been increase by about 1.5L/s, the impact of the increased flow should be minor. The existing sewers from manhole FMH1004660 to FMH1004658 is capable to cater the increased sewerage flow.
- 5.1.5 The checking on the existing pipes up to FMH1004031 shows that the DN1800 main trunk provides sufficient capacity to cater for the sewage generated from the housing development and the base flow. Hence, no further checking on the downstream is required.

6. MITIGATION MEASURES

6.1 Sewerage Impact After the Completion of the Site

6.1.1 As mentioned in **Section 5.1.1**, the utilization of the sewer sections between manholes FMH1004664 and FMH1004662 would exceed 100% of the full-bore capacity. Mitigation measures should be proposed to cater the insufficient capacity of the existing sewerage system between the site and the DSD main sewerage networks.

6.2 Upgrading Works for Sewer from FMH1004664 to FMH1004662

6.2.1 To raise the capacity of the section, a pipe with larger nominal diameter shall replace the original DN225 sewers. The existing sewer FWD1005561 shall be upgraded to accommodate sewage arising from the Site.

6.2.2 This section will justify the adequacy of capacity of installing DN300 concrete sewers to replace the original sewers.

6.2.3 **Appendix E** and **Table 6.1.4a** showed the detail calculation of the section, while **Appendix F** and **Table 6.1.4b** illustrate the capacity change of the sewer section before and after adopting the DN300 pipes.

Table 6.1.4a – Initial Condition of Sewer Sections FMH1004664 to FMH1004662

Sewer	Pipe Diameter	US IL	DS IL	Increased Sewage Flow	Cumulative Peak Flow	Pipe Capacity	Utilization
	(mm)	(mPD)	(mPD)	(L/sec)	(L/sec)	(L/sec)	(%)
FWD1005561	225.0	6.42	6.03	20.58	102.89	56.92	180.8
FWD1005560	225.0	6.03	5.47	20.58	102.89	68.01	151.3

Table 6.1.4b – Results of the Sewer Sections Adopting DN300 Pipes

Sewer	Pipe Diameter	US IL	DS IL	Increased Sewage Flow	Cumulative Peak Flow	Pipe Capacity	Utilization
	(mm)	(mPD)	(mPD)	(L/sec)	(L/sec)	(L/sec)	(%)
FWD1005561	300.0	6.42	6.03	20.58	102.89	123.59	83.3
FWD1005560	300.0	6.03	5.47	20.58	102.89	147.66	69.7

6.2.4 **Table 6.1.4a** and **Table 6.1.4b** show clearly that the capacity has risen more than double when the original sewers by DN300 concrete pipes. Thus, to summarize, the inadequacy occurs in the sewer sections between manholes FMH1004664 to FMH1004662 can be resolved with replacing the original sewers by DN300 concrete pipes.

7. CONCLUSIONS AND RECOMMENDATIONS

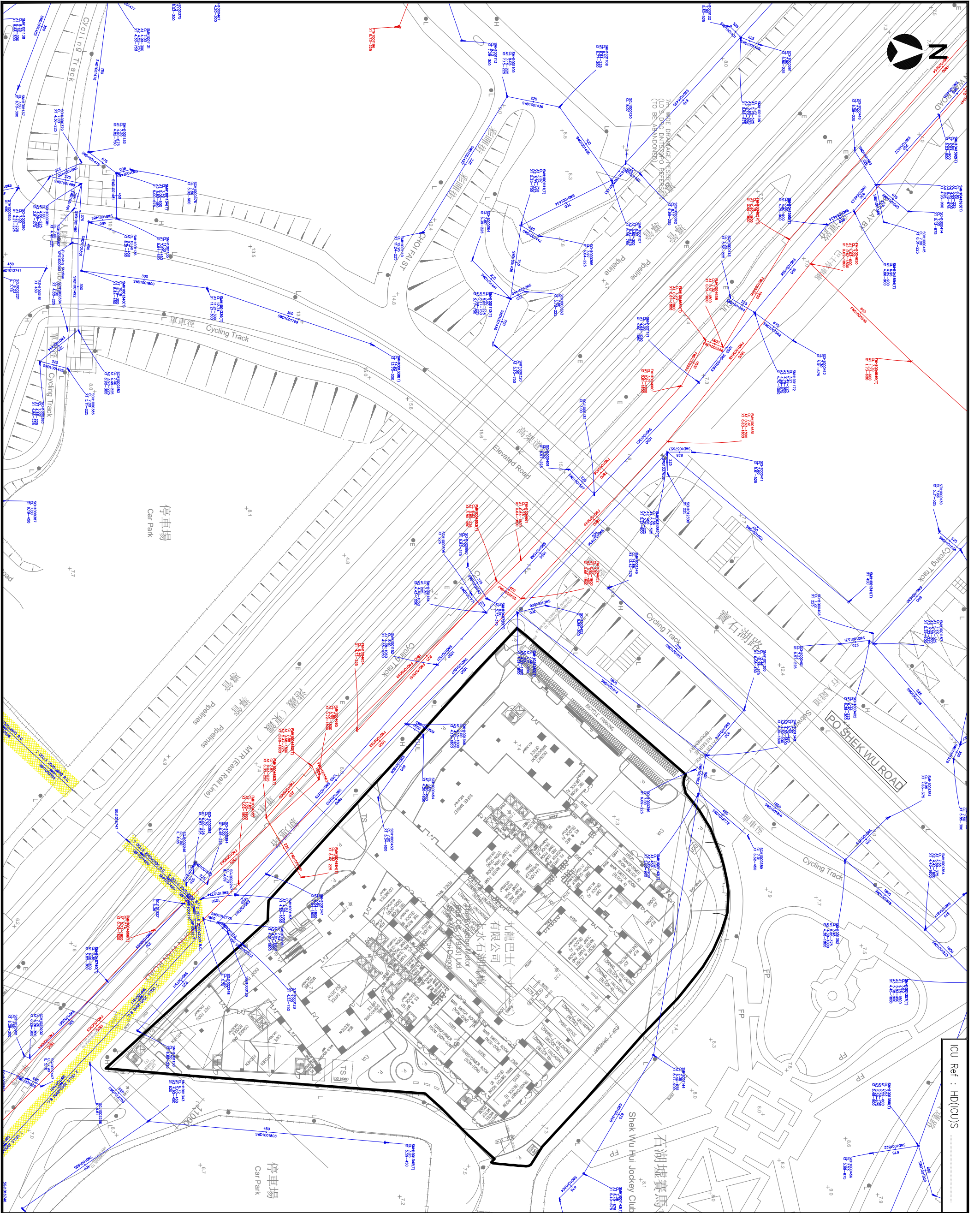
- 7.1.1 The Sewerage Impact Assessment (SIA) has been conducted to evaluate the possible impact on the existing sewerage system due to additional flow generated from the proposed public housing developments.
- 7.1.2 The main trunk is mainly responsible for transferring the sewage flow of the residential buildings and commercial buildings of Sheung Shui region to SWHSTW. The additional flow generated from the Site would only occupy about 1.5% of the utilization of the main trunk. The main trunk contains about 10% capacity for the further planning. Therefore, the sewage generation from the Site has minimal effect to the existing sewerage system.
- 7.1.3 Under Scenario 1 in Section 4.1.1, the estimated peak flow in the sewer section between manholes FMH1004664 and FMH1004662 exceeds 100% of full-bore capacity. It is recommended to upgrade the sewer section to 300dia concrete sewer.
- 7.1.4 The full-bore capacity of the DN1800 sewer section between manholes FMH1004651 and FMH1004650 is lower than other DN1800 sewer sections in the vicinity due to gentle gradient.

8. REFERENCES

- Site Layout Plan (with Typical Floor) (Option 10) (Drawing No. NO09/SCHEME B/LO-00/K), HKHA
- EPD/TP1/05 “Guidelines for Estimating Sewerage Flows for Sewage Infrastructure Planning”
- The Hong Kong Planning Standards and Guidelines (HKPSG), PlanD
- Sewerage Manual Part 1, Key Planning Issues and Gravity Collection System, DSD
- Commercial and Industrial Floor Space Utilization Survey, PD
- Guidelines for Registration of a New School, EDB
- Manhole and Flow Data, EPD
- Po Shek Wu Road Sewerage Impact Assessment Report (Report no. R3509/009)

Appendix A

Sewerage Layout Plans near the Site



ICU Ref : HD(CU)S

LEGEND:
 — SITE BOUNDARY
 — EXISTING SEWER

NO	DESCRIPTION AND DATE	INITIAL AND DESIGNATION

AUTHORISED	---
ENDORSED	---
CHECKED	---
DRAWN	---

AGREEMENT NO. : CB 20210448

PROJECT : Term Engineering Consultancy Services for New Territories East Region (2021-2023) - Instruction No. WP04 - Potential Public Housing at Po Shek Wu Road, Sheung Shui - Investigation

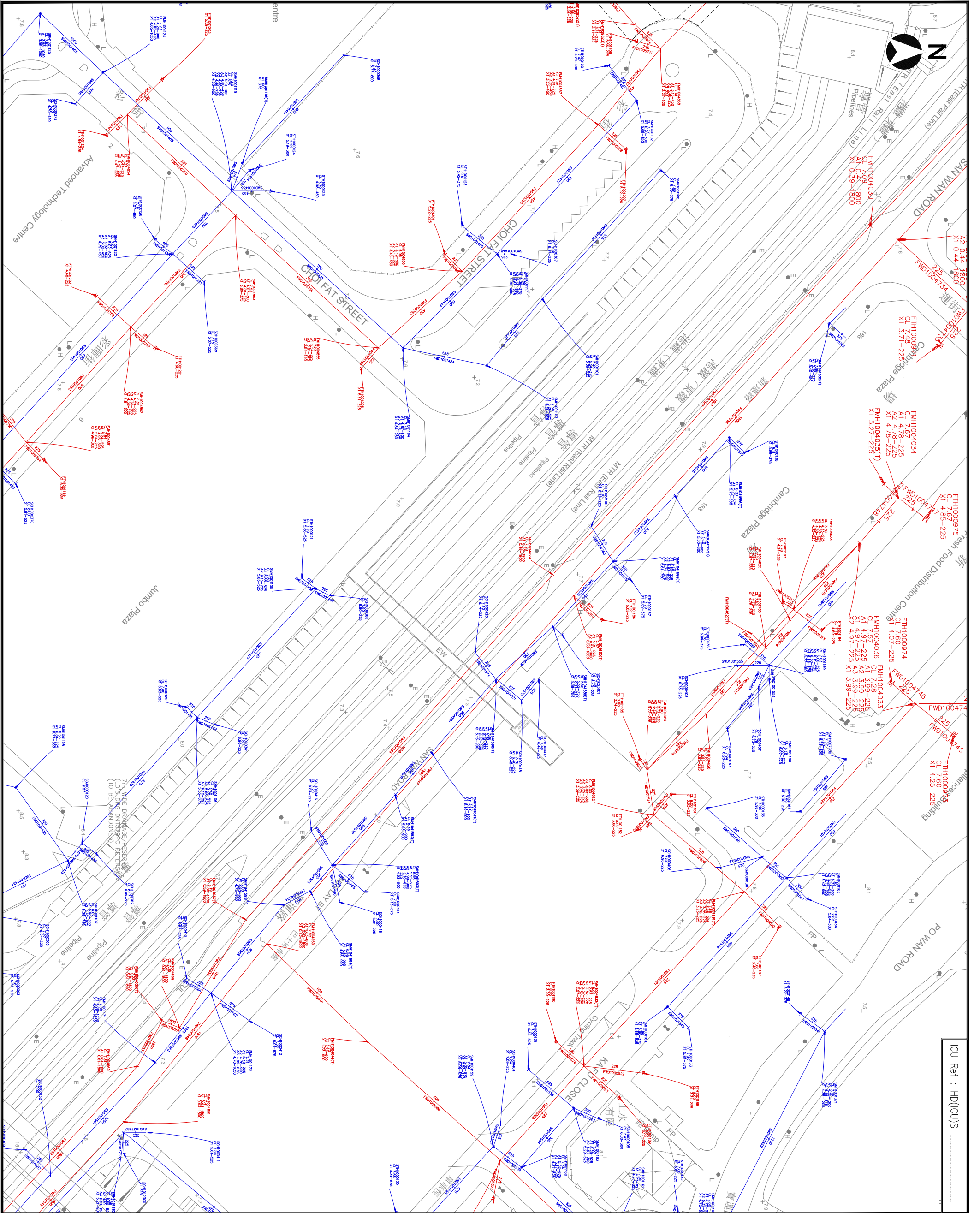
JOB NO. : 2512243A

DRAWING TITLE : SEWERAGE LAYOUT PLAN (SHEET 1 OF 2)

SCALE : 1 : 1000 @ A3

DRAWING NO. : WP04/SIA/001





ICU Ref : HD(CU)S

LEGEND:
 - - - - - SITE BOUNDARY
 - - - - - EXISTING SEWER

REVISIONS		INITIAL AND DESIGNATION	
NO	DESCRIPTION AND DATE	DMN	CRD / AUTH

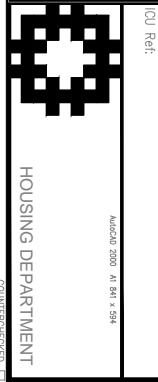
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ENDORSED	--/--
CHECKED	--/--
DRAWN	--/--

PROJECT
 Term Engineering Consultancy Services for
 New Territories East Region (2021-2023) -
 Instruction No. WP04 - Potential Public
 Housing at Po Shek Wu Road, Sheung Shui
 -Investigation

AGREEMENT NO. CB 20210448
 JOB NO. 2512243A

DRAWING TITLE
SEWERAGE LAYOUT PLAN
 (SHEET 2 OF 2)

SCALE 1 : 1000 @ A3
 DRAWING NO. WP04/SIA/002
 SOURCE
 ICU Ref:



Appendix B

Manhole and Flow Data Provided by
EPD (Extracted from Previous SIA
Report)

Location: **San Wan Road**
 Conditions: **Peak Wet Weather Flow**

Upstream Manhole No.	Downstream Manhole No.	Diameter (mm)	Length (m)	Sewer										Base Flow at Upstream Manhole				Base Flow at Downstream Manhole					
				Upstream G.L. (mPD)	Downstream G.L. (mPD)	Upstream I.L. (mPD)	Downstream I.L. (mPD)	Gradient (abs)	Grid (110)	Capacity (m³/s)	Capacity (l/s)	Water Level (m)	Velocity (m/s)	Flow (m³/s)	Flow (l/s)	Depth (m)	Velocity (m/s)	Flow (m³/s)	Flow (l/s)				
FMH1004754	FMH1004753	375	9.22	7.80	7.85	6.34	6.39	5.00	1.1966	N/A	N/A	N/A	0.7077	708	0.121	0.015	0.00038	0.38	0.072	0.042	0.00038	0.38	
FMH1004753	FMH1004752	375	7.07	12.85	7.85	7.61	1.59	1.11	0.0138	72	5.5767	72	5.5767	708	0.072	0.042	0.00038	0.38	0.072	0.042	0.00038	0.38	
FMH1004752	FMH1004667	1350	34.71	7.85	7.85	6.34	6.39	5.00	1.1966	N/A	N/A	N/A	0.7077	708	0.072	0.042	0.00038	0.38	0.072	0.042	0.00038	0.38	
FMH1004667	FMH1004666	1800	89.14	7.61	7.14	0.81	0.73	0.0009	114	3.0243	3024	1.110	1.110	1.110	1.110	0.711	1.04356	1043.56	1.141	0.685	1.05666	1056.66	
FMH1004666	FMH1004665	1800	67.70	7.14	7.85	0.73	0.72	0.0002	6370	1.2604	12604	1.140	0.685	1.03645	1036.45	1.144	0.707	1.02006	1020.06	1.144	0.699	1.03154	1031.54
FMH1004665	FMH1004662	1800	4.4714	7.85	7.89	0.72	0.68	0.0089	112	9.5648	9565	1.11	1.03183	1031.83	1.148	0.679	1.03154	1031.54	1.148	0.679	1.03154	1031.54	
FMH1004664	FMH1004663	225	19.2726	7.03	7.82	6.42	6.03	0.0198	51	0.0573	57	0.111	1.014	0.01771	17.71	0.111	0.111	0.01761	17.61	0.111	0.111	0.01761	17.61
FMH1004663	FMH1004662	225	19.8499	7.82	7.89	6.03	5.47	0.0282	35	0.0084	68	0.103	1.132	0.01758	17.58	0.103	1.132	0.01757	17.57	0.103	1.132	0.01757	17.57
FMH1004662	FMH1004661	1800	84.148	7.89	7.78	0.68	0.64	0.0005	2104	2.1989	2199	1.148	0.681	1.03149	1031.49	1.139	0.686	1.02905	1029.05	1.139	0.693	1.02905	1029.05
FMH1004661	FMH1004660	1800	67.941	7.78	7.31	0.64	0.61	0.0004	2265	2.1191	2119	1.138	0.666	1.02907	1029.07	1.122	0.701	1.02917	1029.17	1.122	0.701	1.02917	1029.17
FMH1004660	FMH1004659	1800	14.7651	7.31	7.32	0.61	0.61	0	N/A	N/A	N/A	1.118	0.704	1.02918	1029.18	1.115	0.706	1.02921	1029.21	1.115	0.706	1.02921	1029.21
FMH1004659	FMH1004658	1800	5.3849	7.23	7.32	0.61	0.61	0	N/A	N/A	N/A	1.111	0.709	1.02922	1029.22	1.099	0.721	1.02929	1029.29	1.099	0.721	1.02929	1029.29
FMH1004658	FMH1004657	1800	36.3397	7.32	7.19	0.61	0.6	0.0003	3636	1.6708	1671	1.111	0.709	1.02922	1029.22	1.121	0.708	1.02929	1029.29	1.121	0.708	1.02929	1029.29
FMH1004657	FMH1004659	1800	133.4572	7.19	7.2	0.59	0.5	0.0007	1472	2.6308	2630	1.108	0.713	1.02983	1029.83	1.113	0.785	1.17184	1171.84	1.113	0.785	1.17184	1171.84
FMH1004659	FMH1004749	1350	4.9997	7.85	7.77	7.09	7.09	0.49	0.41	0.0006	1690	2.4542	2454	2454	1.13	0.767	1.16964	1169.64	1.113	0.785	1.17184	1171.84	
FMH1004752	FMH1004749	1350	135.2077	7.2	7.2	0.49	0.41	0.0006	1690	2.4542	2454	1.13	0.767	1.16964	1169.64	1.113	0.785	1.17184	1171.84	1.113	0.785	1.17184	1171.84
FMH1004748	FMH1004748	600	28.8367	7.8	7.61	1.84	1.73	0.0038	262	0.343	343	0.352	0.945	0.11815	118.15	0.259	1.369	0.11815	118.15	0.259	1.369	0.11815	118.15
FMH1004751	FMH1004748	450	27.0741	7.88	7.61	2.81	2.83	0.0116	63	0.0512	51	0.064	0.449	0.00032	3.2	0.095	0.23	0.000316	3.16	0.095	0.23	0.000316	3.16
FMH1004749	FMH1004749	1350	12.8659	7.61	7.77	1.73	1.63	0.0078	138	N/A	N/A	0.881	0.368	0.00428	4.28	0.076	0.419	0.00427	4.27	0.076	0.419	0.00427	4.27
FMH1004748	FMH1004656	1800	36.1251	7.77	7.86	1.18	1.11	0.0019	516	4.4474	4447	0.928	0.925	1.20455	1204.55	0.986	0.854	1.20359	1203.59	0.986	0.854	1.20359	1203.59
FMH1004656	FMH1004655	1800	114.5311	7.86	7.65	1.11	1.02	0.0008	1275	2.8292	2829	0.985	0.947	1.20352	1203.52	0.901	1.25	1.20264	1202.64	0.901	1.25	1.20264	1202.64
FMH1004655	FMH1004652	1800	115.2603	7.65	7.85	1.02	0.65	0.0032	312	5.7266	5727	0.901	1.012	1.20363	1202.63	1.242	0.656	1.20212	1202.12	1.242	0.656	1.20212	1202.12
FMH1004654	FMH1004653	225	58.7384	6.46	6.32	4.73	3.8	0.0158	63	0.0512	51	0.064	0.449	0.00032	3.2	0.095	0.23	0.000316	3.16	0.095	0.23	0.000316	3.16
FMH1004653	FMH1004652	450	8.602	6.32	7.85	3.8	3.7	0.0116	86	0.2792	279	0.095	0.196	0.00315	3.15	0.095	0.196	0.00316	3.16	0.095	0.196	0.00316	3.16
FMH1004652	FMH1004651	1800	61.555	7.85	7.41	0.65	0.63	0.0003	3078	1.8167	1817	1.241	0.71	1.20390	1203.90	1.226	0.724	1.20265	1202.65	1.226	0.724	1.20265	1202.65
FMH1004651	FMH1004650	1800	65.4373	7.41	7.02	0.63	0.62	0.0002	6544	1.2435	1244	1.225	0.724	1.20265	1202.65	1.176	0.837	1.35662	1356.62	1.176	0.837	1.35662	1356.62
FMH1004650	FMH1004650	1800	135.2058	7.02	7.57	0.62	0.53	0.0007	1480	2.6231	2623	1.194	0.816	1.35298	1352.98	1.176	0.837	1.35662	1356.62	1.176	0.837	1.35662	1356.62
FMH1004650	FMH1004626	1800	138.0332	7.57	7.72	0.53	0.44	0.0007	1534	2.5766	2577	1.175	0.839	1.35667	1356.67	1.144	0.879	1.3637	1363.7	1.144	0.879	1.3637	1363.7
FMH1004626	FMH1004027	1800	101.1782	7.72	7.12	0.44	0.37	0.0007	1445	2.6544	2654	1.143	0.881	1.365	1.365	1.122	0.931	1.37278	1372.78	1.122	0.931	1.37278	1372.78
FMH1004027	FMH1004029	1800	101.9799	7.12	5.4	0.37	0.29	0.0008	1275	2.827	2827	1.121	0.977	1.48	1.48	1.104	1.107	1.48242	1482.42	1.104	1.107	1.48242	1482.42
FMH1004029	FMH100411	1800	67.9912	5.4	7	0.29	0.21	0.0001	971	3.2409	3241	1.104	0.821	1.15253	1152.53	1.136	0.823	1.15485	1154.85	1.136	0.823	1.15485	1154.85
FMH100411	FMH1004113	1800	12.5305	7	0.22	0.22	0.21	0.0008	1235	2.8514	2851	1.133	0.826	1.15499	1154.99	1.136	0.83	1.15561	1155.61	1.136	0.83	1.15561	1155.61
FMH1004113	FMH1004115	1500	61.6195	7.09	5	0.21	0.12	0.0015	685	2.3887	2389	1.133	0.832	1.15575	1155.75	1.095	0.805	1.15951	1159.51	1.095	0.805	1.15951	1159.51
FMH1004115	FMH1004031	1800	103.2766	7.09	6.99	0.36	0.36	0.0003	3443	1.7173	1717	1.132	0.766	1.17188	1171.88	1.097	0.835	1.17356	1173.56	1.097	0.835	1.17356	1173.56
FMH1004031	FMH1004032	1800	104.6983	5	6.99	0.3	0.29	0.0001	10669	0.9816	982	1.136	0.771	1.17341	1173.41	1.104	0.88	1.156135	1563.35	1.104	0.88	1.156135	1563.35
FMH1004032	FMH1004112	1800	67.9912	6.99	0.25	0.18	0.18	0.0001	971	3.2409	3241	1.135	1.064	1.56029	1560.29	1.14	1.15	1.56135	1563.35	1.14	1.15	1.56135	1563.35
FMH1004112	FMH1004114	1500	62.3701	6.99	0.18	0.18	0.001	1040	1.976	1976	1.139	1.04	1.56352	1563.52	1.178	1.017	1.56752	1567.52	1.178	1.017	1.56752	1567.52	
FMH1004114	FMH1004117	1800	37.5897	0.18	0.08	0.12	0.08	0.0011	940	3.2938	3294	1.102	2.446	3.99102	3991.02	0.988	2.789	3.99063	3990.63	0.988	2.789	3.99063	3990.63
FMH1004029	FMH1004032	1800	5.3851	5.4	6.99	0.29	0.29	0	N/A	N/A	N/A	1.104	0.376	0.35111	351.11	1.104	0.378	0.3516	351.6	1.104	0.378	0.3516	351.6
FMH1004115	FMH1004114	1500	9.2193	0.12	0.12	0	0	0	N/A	N/A	N/A	1.184	0.931	1.15973	1159.73	1.178	0.947	1.16029	1160.29	1.178	0.947	1.16029	1160.29

Appendix C

Estimation of Pipeline Roughness
Coefficient (Extracted from
Previous SIA Report)

Project : Sewerage Impact Assessment for Po Shek Wu Road
Project No.: 3509

	INITIAL	DATE	REV.
CHECKED BY	AK	Mar-17	1
PREPARED BY	LE	Mar-17	1

Hydraulic pipeline roughness (m) = 0.00312

Manhole		Pipe Diameter (mm)	Cover Level (mPD)		Invert Level (mPD)		Pipe Length (m)	Hydraulic Gradient (1 in)	Capacity by Colebrook-White Equation (l/s)	Capacity Provided by EPD (l/s)	Error (%)
From	To		Upstream manhole	Downstream manhole	From	To					
FMH1004664	FMH1004663	225	7.03	7.82	6.42	6.03	19.72	50.6	57.00	57.00	0.01
FMH1004663	FMH1004662	225	7.82	7.89	6.03	5.47	19.8	35.4	68.09	68.00	0.13
FMH1004662	FMH1004661	1800	7.89	7.78	0.68	0.64	84.15	2103.7	2195.40	2199.00	-0.16
FMH1004661	FMH1004660	1800	7.78	7.31	0.64	0.61	67.94	2264.7	2115.92	2119.00	-0.15
FMH1004658	FMH1004657	1800	7.32	7.19	0.61	0.60	36.36	3636.0	1669.91	1671.00	-0.06
FMH1004657	FMH1004629	1800	7.19	7.20	0.59	0.50	132.46	1471.7	2624.75	2630.00	-0.20
FMH1004629	FMH1004030	1800	7.20	7.09	0.49	0.41	135.21	1690.1	2449.34	2454.00	-0.19
FMH1004030	FMH1004031	1800	7.09	5.00	0.39	0.36	103.28	3442.55	1716.19	1717.00	-0.05
Total Absolute Error =										0.95	

Hydraulic pipeline roughness (m) = 0.00311

Manhole		Pipe Diameter (mm)	Cover Level (mPD)		Invert Level (mPD)		Pipe Length (m)	Hydraulic Gradient (1 in)	Capacity by Colebrook-White Equation (l/s)	Capacity Provided by EPD (l/s)	Error (%)
From	To		Upstream manhole	Downstream manhole	From	To					
FMH1004664	FMH1004663	225	7.03	7.82	6.42	6.03	19.72	50.6	57.04	57.00	0.06
FMH1004663	FMH1004662	225	7.82	7.89	6.03	5.47	19.8	35.4	68.13	68.00	0.19
FMH1004662	FMH1004661	1800	7.89	7.78	0.68	0.64	84.15	2103.7	2196.32	2199.00	-0.12
FMH1004661	FMH1004660	1800	7.78	7.31	0.64	0.61	67.94	2264.7	2116.81	2119.00	-0.10
FMH1004658	FMH1004657	1800	7.32	7.19	0.61	0.60	36.36	3636.0	1670.61	1671.00	-0.02
FMH1004657	FMH1004629	1800	7.19	7.20	0.59	0.50	132.46	1471.7	2625.85	2630.00	-0.16
FMH1004629	FMH1004030	1800	7.20	7.09	0.49	0.41	135.21	1690.1	2450.37	2454.00	-0.15
FMH1004030	FMH1004031	1800	7.09	5.00	0.39	0.36	103.28	3442.55	1716.90	1717.00	-0.01
Total Absolute Error =										0.81	

Hydraulic pipeline roughness (m) = 0.00310

Manhole		Pipe Diameter (mm)	Cover Level (mPD)		Invert Level (mPD)		Pipe Length (m)	Hydraulic Gradient (1 in)	Capacity by Colebrook-White Equation (l/s)	Capacity Provided by EPD (l/s)	Error (%)
From	To		Upstream manhole	Downstream manhole	From	To					
FMH1004664	FMH1004663	225	7.03	7.82	6.42	6.03	19.72	50.6	57.07	57.00	0.12
FMH1004663	FMH1004662	225	7.82	7.89	6.03	5.47	19.8	35.4	68.17	68.00	0.24
FMH1004662	FMH1004661	1800	7.89	7.78	0.68	0.64	84.15	2103.7	2197.24	2199.00	-0.08
FMH1004661	FMH1004660	1800	7.78	7.31	0.64	0.61	67.94	2264.7	2117.70	2119.00	-0.06
FMH1004658	FMH1004657	1800	7.32	7.19	0.61	0.60	36.36	3636.0	1671.32	1671.00	0.02
FMH1004657	FMH1004629	1800	7.19	7.20	0.59	0.50	132.46	1471.7	2626.96	2630.00	-0.12
FMH1004629	FMH1004030	1800	7.20	7.09	0.49	0.41	135.21	1690.1	2451.40	2454.00	-0.11
FMH1004030	FMH1004031	1800.00	7.09	5.00	0.39	0.36	103.28	3442.55	1717.62	1717.00	0.04
Total Absolute Error =										0.79	

Hydraulic pipeline roughness (m) = 0.00309

Manhole		Pipe Diameter (mm)	Cover Level (mPD)		Invert Level (mPD)		Pipe Length (m)	Hydraulic Gradient (1 in)	Capacity by Colebrook-White Equation (l/s)	Capacity Provided by EPD (l/s)	Error (%)
From	To		Upstream manhole	Downstream manhole	From	To					
FMH1004664	FMH1004663	225	7.03	7.82	6.42	6.03	19.72	50.6	57.10	57.00	0.18
FMH1004663	FMH1004662	225	7.82	7.89	6.03	5.47	19.8	35.4	68.21	68.00	0.30
FMH1004662	FMH1004661	1800	7.89	7.78	0.68	0.64	84.15	2103.7	2198.16	2199.00	-0.04
FMH1004661	FMH1004660	1800	7.78	7.31	0.64	0.61	67.94	2264.7	2118.59	2119.00	-0.02
FMH1004658	FMH1004657	1800	7.32	7.19	0.61	0.60	36.36	3636.0	1672.02	1671.00	0.06
FMH1004657	FMH1004629	1800	7.19	7.20	0.59	0.50	132.46	1471.7	2628.06	2630.00	-0.07
FMH1004629	FMH1004030	1800	7.20	7.09	0.49	0.41	135.21	1690.1	2452.43	2454.00	-0.06
FMH1004030	FMH1004031	1800	7.09	5.00	0.39	0.36	103.28	3442.55	1718.35	1717.00	0.08
Total Absolute Error =										0.82	

Hydraulic pipeline roughness (m) = 0.00308

Manhole		Pipe Diameter (mm)	Cover Level (mPD)		Invert Level (mPD)		Pipe Length (m)	Hydraulic Gradient (1 in)	Capacity by Colebrook-White Equation (l/s)	Capacity Provided by EPD (l/s)	Error (%)
From	To		Upstream manhole	Downstream manhole	From	To					
FMH1004664	FMH1004663	225	7.03	7.82	6.42	6.03	19.72	50.6	57.14	57.00	0.24
FMH1004663	FMH1004662	225	7.82	7.89	6.03	5.47	19.8	35.4	68.25	68.00	0.36
FMH1004662	FMH1004661	1800	7.89	7.78	0.68	0.64	84.15	2103.7	2199.09	2199.00	0.00
FMH1004661	FMH1004660	1800	7.78	7.31	0.64	0.61	67.94	2264.7	2119.48	2119.00	0.02
FMH1004658	FMH1004657	1800	7.32	7.19	0.61	0.60	36.36	3636.0	1672.73	1671.00	0.10
FMH1004657	FMH1004629	1800	7.19	7.20	0.59	0.50	132.46	1471.7	2629.17	2630.00	-0.03
FMH1004629	FMH1004030	1800	7.20	7.09	0.49	0.41	135.21	1690.1	2453.46	2454.00	-0.02
FMH1004030	FMH1004031	1800	7.09	5.00	0.39	0.36	103.28	3442.55	1719.07	1717.00	0.12
Total Absolute Error =										0.90	

Note: The highlighted cells represent the hydraulic pipeline roughness with the calculated capacities best fit the data provided by EPD.

Appendix D

Sewerage Flow Generated by the Site

Appendix D - Estimation of Sewage Flow from the Development

Pcif = 1.0 UFF Workers = 0.28

1) Domestic Flow

1.1 Public Residential Building Block:

Total Flat	=	1904 flat	
Assumed Household Size	=	2.8 persons/household	
Total Population	=	5332	
Factored Total Population	=	5866 people	(with 10% allowance)
Unit Flow Factor	=	0.27 m ³ /d/person	(Unit flow for Subsidised Sales Flats)
Estimated ADWF	=	5866 x 0.27	= 1583.8 m ³ /day
Total ADWF with CIF 1			1583.8 m³/day

2) Commercial and Institutional Flow

2.1 Retail

Total Floor Area (Internal Floor Area)	=	1800 m ²	
GFA	=	2394 m ²	(Assume = 1.33*NOFA)
Worker Density	=	3.5 staff/100m ²	(Assumed Retail Trade (Commercial and Industrial Floor Space Utilization Survey)
Total numbers of staff	=	84 staff	
Unit Flow Factor for workers	=	0.28 m ³ /d/person	(Unit flow for J4 Wholesale & Retail in GEFS)
Estimated ADWF	=		23.5 m ³ /day
Total ADWF with CIF 1			23.5 m³/day

2.2 Kindergarten

Number of Classroom	=	6 rooms	
GFA	=	985 m ²	
Students / Classroom	=	30 per classroom	
Number of Students	=	180 students	
Factored Student's Number	=	198 people	(with 10% allowance)
Staffs Number	=	3.3 staff/100m ²	(Assumed Community, Social & Personal Services (Commercial and Industrial Floor Space Utilization Survey)
Total numbers of staffs	=	33 staff	
Unit Flow Factor for staffs	=	0.28 m ³ /d/person	(Unit flow for J11 Community, Social & Personal Services in GEFS)
Unit Flow Factor for students	=	0.04 m ³ /d/person	(Unit flow for School student in GEFS)
Estimated ADWF	=		17.0 m ³ /day
Total ADWF with CIF 1			17.0 m³/day

2.3 Post office

Total Floor Area (Internal Floor Area)	=	400 m ²	
GFA	=	532 m ²	(Assume = 1.33*NOFA)
Worker Density	=	3.3 staff/100m ²	(Assumed Community, Social & Personal Services (Commercial and Industrial Floor Space Utilization Survey)
Total numbers of staff	=	18 staff	
Unit Flow Factor for workers	=	0.28 m ³ /d/person	(Unit flow for J11 Community, Social & Personal Services in GEFS)
Estimated ADWF	=		5.0 m ³ /day
Total ADWF with CIF 1			5.0 m³/day

2.4 A district management office and A management office for the Site

Total Floor Area (Internal Floor Area)	=	558 m ²	
GFA	=	742.14 m ²	(Assume = 1.33*NOFA)
Worker Density	=	3.3 staff/100m ²	(Assumed Community, Social & Personal Services (Commercial and Industrial Floor Space Utilization Survey)
Total numbers of staff	=	25 staff	
Unit Flow Factor for workers	=	0.28 m ³ /d/person	(Unit flow for J11 Community, Social & Personal Services in GEFS)
Estimated ADWF	=		7.0 m ³ /day
Total ADWF with CIF 1			7.0 m³/day

2.5 Associated ancillary facilities and external works, including open parking spaces for bicycles;

Total Floor Area (Internal Floor Area)	=	5759 m ²	
GFA	=	7659.47 m ²	(Assume = 1.33*NOFA)
Worker Density	=	3.8 staff/100m ²	(Assumed Transport (Commercial and Industrial Floor Space Utilization Survey)
Total numbers of staff	=	292 staff	
Unit Flow Factor for workers	=	0.18 m ³ /d/person	(Unit flow for J3 Transport, Storage & Communication in GEFS)
Estimated ADWF	=		52.6 m ³ /day
Total ADWF with CIF 1			52.6 m³/day

2.6 A 100-place Child Care Centre (CCC);

Total Floor Area (Internal Floor Area)	=	530 m ²	
GFA	=	704.9 m ²	(Assume = 1.33*NOFA)
Total numbers of Child	=	100 persons	
Total numbers of staff	=	33 staff	(From Notional Staffing Establishments of Social Welfare Department, 1 workers for 3 places)
Unit Flow Factor for Child	=	0.19 m ³ /d/person	
Unit Flow Factor for workers	=	0.28 m ³ /d/person	(Unit flow for J11 Community, Social & Personal Services in GEFS)
Estimated ADWF	=		28.3 m ³ /day
Total ADWF with CIF 1			28.3 m³/day

2.7 A 100-place Residential Care Home for the Elderly (RCHE);

Total Floor Area (Internal Floor Area)	=	1354 m ²	
GFA	=	1800.82 m ²	(Assume = 1.33*NOFA)
Total numbers of Elderly Persons	=	100 persons	
Total numbers of staff	=	54 staff	(From Notional Staffing Establishments of Social Welfare Department, 108 workers for 200 places)
Unit Flow Factor for Elderly	=	0.19 m ³ /d/person	
Unit Flow Factor for workers	=	0.28 m ³ /d/person	(Unit flow for J11 Community, Social & Personal Services in GEFS)
Estimated ADWF	=		34.1 m ³ /day
Total ADWF with CIF 1			34.1 m³/day

2.8 A main base of Short-term Food Assistance Service Team (STFAST);

Total Floor Area (Internal Floor Area)	=	92.5 m ²	
GFA	=	123.025 m ²	(Assume = 1.33*NOFA)
Worker Density	=	3.3 staff/100m ²	(Assumed Community, Social & Personal Services (Commercial and Industrial Floor Space Utilization Survey)
Total numbers of staff	=	5 staff	
Unit Flow Factor for workers	=	0.28 m ³ /d/person	(Unit flow for J11 Community, Social & Personal Services in GEFS)
Estimated ADWF	=		1.4 m ³ /day
Total ADWF with CIF 1			1.4 m³/day

2.9 Home Care Services (HCS) for Frail Elderly Persons

Total Floor Area (Internal Floor Area)	=	142 m ²	
GFA	=	188.86 m ²	(Assume = 1.33*NOFA)
Total numbers of Elderly Persons	=	100 persons	
Total numbers of staff	=	22 staff	(From Notional Staffing Establishments of Social Welfare Department, 15.51 workers for 70 places)
Unit Flow Factor for Elderly	=	0.19 m ³ /d/person	
Unit Flow Factor for staffs	=	0.28 m ³ /d/person	(Unit flow for J11 Community, Social & Personal Services in GEFS)
Estimated ADWF	=		25.2 m ³ /day
Total ADWF with CIF 1			25.2 m³/day

Appendix E

Hydraulic Analysis for Existing Sewers

Job No.	231243A	Sheet No.	
Proposed Housing Development at Po Shek Wu Road			
Member/Location			
Dwg Ref.			
Drawn by		Date	10-Aug-2023
Check by			

Proposed Housing Development at Po Shek Wu Road
 Appendix E1 - Hydraulic Analysis for Existing Sewers (including other Planning Developments)

Colebrook-White Equation:

$$V = \sqrt{(8gDS)} \log\left(\frac{ks}{3.7D} + \frac{2.51v}{D\sqrt{(2gDS)}}\right)$$

kinematic viscosity of water = 0.00000114 m²/s
 Vitrified clay pipe: ks= 0.600 mm
 HDPE pipe: ks= 0.300 mm
 Concrete pipe (Existing): ks= 3.100 mm
 g= 9.81 m/s²

Existing Sewerage System		No.		Length (m)	Dia. (mm)	Pipe Material	Roughness (mm)	US Cl. (m ² /D)	DS Cl. (m ² /D)	US IL. (m ² /D)	DS IL. (m ² /D)	US Cover (m)	DS Cover (m)	Gradient (1 in x)	Pipe Area (m ²)	Perimeter (m)	R=4/P (m)	Vel. @ full bore (m/sec)	Contributing Zones	Sewerage Flow Increased due to the Site (L/sec)	Existing Peak Flow (L/sec)	Cumulative Sewerage Flow (L/sec)	Cumulative Sewerage Flow (m ³ /day)	Contributing Population	Peaking Factor ¹⁾	Cumulative Peak Flow (L/sec)	Pipe Capacity (L/sec)	Utilization (%)	Flow Capacity Check	Remark
No.	DS MH																													
FMH1004664	FMH1004663	19.72	225	19.72	1800	Concrete pipe (Existing)	3.10	7.03	7.82	6.42	6.03	4.56	1.54	0.0198	0.04	0.71	0.06	1.43	EPDS Data	0.00	17.7	17.71	1530.14	5667	1.00	17.71	56.92	31.1	YES	
FMH1004663	FMH1004662	19.85	225	19.85	1800	Concrete pipe (Existing)	3.10	7.82	7.89	6.03	5.47	1.54	2.17	0.0282	0.04	0.71	0.06	1.71	EPDS Data	0.00	17.6	17.58	1518.91	5626	1.00	17.58	68.01	25.8	YES	
FMH1004662	FMH1004661	84.15	1800	84.15	1800	Concrete pipe (Existing)	3.10	7.89	7.78	6.68	6.64	5.19	5.12	0.0005	2.54	5.65	0.45	0.86	EPDS Data	0.00	1031.5	1031.49	89120.74	330077	1.00	1031.49	2188.68	47.1	YES	
FMH1004661	FMH1004660	67.94	1800	67.94	1800	Concrete pipe (Existing)	3.10	7.78	7.31	6.64	6.61	5.12	4.68	0.0004	2.54	5.65	0.45	0.83	EPDS Data	0.00	1029.0	1029.07	88903.60	329280	1.00	1029.07	2109.19	48.8	YES	
FMH1004660	FMH1004659	14.77	1800	14.77	1800	Concrete pipe (Existing)	3.10	7.31	7.23	6.61	6.61	4.68	4.60	N/A	2.54	5.65	0.45	N/A	EPDS Data	0.00	1029.1	1029.07	88903.60	329280	1.00	1029.07	N/A	N/A	N/A	N/A
FMH1004659	FMH1004658	5.38	1800	5.38	1800	Concrete pipe (Existing)	3.10	7.23	7.32	6.61	6.61	4.69	4.69	N/A	2.54	5.65	0.45	N/A	EPDS Data	0.00	1029.2	1029.18	88921.15	329338	1.00	1029.18	N/A	N/A	N/A	N/A
FMH1004658	FMH1004657	56.56	1800	56.56	1800	Concrete pipe (Existing)	3.10	7.32	7.19	6.61	6.60	4.68	4.57	0.0003	2.54	5.65	0.45	0.65	EPDS Data	0.00	1029.2	1029.22	88924.61	329350	1.00	1029.22	1663.06	61.9	YES	
FMH1004657	FMH1004629	132.46	1800	132.46	1800	Concrete pipe (Existing)	3.10	7.19	7.20	6.59	6.50	4.68	4.68	0.0006	2.54	5.65	0.45	1.03	EPDS Data	0.00	1029.8	1029.83	88977.31	329346	1.00	1029.83	2618.17	39.3	YES	
FMH1004629	FMH1004031	132.21	1800	132.21	1800	Concrete pipe (Existing)	3.10	7.20	7.09	6.59	6.41	4.69	4.66	0.0005	2.54	5.65	0.45	0.96	EPDS Data	0.00	1169.6	1169.64	101056.90	374285	1.00	1169.64	2442.70	47.9	YES	
FMH1004031		103.28	1800	103.28	1800	Concrete pipe (Existing)	3.10	7.09	5.00	6.59	6.36	4.68	2.62	0.0003	2.54	5.65	0.45	0.67	EPDS Data	0.00	1171.9	1171.88	101250.43	375002	1.00	1171.88	1709.34	68.6	YES	

1. Peaking factor (including stormwater allowance) is used for existing sewer. Peaking factor is 1 because the existing flow data from EPD has already included peaking factor.
 2. The assumption on the baseline upstream peak flow is based on EPD's data for the exact sewerage flow from the upstream of the FMH1004662.
 3. The sewerage amount from the upstream of manhole FMH1004662 is based on the information from EPD.

Proposed Housing Development at Pot Still Way Road

Appendix E2 - Hydraulic Analysis for Sewers After Development without Mitigation Measures

$$V = \left(\frac{8.49 S}{k_s} \right)^{0.54} \log k_s \left(\frac{2.51 V}{5.7 D} + D \right)^{0.54}$$

Hydraulic viscosity of water = 0.0000114 m²/s
 Virtual clay pipe: k_s = 0.600 mm
 HDPE pipe: k_s = 0.300 mm
 Concrete pipe (existing): k_s = 3.81 mm/s²

Job No.	201223A	Sheet No.	
Proposed Housing Development at Pot Still Way Road			
Member Location			
Prop. Ref.			
Scale by	1:500	Date	19/06/2022

Existing Sewerage System After the Completed the Development

No.	US MH	USMH	Length (m)	Dia. (mm)	Pipe Material	Roughness (mm)	US GL (mPD)	DS GL (mPD)	US TL (mPD)	DS TL (mPD)	US Cover (m)	DS Cover (m)	Gradient (1 in 100)	Gradient (1 in 100)	Pipe Area (m ²)	Perimeter (m)	R & A/P (m ² /m)	Vd @ full flow (m/s)	Contributing Zones	Sewage Flow Increased due to the Site (l/s)	Existing Peak Sewage Flow (l/s)	Cumulative Sewage Flow (l/s)	Cumulative Sewage Flow (l/d)	Contributing Population	Peaking Factor ¹	Cumulative Peak Flow (l/s)	Pipe Capacity (l/s)	Utilisation (%)	Flow Capacity Check	Remark
FMH100664	FMH100664	FMH100664	18.72	225	Concrete pipe (existing)	3.00	7.82	7.82	6.62	6.62	0.36	1.54	0.008	5.1	0.04	0.71	0.06	1.43		20.58	0.00	20.58	1778.02	688	5.00	102.89	56.92	18.8	NGP ²	
FMH100665	FMH100665	FMH100665	19.88	225	Concrete pipe (existing)	3.00	7.82	7.82	6.62	6.62	0.36	1.54	0.008	5.1	0.04	0.71	0.06	1.43		20.58	0.00	20.58	1778.02	688	5.00	102.89	56.92	18.8	NGP ²	
FMH100666	FMH100666	FMH100666	84.13	180	Concrete pipe (existing)	3.00	7.89	7.78	6.08	6.04	5.12	4.68	0.004	21.04	2.54	5.65	0.45	0.84		283.92	101.49	313.41	11424.96	42039	2.40	315.97	218.66	14.2	NGP ²	
FMH100667	FMH100667	FMH100667	67.94	180	Concrete pipe (existing)	3.00	7.78	7.71	6.04	6.01	5.12	4.68	0.004	22.06	2.54	5.65	0.45	0.84		283.92	102.00	313.92	11424.96	42039	1.00	317.92	219.19	62.2	YES	
FMH100668	FMH100668	FMH100668	5.38	180	Concrete pipe (existing)	3.00	7.21	7.21	6.01	6.01	4.69	4.69	N/A	N/A	2.54	5.65	0.45	N/A		283.92	102.18	313.10	11343.41	42039	1.00	313.10	N/A	N/A	YES	
FMH100669	FMH100669	FMH100669	34.36	180	Concrete pipe (existing)	3.00	7.21	7.19	6.01	6.00	4.69	4.67	0.003	36.36	2.54	5.65	0.45	0.65		283.92	102.22	313.14	11343.41	42039	1.00	313.14	1681.06	79.0	YES	
FMH100670	FMH100670	FMH100670	133.46	180	Concrete pipe (existing)	3.00	7.20	7.20	6.00	6.00	4.68	4.68	0.007	142.7	2.54	5.65	0.45	1.03		283.92	102.81	313.75	11397.57	42039	1.00	313.75	242.70	59.2	YES	
FMH100671	FMH100671	FMH100671	133.21	180	Concrete pipe (existing)	3.00	7.20	7.20	6.00	6.00	4.69	4.69	0.006	140.0	2.54	5.65	0.45	0.96		283.92	117.28	313.96	12580.09	42039	1.00	313.96	179.25	63.2	YES	

1. Peaking factor (existing sewerage network) based on the existing flow data from IPTD.
 2. The average value of the peak flow rate (l/s) for the sewerage system based on the operation of the FMH100662.
 3. The average value from the operation of the FMH100662's based on the information from IPTD.

Appendix F

Sewerage Layout Plan and Hydraulic Analysis for Mitigation Measures

Job No. 2512253A	Sheet No.	Rev.
Proposed Housing Development at Po Shek Wu Road		A
Member/ Location		
Dwg. Ref.		
Made by TC	Date 10/Aug/2023	

Proposed Housing Development at Po Shek Wu Road

Appendix F1 - Hydraulic Analysis for Sewers After Development with Mitigation Measures

Colebrook-White Equation:
$$f = \frac{1}{\left(\frac{1.49}{k_s} \log \left(\frac{3.7D}{k_s} + \frac{2.51v}{D \sqrt{2gDs}} \right) \right)^2}$$

Kinematic viscosity of water = 0.00000114 m²/s
 Vitrified clay pipe ks = 0.600 mm
 HDPE pipe ks = 0.300 mm
 Concrete pipe (Existing) ks = 3.100 mm
 Concrete pipe (Proposed) ks = 3.000 mm
 r = 9.81 m/s²

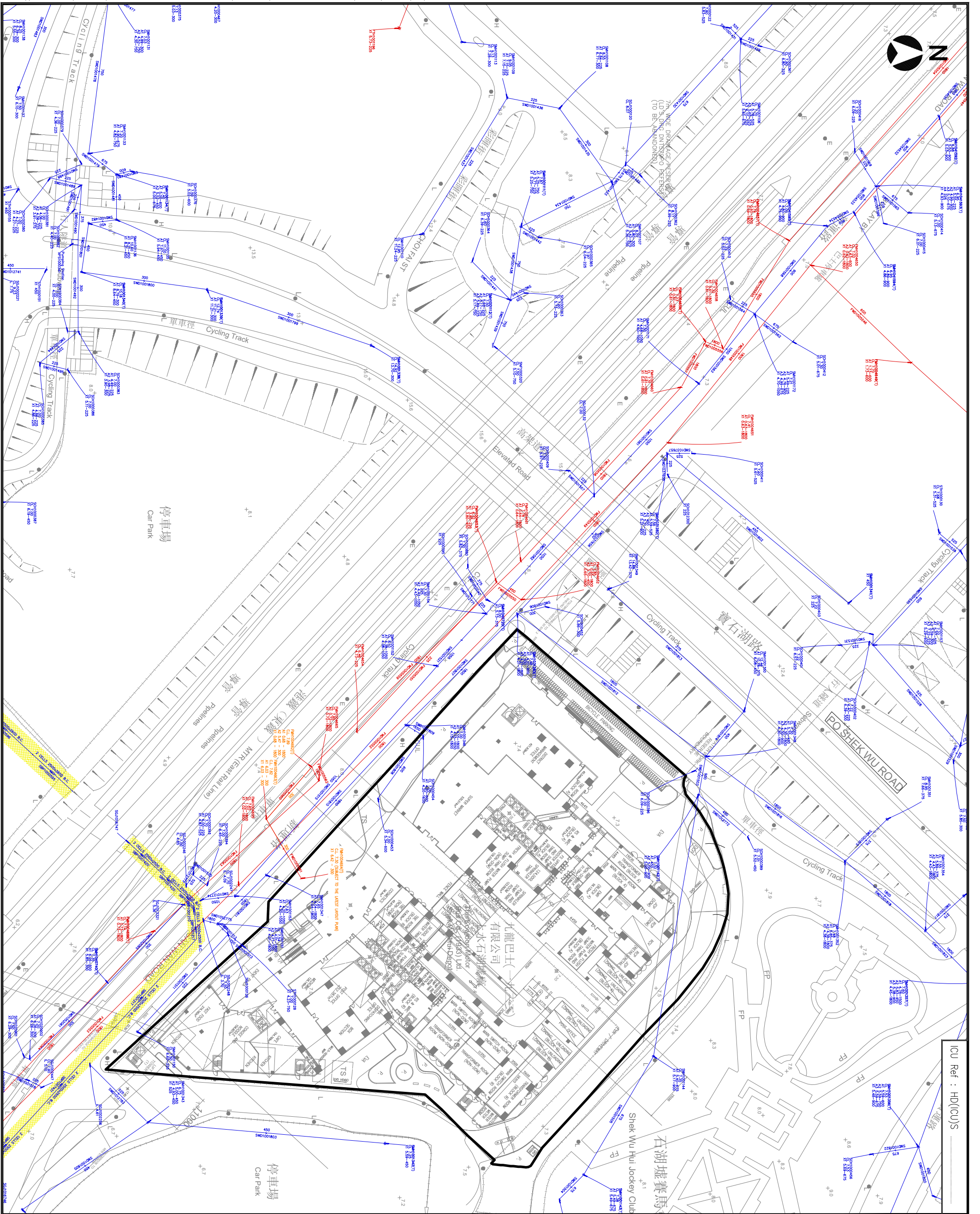
Existing Sewerage System After Upgrading Works		Length		Dia.		Pipe Material		Roughness		US GL		DS GL		US IL		DS IL		US Cover		DS Cover		Gradient		Pipe Area		Perimeter		R = A/P		Vd @ full bore		Contributing Zones		Sewage Flow Increased due to the Site		Existing Peak Flow		Cumulative Sewage Flow		Cumulative Sewage Flow		Contributing Population		Peaking Factor ⁽¹⁾		Cumulative Peak Flow		Pipe Capacity		Utilization (%)		Flow Capacity Check		Remark	
No.	DS MH	US MH	(m)	(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	(mPD)	(mPD)	(mPD)	(mPD)	(m)	(m)	(m)	(m)	(m)	(m)	(m)	(m)	(1 in x)	(m ²)	(m)	(m)	(m/sec)	(m/sec)		(L/sec)	(L/sec)	(L/sec)	(m ³ /day)		(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)	(L/sec)							
FMH1004664	FMH1004663		19.72	300	Concrete pipe (Proposed)	3.00	7.30	7.82	6.42	6.03	5.47	1.45	2.08	0.07	0.94	0.94	0.08	1.75	2.09	the Site	20.58	0.00	20.58	1778.02	6885	5.00	102.89	123.59	83.3	YES	Upgraded to 300dia pipe																								
FMH1004663	FMH1004662		19.85	300	Concrete pipe (Proposed)	3.00	7.82	7.89	6.03	5.47	1.45	2.08	0.08	0.07	0.94	0.94	0.08	1.75	2.09	the Site	20.58	0.00	20.58	1778.02	6885	5.00	102.89	147.66	69.7	YES																									
FMH1004662	FMH1004661		84.15	180	Concrete pipe (Existing)	3.10	7.89	7.78	0.68	0.64	5.19	5.12	4.68	0.00004	2.54	5.65	0.45	0.86	0.83	Planning	283.92	1031.49	1315.41	113650.99	4209.30	1.00	1315.41	2188.68	60.1	YES																									
FMH1004661	FMH1004660		67.94	180	Concrete pipe (Existing)	3.10	7.78	7.31	0.61	0.61	4.68	4.60	4.60	0.0004	2.54	5.65	0.45	0.83	N/A	Developments/	283.92	1029.00	1312.92	113435.86	4201.33	1.00	1312.92	2109.19	62.2	YES																									
FMH1004660	FMH1004659		14.77	180	Concrete pipe (Existing)	3.10	7.31	7.23	0.61	0.61	4.60	4.60	4.60	N/A	2.54	5.65	0.45	N/A	N/A	Applications	283.92	1029.07	1312.99	113441.91	4201.55	1.00	1312.99	N/A	N/A	YES																									
FMH1004659	FMH1004658		5.38	180	Concrete pipe (Existing)	3.10	7.23	7.32	0.61	0.61	4.60	4.69	4.57	0.0003	2.54	5.65	0.45	N/A	0.65	the Site	283.92	1029.18	1313.10	113451.41	4201.90	1.00	1313.10	N/A	N/A	YES																									
FMH1004658	FMH1004657		36.36	180	Concrete pipe (Existing)	3.10	7.32	7.19	0.59	0.50	4.58	4.68	4.68	0.0007	2.54	5.65	0.45	1.03	0.65	the Site	283.92	1029.22	1313.14	113454.87	4202.03	1.00	1313.14	1663.06	79.0	YES																									
FMH1004657	FMH1004629		132.46	180	Concrete pipe (Existing)	3.10	7.19	7.20	0.59	0.50	4.58	4.68	4.68	0.0006	2.54	5.65	0.45	0.96	0.67	the Site	283.92	1169.64	1313.75	113507.57	4203.98	1.00	1313.75	2618.17	50.2	YES																									
FMH1004629	FMH1004030		135.21	180	Concrete pipe (Existing)	3.10	7.20	7.09	0.49	0.41	4.69	4.66	4.66	0.0006	2.54	5.65	0.45	0.96	0.67	the Site	283.92	1171.88	1453.56	125587.15	4651.58	1.00	1453.56	2442.70	59.5	YES																									
FMH1004030	FMH1004031		103.28	180	Concrete pipe (Existing)	3.10	7.09	5.00	0.39	0.36	4.68	2.62	2.62	0.0003	2.54	5.65	0.45	0.67	0.67	the Site	283.92	1171.88	1455.80	125780.69	4658.54	1.00	1455.80	1709.34	85.2	YES																									

1. Peaking factor (including stormwater allowance) is used for existing sewer. Peaking factor is 1 because the existing flow data from EPD has already included peaking factor.

2. Existing Sewer from FMH1004664 to FMH1004662 will be upgraded to 300 dia pipe

3. The assumption on the baseline upstream peak flow is based on EPD's data for the exact sewerage flow from the upstream of the FMH1004662.

4. The sewerage amount from the upstream of manhole FMH1004662 is based on the information from EPD



ICU Ref : HD(CU)S

LEGEND:

- SITE BOUNDARY
- EXISTING SEWER
- PROPOSED SEWER

NO	DESCRIPTION AND DATE	INITIAL AND DESIGNATION	DATE

wsp	
AUTHORISED	—/—
ENDORSED	—/—
CHECKED	—/—
DRAWN	—/—

AGREEMENT NO. CB 20210448

PROJECT
 Term Engineering Consultancy Services for New Territories East Region (2021-2023) - Instruction No. WP04 - Potential Public Housing at Po Shek Wu Road, Sheung Shui - Investigation

JOB NO. 2512243A

DRAWING TITLE
PROPOSED MITIGATION MEASURE

SCALE 1 : 1000 @ A3

DRAWING NO. WP04/SIA/003

HOUSING DEPARTMENT

DATE: _____

Appendix G

Sewerage Amount from the
Planning Development /
Applications (EPD's Information)

Appendix G - Sewerage Amount from the Planning Development / Applications (EPD's Information)

Planning Developments/ Applications	ADWF (m3/day)	Peak Flow (l/s)	Discharge Manhole
Public Housing Development at Ching Hui Road	628	43.3	FMH1025202
Community Health Centre Cum Social Welfare Facilities	237	22	FMH1003889
Expansion of North District Hospital	1892	110	FMH1003880
Residential Development at Lot no. 4076 in DD 91	610.9	42.4	FMH1003863
A/NE-KTS/460	2.2	0.2	FMH1029682
Y/NE-KTS/13	343	37.8	FMH1029683
Y/KTN/2	492	38	FMH1021543
A/KTS/506	2007	124	FMH1030384
A/NE-KTS/466	49	5	FMH1029681
A/NE-KTS/484	704	50	FMH1030364
Beas River Equestrian Centre	272	19	FMH1028616
Y/FSS/19	799	56	FMH1023220
Y/NE-KTS/14	1153	80	FMH1030367
Y/NE-KTS/17	291	20	FMH1030367
Total Sewerage Flow (m3/day)			
		9480.1	
Total Sewerage Flow (L/s) ⁽¹⁾			
		109.7	
Peaking Factor			
		2.4	
Total Sewerage Flow (L/s) ⁽¹⁾			
		263.3	

1. The peaking factors for the planning development will adopt 2.4