| | | Appendix | A |
|---------|--------|----------|----|
| Traffic | Impact | Assessme | nt |

Section 16 Planning Application for Proposed Hotel with Minor Relaxation of Plot Ratio and Building Height Restrictions at 201 and 203 Wai Yip Street, Kwun Tong, Kowloon

Traffic Impact Assessment Final Report August 2024

Prepared by: CKM Asia Limited

Section 16 Planning Application for Proposed Hotel with Minor Relaxation of Plot Ratio and Building Height Restrictions at 201 and 203 Wai Yip Street, Kwun Tong, Kowloon

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1.0 INTRODUCTION

Background

- 1.1 The Subject Site comprises of 2 existing buildings, i.e. the Siu Fu Factory Building at 201 Wai Yip Street, and the Tungtex Building at 203 Wai Yip Street (the "2 Existing Buildings"). Figure 1.1 shows the location of the Subject Site.
- 1.2 On 17th January 2020, the Town Planning Board ("TPB") approved the S16 Planning Application for Industrial Building at 203 Wai Yip Street (TPB ref: A/K14/778). On 4th March 2022, the Town Planning Board ("TPB") approved the S16 Planning Application for Commercial Building at 201 Wai Yip Street (TPB ref: A/K14/808).
- 1.3 The Applicant now intends to redevelop the 2 Existing Buildings into a hotel, with 20% increase in plot ratio, i.e., from the maximum permitted plot ratio of 12.0 to plot ratio of 14.4 (the "Proposed Redevelopment"). CKM Asia Limited, a traffic and transportation planning consultancy firm, was commissioned by the Applicant to prepare a Traffic Impact Assessment ("TIA") in support of the Proposed Redevelopment.

Scope of the Assessment

- 1.4 The main objectives of this TIA are as follows:
 - To assess the existing traffic issues in the vicinity of the Subject Site;
 - To quantify the amount of traffic generated by the Proposed Redevelopment; and
 - To examine the traffic impact on the local road network in the vicinity of the Subject Site.

Contents of the Report

1.5 After this introduction, the remaining chapters contain the following:

Chapter Two
 Chapter Three
 Chapter Four
 Chapter Five
 describes the existing situation;
 outlines the development proposal;
 presents the traffic impact analysis; and
 summarises the overall conclusion.

2.0 THE EXISTING SITUATION

The Subject Site

2.1 The Subject Site fronts onto Wai Yip Street to the south, the Wai Yip Street CLP Substation to the west and a rear lane to the north. The section of Wai Yip Street fronting the Subject Site is a dual carriageway 3-lane road. The run-in/out of the Tungtex Building is provided at Wai Yip Street.

Traffic Survey

- 2.2 To quantify the traffic flows at the junctions chosen for the conduct of capacity analysis, manual classified counts were undertaken on Friday, 15th March 2024 during the AM and PM peak periods. The location of the junctions and area of influence is presented in Figure 2.1 and their layout is shown in Figures 2.2 to 2.8.
- 2.3 The surveyed junctions include the following:
 - J1: Hung To Road / Hoi Yuen Road / Wai Yip Street;
 - J2: Wai Yip Street / Hoi Yuen Road;
 - J3: Hung To Road / Tsun Yip Street;
 - J4: Wai Yip Street / Tsun Yip Street;
 - J5: Wai Yip Street / How Ming Street;
 - J6: Kei Yip Street / Kei Yip Lane; and
 - J7: Wai Yip Street / Kei Yip Street.
- 2.4 In view that the junction of Tsun Yip Street / Hoi Bun Road is not a signal controlled or priority junction, the junction performance assessment is not conducted. The counts were classified by vehicle type to enable traffic flows in passenger car units ("pcu") to be calculated. From the survey, the AM and PM peak hours were found to be between 0845 0945 and 1730 1830 hours respectively.

Review of the Traffic Flows obtained from the Traffic Survey

2.5 The traffic flows obtained from the survey in March 2024 are adjusted based on the Annual Average Daily Traffic ("AADT") of station 3020 Wai Yip Street (from Lai Yip Street to Hoi Yuen Road) found in the Annual Traffic Census ("ATC"). The adjusted 2024 peak hour traffic flows are presented in Figure 2.9.

Operational Performance of the Key Junctions

2.6 The existing operational performance of the key junctions is calculated based on the observed traffic counts and the analysis is undertaken using the methods outlined in Volume 2 of Transport Planning and Design Manual ("TPDM"). The results of the existing operational performance of the junctions are summarised in Table 2.1 and the detailed calculations are found in Appendix 1.

TABLE 2.1 EXISTING JUNCTION OPERATIONAL PERFORMANCE

| Ref. | Junction | Type of Junction | Parameter ⁽¹⁾ | AM Peak Hour | PM Peak Hour |
|------|---|---------------------|--------------------------|-----------------|-----------------|
| J1 | Hung To Road / Hoi Yuen Road / Wai | Signal | RC | 87% | 90% |
| | Yip Street | | | | |
| J2 | Wai Yip Street / Hoi Yuen Road | Roundabout | RFC | 0.683 | 0.607 |
| J3 | Hung To Road / Tsun Yip Street ⁽²⁾ | Signal | RC | 52% | 89% |

| Ref. | Junction | Type of Junction | Parameter ⁽¹⁾ | AM Peak Hour | PM Peak Hour |
|------|---|--|--------------------------|-----------------|-----------------|
| J4 | Wai Yip Street / Tsun Yip Street ⁽²⁾ | Signal | RC | 78% | 97% |
| J5 | Wai Yip Street / How Ming Street(2) | Signal | RC | 79% | 87% |
| J6 | Kei Yip Street / Kei Yip Lane | Priority | RFC | 0.021 | 0.028 |
| J7 | Wai Yip Street / Kei Yip Street | Not a signal controlled or priority junction | | | nction |

Notes: (1) RC – Reserve Capacity

RFC - Ratio of Flow to Capacity

2.7 The results in Table 2.1 indicate that the junctions now operate with capacities during the AM and PM peak hours.

Pedestrian Facilities

2.8 Good pedestrian facilities provided in the vicinity of the Subject Site, including footpaths, and at-grade pedestrian crossings at the signalised road junctions.

Availability of Public Transport Facilities

2.9 The Subject Site is well-served by various public transport services, including franchised bus and green minibus ("GMB"), and these services operate mainly along Hoi Yuen Road, Wai Yip Street and Kwun Tong Road. The closest entrance to the MTR Kwun Tong Station is at Hoi Yuen Road, which is some 670 metres or 10 minutes' walk away. Details of the franchised bus and GMB routes operating in the vicinity of the Subject Site are presented in Figure 2.10 and Table 2.2.

TABLE 2.2 FRANCHISED BUS AND GMB SERVICES OPERATING CLOSE TO THE SUBJECT SITE

| | THE SUBJECT SHE | |
|---------|---|------------------------|
| Route | Routing | Frequency (minutes) |
| KMB 1A | Sau Mau Ping (Central) – Star Ferry | 5 – 15 |
| KMB 3D | Tsz Wan Shan (Central) – Kwun Tong (Yue Man Square) | 4 – 16 |
| KMB 5R | Kai Tak Cruise Terminal – Kwun Tong (apm) (Circular) | 30 |
| KMB 6P | Cheung Sha Wan (So Uk Estate) – Lei Yue Mun Estate | AM, PM Peak |
| KMB 11B | Kwun Tong (Tsui Ping Road) – Kowloon City Ferry | 10 – 25 |
| KMB 11C | Chuk Yuen Estate – Sau Mau Ping (Upper) | 15 – 25 |
| KMB 11D | Lok Fu – Kwun Tong Ferry | 15 – 30 |
| KMB 11X | On Tai (North) – Hung Hom Station | 10 – 25 |
| KMB 13D | Po Tat – Island Harbourview | 15 – 25 |
| KMB 13M | Kwun Tong (Elegance Road) – Po Tat (Circular) | 15 – 30 |
| KMB 13P | Po Tat – Cheung Sha Wan (Lai Kok Estate) | AM Peak |
| KMB 14 | Lei Yue Mun Estate – China Ferry Terminal | 12 – 25 |
| KMB 14B | Ngau Tau Kok – Lam Tin (Kwong Tin Estate) | 15 – 25 |
| KMB 14X | Yau Tong (Shung Tak Wai) – Tsim Sha Tsui (Circular) | 15 – 30 |
| KMB 15 | Ping Tin – Hung Hom (Hung Luen Road) | 12 – 20 |
| KMB 15A | Ping Tin – Tsz Wan Shan (North) | 20 – 30 |
| KMB 15X | Lam Tin (Kwong Tin Estate) – Hung Hom Station | AM, PM Peak |
| KMB 16 | Lam Tin (Kwong Tin Estate) – Mong Kok (Park Avenue) | 8 – 20 |
| KMB 16M | Kwun Tong (Yue Man Square) – Lam Tin (Hong Wah Court) | 15 – 30 |
| | (Circular) | |
| KMB 16P | Kwun Tong Ferry – Mong Kok (Park Avenue) | AM, PM Peak |
| KMB 17 | Kwun Tong (Yue Man Square) – Ho Man Tin (Oi Man Estate) | 5 – 20 |
| KMB 23 | Kwun Tong Ferry – Shun Lee (Circular) | 14 – 25 |
| KMB 23M | Lok Wah – Shun Lee (Circular) | 12 – 20 |
| KMB 28B | Choi Fook – Kai Tak (Kai Ching Estate) | 15 – 25 |
| KMB 33 | Tsuen Wan West Station – Yau Tong | 15 – 30 |

⁽²⁾ Kerbside on-street activities are reflected in the junction performance

| . | T | Tillal Report |
|----------|--|------------------------|
| Route | Routing | Frequency (minutes) |
| KMB 33B | Tsuen Wan West Station – Yau Tong | 20 – 25 |
| KMB 38 | Kwai Shing (East) – Ping Tin | 5 – 20 |
| KMB 38P | Kwai Shing (Central) – Ping Tin | AM Peak |
| KMB 40 | Tsuen Wan (Belvedere Garden) – Laguna City | 12 – 25 |
| KMB 40A | Ping Tin – Kwai Hing Station | AM, PM Peak |
| KMB 40B | Kwai Chung Estate – Ping Tin | AM Peak |
| KMB 40P | Kwun Tong Ferry – Tsuen Wan (Shek Wai Kok) | AM, PM Peak |
| KMB 42C | Tsing Yi (Cheung Hang Estate) – Lam Tin Station | 5 – 15 |
| KMB 49 | Ching Fu Court – Tseung Kwan O Industrial Estate | AM, PM Peak |
| KMB 62X | Tuen Mun Central – Lei Yue Mun Estate | 8 – 25 |
| KMB 62P | Tuen Mun Central – Lei Yue Mun Estate | 8 – 25 |
| KMB 69C | Tin Yan Estate – Kwun Tong Ferry | AM, PM Peak |
| KMB 74C | Kau Lung Hang – Kwun Tong Ferry | AM Peak |
| KMB 74D | Kau Lung Hang – Kwun Tong Ferry | 25 – 60 |
| KMB 74E | Tai Mei Tuk – Kwun Tong Ferry | AM, PM Peak |
| KMB 74F | Kwun Tong Ferry – Education University of Hong Kong | AM Peak |
| KMB 74P | Kwun Tong Ferry – Tai Po Central | AM Peak |
| KMB 74X | Tai Po Central – Kwun Tong Ferry | 3 – 15 |
| KMB 80 | Mei Lam – Kwun Tong Ferry | 5 – 20 |
| KMB 80A | Mei Lam – Kwun Tung Ferry | AM Peak |
| KMB 80P | Hin Keng – Kwun Tong Ferry | AM Peak |
| KMB 80X | Chun Shek – Kwun Tong Ferry | 8 – 25 |
| KMB 83A | Shui Chuen O – Kwun Tong Ferry | AM Peak |
| KMB 83X | Shui Chuen O – Kwun Tong Ferry | 8 – 30 |
| KMB 88X | Fo Tan Chung Yeung Estate – Ping Tin (Circular) | 20 – 30 |
| KMB 89 | Lek Yuen – Kwun Tong Station | 8 – 20 |
| KMB 89C | Heng On – Kwun Tong (Tsui Ping Road) | 12 – 30 |
| KMB 89D | Wu Kai Sha Station – Lam Tin Station | 3 – 20 |
| KMB 89P | Ma On Shan Town Centre – Lam Tin Station Bus Terminus | AM Peak |
| KMB 89X | Shatin Station – Kwun Tong (Tsui Ping Road) | 7 – 20 |
| KMB 93A | Po Lam – Kwun Tong Ferry | 20 – 25 |
| KMB 93K | Po Lam – Mong Kok East Station | 15 – 30 |
| KMB 95M | Tsui Lam – Kwun Tong Road (Elegance Road) | 20 – 30 |
| KMB 98 | Tseung Kwan O Industrial Estate – Ngau Tau Kok Station (Circular) | 15 – 20 |
| KMB 98A | Hang Hau (North) (Tseung Kwan O Hospital) – Ngau Tau Kok Station (Circular) | 8 – 20 |
| KMB 98B | Hang Hau (North) (Tseung Kwan O Hospital) – Kwun Tong Station | AM Peak |
| KMB 213B | On Tai – Ting Fu Street (Circular) | AM Peak |
| KMB 215P | Lam Tin (Kwong Tin Estate) – Kowloon Station | AM Peak |
| KMB 215X | Lam Tin (Kwong Tin Estate) – Kowloon Station | 5 – 20 |
| KMB 234C | Sham Tseng – Kwun Tong Station | AM, PM Peak |
| KMB 234D | Tsing Lung Tau – Kwun Tong Station | AM, PM Peak |
| KMB 252X | Handsome Court – Lam Tin Station | AM, PM Peak |
| KMB 258A | Hung Shui Kiu (Hung Fuk Estate) – Lam Tin Station | AM Peak |
| KMB 258D | Tuen Mun (Po Tin Estate) – Lam Tin Station | 5 – 20 |
| KMB 258P | Hung Shui Kiu (Hung Fuk Estate) – Lam Tin Station | AM, PM Peak |
| KMB 258S | Tuen Mun (Shan King Estate) – Lam Tin Station | AM Peak |
| KMB 258X | Tuen Mun (Po Tin Estate) – Kwun Tong Ferry | AM, PM Peak |
| KMB 259D | Tuen Mun (Lung Mun Oasis) – Lei Yue Mun Estate | 7 – 25 |
| KMB 259S | Tuen Mun (Lung Mun Oasis) – Kwun Tong Ferry | AM Peak |
| KMB 259X | Lung Mun Oasis – Kwun Tong Ferry | AM, PM Peak |
| KMB 267X | Tuen Mun (Siu Hong Court) – Lam Tin Station | AM, PM Peak |
| KMB 268A | Long Ping Estate – Kwun Tong Ferry | AM, PM Peak |
| KMB 268C | Long Ping Station – Kwun Tong Ferry | 5 – 20 |
| 2000 | 1 == ····g · ····g · ····g · ····g | |

| Route | Routing | Frequency (minutes) |
|--------------------|---|------------------------|
| KMB 268P | Ma Wang Road (Shan Shui House) – Kwun Tong Ferry Kwun Tong Ferry – Long Ping Station | AM, PM Peak |
| KMB 269C | Tin Shui Wai Town Centre – Kwun Tong Ferry | 5 – 20 |
| KMB 269S | Tin Shui Wai Town Centre – Kwun Tong Ferry | AM, PM Peak |
| KMB 274X | Kwun Tong Ferry – Tai Po Central | PM Peak |
| KMB 277A | Sha Tau Kok – Lam Tin Station | AM, PM Peak |
| KMB 277E | Lam Tin Station – Sheung Shui (Tin Ping) | 15 – 30 |
| KMB 277P | Sheung Shui (Tin Ping) – Lam Tin Station | AM, PM Peak |
| KMB 277X | Fanling (Luen Wo Hui) – Lam Tin Station | 5 – 30 |
| KMB 292P | Sai Kung – Kwun Tong | AM Peak |
| KMB 296A | Sheung Tak – Ngau Tau Kok Station (Circular) | 7 – 15 |
| KMB 296C | Sheung Tak – Cheung Sha Wan (Hoi Ying Estate) | 15 – 30 |
| KMB N3D | Kwun Tong (Yue Man Square) – Tsz Wan Shan (Central) | Overnight |
| KMB N293 | Sheung Yak – Mong Kok East Station | Overnight |
| KMB T74 | Tai Po (Tai Wo) – Kwun Tong Ferry | AM Peak |
| KMB T277 | Sheung Shui – Lam Tin Station | AM, PM Peak |
| KMB W2 | Jordan (West Kowloon Station) – Kwun Tong (Circular) | 30 – 60 |
| KMB X42C | Tsing Yi (Cheung Hang Estate) – Yau Tong | 7 – 30 |
| KMB X42P | Tsing Yi (Cheung On Estate) – Lam Tin Station | AM Peak |
| KMB X89D | Nai Chung – Kwun Tong Ferry | AM, PM Peak |
| KMB/CTB 101 | Kwun Tong (Yue Man Square) – Kennedy Town | 6 – 20 |
| KMB/CTB 606 | Siu Sai Wan (Island Resort) – Choi Wan (Fung Shing Street) | 20 – 25 |
| KMB/CTB 606A | Shau Kei Wan (Yiu Tung Estate) – Choi Wan (Fung Shing Street) | AM Peak |
| KMB/CTB 606X | Siu Sai Wan (Island Resort) – Kowloon Bay | AM, PM Peak |
| KMB/CTB 619 | Shun Lee – Central (Macau Ferry) | 4 – 25 |
| KMB/CTB 619P | Shun Lee – Central (Macau Ferry) | AM Peak |
| KMB/CTB 641 | Kai Tak (Kai Ching Estate) – Central (Macau Ferry) | AM, PM Peak |
| KMB/CTB 671 | Diamond Hill Station – Ap Lei Chau Lee Lok Street | 15 – 45 |
| KMB/CTB 671X | Ap Lei Chau Lee Lok Street – Diamond Hill Station | AM Peak |
| KMB/CTB N619 | Shun Lee – Central (Macau Ferry) | Overnight |
| CTB 55 | Ching Tin and Wo Tin – Kwun Tong Ferry Pier | AM, PM Peak |
| CTB 61R | Lam Tin Station – City One Shatin | 12 – 20 |
| CTB 78C | Queen's Hill Fanling – Kai Tak | AM, PM Peak |
| CTB 78P | Queen's Hill Fanling – Kwun Tong | AM Peak |
| CTB 78X | Queen's Hill Fanling – Kai Tak | 30 – 60 |
| CTB 796S | Tseung Kwan O Station – Ngau Tau Kok Station (Circular) | Overnight |
| CTB 797 CTB A22 | Lohas Park – Kowloon Bay (Circular) Lam Tin Station – Airport | 15 – 20 |
| CTB A29 | Tseung Kwan O (Po Lam) – Airport / HZMB Hong Kong Port | 15 – 40 20 – 60 |
| CTB E22 | Lam Tin (North) – AsiaWorld-Expo | 8 – 20 |
| CTB E22A | Hong Sing Garden – AsiaWorld-Expo | 25 – 30 |
| CTB E22C | Tiu Keng Leng Station – Aircraft Maintenance Area | AM, PM Peak |
| CTB E22S | Tung Chung (Mun Tung Estate) – Tseung Kwan O (Po Lam) | AM, PM Peak |
| CTB E22X | Yau Tong – AsiaWorld-Expo | AM, PM Peak |
| CTB N29 | Hong Sing Garden – Tung Chung Station | Overnight |
| CTB N796 | Lohas Park / Tseung Kwan O Station – Mongkok | Overnight |
| CTB NA29 | Tseung Kwan O (Po Lam) – Airport / HZMB Hong Kong Port | Overnight |
| GMB 22A | Lok Wah Estate – Cheung Yip Street / Kwun Tong Ferry Pier (Circular) | 20 |
| GMB 35 | Choi Ha Estate – Hong Lee Court | 5 – 7 |
| GMB 62S | Kwong Tin Estate – Tsim Sha Tsui (Haiphong Road) | Overnight |
| GMB 90A | Yau Lai Estate – HK Children's Hospital | 20 |
| GMB 90B | Sau Mau Ping Estate Phase 5 – HK Children's Hospital | 15 – 20 |
| GMB 102 | Hang Hau Station – San Po Kong (Hong Keung Street) | 2 – 15 |
| GMB 102B | Hang Hau (Yuk Ming Court) – Choi Hung | 12 – 20 |
| GMB 102S | Hang Hau Station – San Po Kong (Hong Keung Street) | Overnight |

| Route | Routing | Frequency (minutes) |
|----------|--|------------------------|
| GMB 103 | Clear Water Bay – Kwun Tong Ferry | 10 – 15 |
| GMB 104 | HKUST – Ngau Tau Kok Station | 12 – 25 |
| GMB 106 | Tseung Kwan O (Po Lam) – Kowloon Bay (Enterprise Square) | 7 – 25 |
| GMB 501S | Sheung Shui Station – Kwun Tong (Yue Man Square) | Overnight |

Note: KMB – Kowloon Motor Bus CTB – Citybus GMB – Green Minibus

3.0 THE PROPOSED REDEVELOPMENT

Development Schedule

3.1 The Proposed Redevelopment is a Hotel with 448 guest rooms and 1,232.237m² GFA of conference or banqueting facilities.

Provision of Internal Transport Facilities

3.2 A comparison of the internal transport facilities recommended by the Hong Kong Planning Standards and Guidelines ("HKPSG") and the internal transport facilities provided are presented in **Table 3.1**.

TABLE 3.1 COMPARISONS OF THE INTERNAL TRANSPORT FACILITIES FOR THE PROPOSED REDEVELOPMENT

| TOR THE FROM OBLD REDEVILLO | I |
|---|--|
| HKPSG Recommendation for a Hotel with (i) 448 guest rooms, (ii) 1,232.237m² GFA conference and banquet facilities | Proposed Provision |
| Car Parking Space (i) 1 car parking space per 100 rooms. 448 / 100 = 4.5, say 5 nos. (ii) 0.5-1 car space per 200m² GFA of conference and banquet facilities | 9 nos. including (i) 8 nos. @ 5m (L) x 2.5m (W) x 2.4m (H), (ii) 1 no. @ 5m (L) x 3.5m (W) x 2.4m (H) for persons with |
| Minimum = 1,232.237 / 200 x 0.5 = 3.1, say $\frac{4 \text{ nos.}}{1 \text{ nos.}}$ Maximum = 1,232.237 / 200 x 1 = 6.2, say $\frac{7 \text{ nos.}}{1 \text{ nos.}}$ $\frac{\text{Total [(i) + (ii)]}}{\text{Minimum}} = 5 + 4 = \frac{9 \text{ nos.}}{12 \text{ nos.}}$ Maximum = 5 + 7 = $\frac{12 \text{ nos.}}{12 \text{ nos.}}$ | disabilities = HKPSG recommendation |
| Motorcycle Parking Space 5 to 10% of the total provision for private cars Minimum = 9 x 5% = 0.5, say 1 no. Maximum = 9 x 10% = 0.9, say 1 no. | 1 no. @ 2.4m (L) x 1m (W) x 2.4m (H) = HKPSG recommendation |
| Taxi and Private Car Layby Minimum 3 lay-by for taxis and private cars for 300-599 rooms = 3 nos. | 3 nos. @ 5m (L) x 2.5m (W) x 2.4m (H) = HKPSG recommendation |
| Single-Deck Tour Bus Layby Minimum 2-3 lay-by for single-deck tour buses for 300-899 rooms = 2-3 nos. | 3 nos. @ 12m (L) x 3.5m (W) x 3.8m (H) = HKPSG recommendation |
| Goods Vehicle Loading / Unloading Bay 0.5 - 1 goods vehicle bay per 100 rooms Minimum = 448 / 100 x 0.5 = 2.2, say 3 nos. Maximum = 448 / 100 x 1 = 4.5, say 5 nos. | 2 nos. @ 7m (L) x 3.5m (W) x 3.6m (H) for Light Goods Vehicles, plus 1 no. @ 11m (L) x 3.5m (W) x 4.7m (H) for Heavy Goods Vehicles = HKPSG recommendation |

3.3 **Table 3.1** shows that the internal transport facilities provided agree with the recommendations of the HKPSG. The carpark layout plans for G/F and B1/F are shown in **Figures 3.1 – 3.2**.

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Swept Path Analysis

The CAD-based swept path analysis program, Autodesk Vehicle Tracking, was used to check the ease of vehicle manoeuvring, and the swept path analysis drawings for critical movements are found in Appendix 2. Vehicles are found to have no manoeuvring problems and all vehicles could enter and leave the spaces with ease.

4.0 TRAFFIC IMPACT

Design Year

4.1 The Proposed Redevelopment is expected to be completed by 2029, and the design year adopted for the capacity analysis is 2032, i.e. 3 years after the completion of the development.

Traffic Forecasting

4.2 The 2032 traffic flows used for the junction analysis are produced with reference to: (i) 2031 traffic flows from the Base District Traffic Model ("BDTM"); (ii) estimated traffic growth from 2031 to 2032; (iii) the planned developments in the vicinity of the Proposed Redevelopment, and (iv) additional traffic generated by the Proposed Redevelopment.

Estimated Traffic Growth Rate from 2031 to 2032

Reference is made to the 2019 – based Territorial Population and Employment Data Matrix ("TPEDM") data produced by Planning Department for Kwun Tong District, which are for 2019, 2026 and 2031 and are presented in Table 4.1.

TABLE 4.1 2019-BASED TPEDM DATA PRODUCED BY PLANNING DEPARTMENT FOR KWUN TONG DISTRICT

| Item | TPEDM Estimation / Projection | | |
|------------------|--|---------------------------|------------------|
| | 2019 | 2026 | 2031 |
| Population | 693,900 | 769,400 | 741,300 |
| Employment | 395,350 | 410,550 | 408,250 |
| <u>Total</u> | <u>1,089,250</u> | <u>1,179,950</u> | <u>1,149,550</u> |
| Average Growth % | From 2019 to 2026: +1.15% From 2019 to 2031: +0.45% | From 2026 to 2031: -0.52% | N/A |

4.4 Table 4.1 shows that the highest average annual growth rate is 1.15%. In view that there is no estimation beyond 2031 and to err on the high side, the growth rate of 1.15% per annum is adopted for the traffic growth between 2031 and 2032.

Planned Developments in the Vicinity of the Proposed Redevelopment

The planned developments included in the 2032 reference traffic flows are presented in Table 4.2.

TABLE 4.2 PLANNED DEVELOPMENTS IN THE VICINITY OF THE PROPOSED REDEVELOPMENT

| Site | Diagning Application No. / Diag No. | Address | | | |
|------|-------------------------------------|---|--|--|--|
| Site | Planning Application No. / Plan No. | 1 | | | |
| 1 | A/K14/763 | 350 Kwun Tong Road | | | |
| 2 | A/K14/766 | 41 King Yip Street | | | |
| 3 | A/K14/771 | 32 Hung To Road | | | |
| 4 | A/K14/773 | 82 Hung To Road | | | |
| 5 | A/K14/774 | 7 Lai Yip Street | | | |
| 6 | A/K14/775 | 132 Wai Yip Street | | | |
| 7 | A/K14/777 | 71 How Ming Street | | | |
| 8 | A/K14/780 | 107-109 Wai Yip Street | | | |
| 9 | A/K14/782 | 4 Tai Yip Street | | | |
| 10 | A/K14/787 | 33 Hung To Road | | | |
| 11 | A/K14/796 | 28A Hung To Road | | | |

| Site | Planning Application No. / Plan No. | Address |
|------|--|---|
| 12 | A/K14/804 | 334 -336 and 338 Kwun Tong Road |
| 13 | A/K14/806 | 11 Lai Yip Street |
| 14 | A/K14/807 | Kun Tong Inland Lots 1 S.A , 1 RP, 3 and 15 |
| 15 | A/K14/809 | 1 Tai Yip Street and 111 Wai Yip Street |
| 16 | A/K14/810 | 5 Lai Yip Street |
| 17 | A/K14/820 | 73 – 75 Hung To Road |
| 18 | A/K14/822 | 25 Tai Yip Street, Kwun Tong |
| 19 | S/K14S/URA1/3 Urban Renewal | Areas 4 and 5 of Kwun Tong Town Centre |
| | Authority's (URA) latest 'Vertical City' | |
| | scheme of a mixed use development | |
| 20 | N/A | EKEO Lai Yip Street Development |
| 21 | N/A | Kwun Tong Action Area |
| 22 | N/A | Kowloon Bay Action Area |

- 4.6 The infrastructure and road network included in the BDTM are as follows:
 - Kai Tak Development
 - Tseung Kwan O Lam Tin Tunnel
 - Central Kowloon Route
 - Trunk Road T2 between Central Kowloon Route and Tseung Kwan O Lam Tin Tunnel

Traffic Generated by the Proposed Redevelopment

- 4.7 The trip rates found in the TPDM are not used because none of the surveyed hotels are located in Business Areas. Hence, the traffic generated by the Proposed Redevelopment is estimated based trip generation rates of surveyed hotels in Business Areas including the following:
 - (i) 254-room Nina Hotel Kowloon East at 38 Chong Yip St, Kwun Tong
 - (ii) 298-room Tuen Mun Pentahotel at 6 Tsun Wen Road, Tuen Mun
- 4.8 The adopted trip generation rates and the calculated traffic generation associated with the Proposed Redevelopment are presented in Table 4.3.

TABLE 4.3 TRAFFIC GENERATION OF THE PROPOSED REDEVELOPMENT

| Item | AM Peak Hour | | | PM Peak Hour | | | | |
|---|--------------|--------|-----------|--------------|--------|-------|--|--|
| | In | Out | 2-way | In | Out | 2-way | | |
| Trip Generation Rates for hotel (pcu/hour/guest room) | | | | | | | | |
| In-house trip generation for hotel | 0.0591 | 0.0433 | NA | 0.0512 | 0.0472 | NA | | |
| Traffic Generation of Proposed Redevelopment (pcu/hour) | | | | | | | | |
| 448 guest rooms | 27 | 20 | <u>47</u> | 23 | 22 | 45 | | |

4.9 Table 4.3 shows the Proposed Redevelopment generates 47 and 45 more pcu (2-way) during the AM and PM peak hours respectively.

Comparison of Traffic Generation between the Approved S16 Scheme and the Proposed Redevelopment

4.10 The traffic generated by the Proposed Redevelopment is compared with the traffic generated by the Approved S16 Scheme at 201 and 203 Wai Yip Street, and is presented in Table 4.4.

TABLE 4.4 COMPARISON OF TRAFFIC GENERATION BETWEEN THE PROPOSED REDEVELOPMENT AND THE APPROVED \$16 SCHEME

| Scheme | Traffic Generation (pcu/hour) | | | | | | |
|---|-------------------------------|------------|------------|--------------|------------|------------|--|
| | AM Peak Hour | | | PM Peak Hour | | | |
| | In | Out | 2-way | In | Out | 2-way | |
| Approved S16 Scheme at 203 Wai Yip Street (TPB ref: A/K14/778) | 19 | 13 | 32 | 15 | 19 | 34 | |
| Approved S16 Scheme at 201 Wai Yip Street (TPB ref: A/K14/808) | 35 | 25 | 60 | 20 | 25 | 45 | |
| Total [A] | <u>54</u> | 38 | <u>92</u> | <u>35</u> | 44 | <u>79</u> | |
| Proposed Redevelopment [B] | <u>27</u> | <u>20</u> | <u>47</u> | <u>23</u> | <u>22</u> | <u>45</u> | |
| Difference [B] – [A] | <u>-27</u> | <u>-18</u> | <u>-45</u> | <u>-12</u> | <u>-22</u> | <u>-34</u> | |

- 4.11 Table 4.4 shows that compared with the Approved S16 Scheme at 201 and 203 Wai Yip Street, the Proposed Redevelopment generates 45 pcu and 34 pcu (2-way) less during the AM and PM peak hours, respectively. Hence, the Proposed Redevelopment is a better-off scheme.
- 4.12 Planned Traffic Improvement in the Vicinity of the Proposed Redevelopment
 The planned improvement schemes in the vicinity of the Proposed Redevelopment are summarized in Table 4.5.

TABLE 4.5 PLANNED TRAFFIC IMPROVEMENT SCHEMES IN THE VICINITY OF THE PROPOSED REDEVELOPMENT

| | Junction | Description of the Works | Indicative Layout | Source | Assumed Completion Year |
|----|------------------|--------------------------|----------------------|----------|----------------------------|
| J2 | Wai Yip Street / | Modification of Wai Yip | Please refer to | Kwun | Before 2032 |
| | Hoi Yuen Road | Street / Hoi Yuen Road | Appendix 3 | Tong | |
| | | roundabout into a signal | | District | |
| | | controlled junction | | Council | |
| J6 | Kei Yip Street / | Change Kei Yip Lane | | | |
| | Kei Yip Lane | from 2-way to 1-way | | | |
| J7 | Wai Yip Street / | Change to 2-way | | | |
| | Kei Yip Street | direction | | | |

2032 Traffic Flows

4.13 Year 2032 traffic flows for the following cases are derived:

2032 without the Proposed

Redevelopment [A]

= 2031 traffic flows derived with reference to BDTM + estimated total growth from 2031 to 2032+ traffic generated by the planned developments in the vicinity

of the Proposed Redevelopment

2032 with the Proposed

= [A] + traffic generated by the Proposed

Redevelopment (Table 4.3)

Redevelopment [B]

4.14 The 2032 peak hour traffic flows for the cases without and with the Proposed Redevelopment, are shown in Figures 4.1 - 4.2, respectively. The ingress / egress route for traffic generated by the Proposed Redevelopment are shown in Figures 4.3.

2032 Junction Operational Performance

4.15 Year 2032 capacity analysis for the cases without and with the Proposed Redevelopment are summarized in Table 4.6 and detailed calculations are found in the Appendix 1.

TABLE 4.6 2032 JUNCTION OPERATIONAL PERFORMANCE

| Ref. | Junction | Type of Junction / Parameter ⁽¹⁾ | Without the Proposed Redevelopment | | With the Proposed Redevelopment | |
|------|---|---|--|-------|---------------------------------------|-------|
| | | | AM | PM | AM | PM |
| | | | Peak | Peak | Peak | Peak |
| J1 | Hung To Road / Hoi Yuen Road / | Signal / RC | 57% | 70% | 57% | 70% |
| | Wai Yip Street | | | | | |
| J2 | Wai Yip Street / Hoi Yuen Road (3) | Signal / RC | 20% | 32% | 20% | 32% |
| J3 | Hung To Road / Tsun Yip Street ⁽²⁾ | Signal / RC | 18% | 37% | 18% | 37% |
| J4 | Wai Yip Street / Tsun Yip Street ⁽²⁾ | Signal / RC | 41% | 49% | 39% | 49% |
| J5 | Wai Yip Street / How Ming Street ⁽²⁾ | Signal / RC | 39% | 55% | 38% | 55% |
| J6 | Kei Yip Street / Kei Yip Lane(3) | Priority - RFC | 0.661 | 0.705 | 0.665 | 0.708 |
| J7 | Wai Yip Street / Kei Yip Street(3) | Priority - RFC | 0.442 | 0.302 | 0.448 | 0.309 |

Notes: (1) RC – Reserve Capacity RFC – Ratio of Flow to Capacity

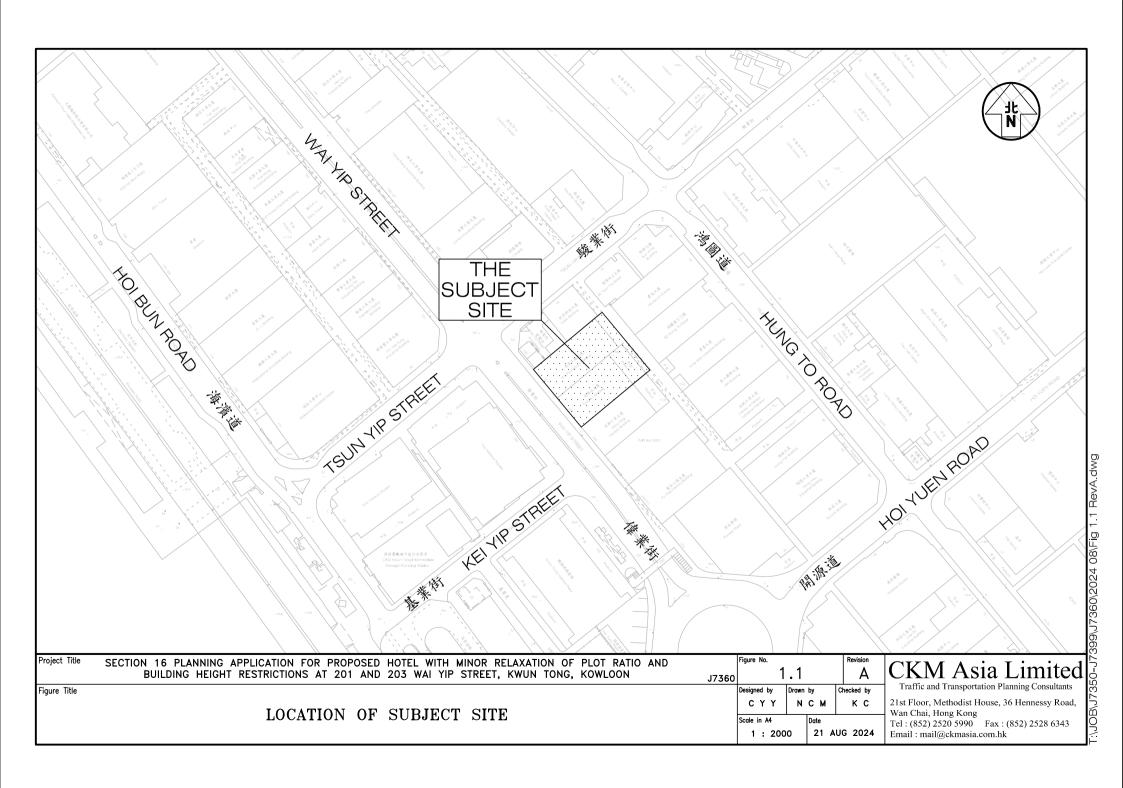
4.16 Table 4.6 shows that the key junctions operate with capacities during the AM and PM peak hours for the cases without and with the Proposed Redevelopment.

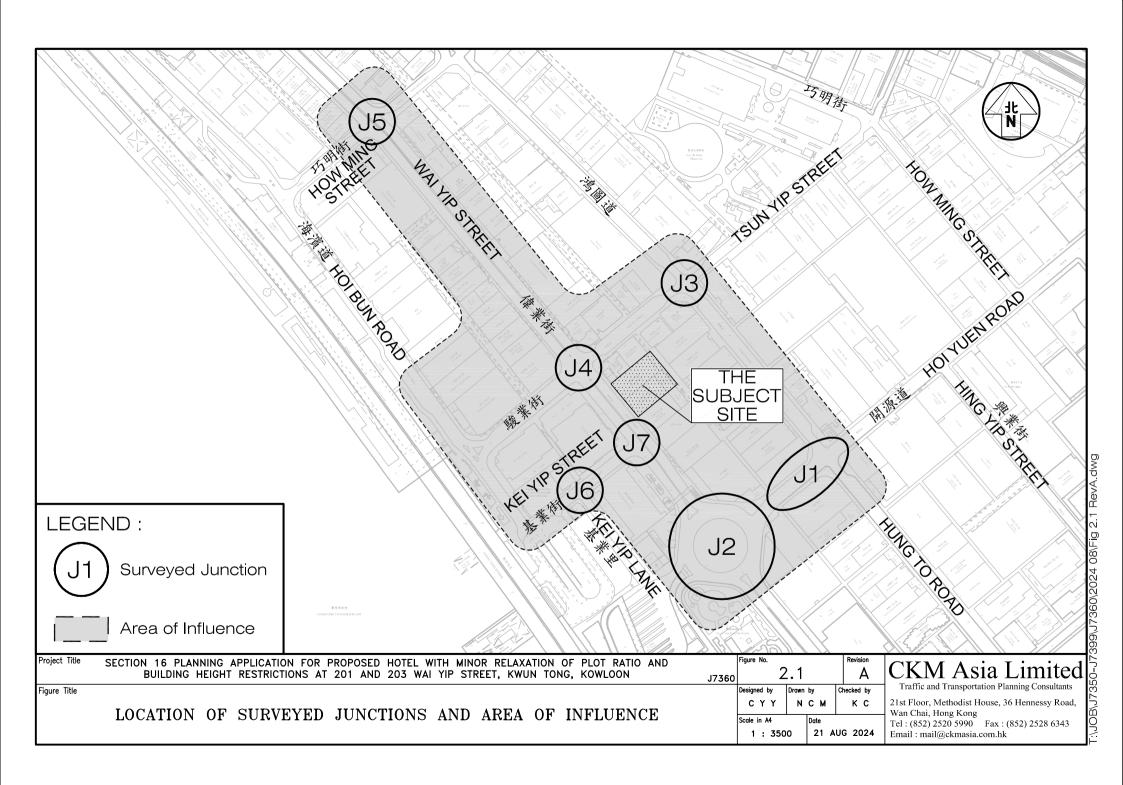
⁽²⁾ Kerbside on-street activities are reflected in the junction performance

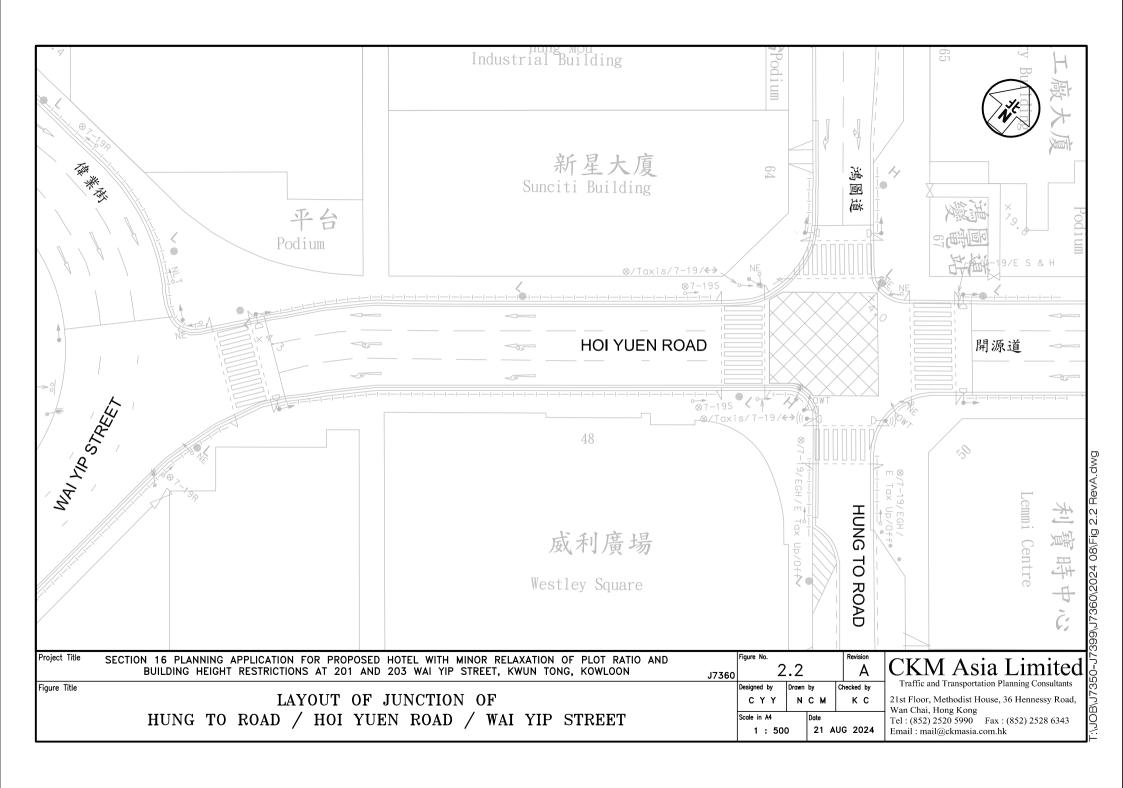
⁽³⁾ Junction Improvement Scheme by other project has been incorporated in the Assessment as explained in Table 4.5

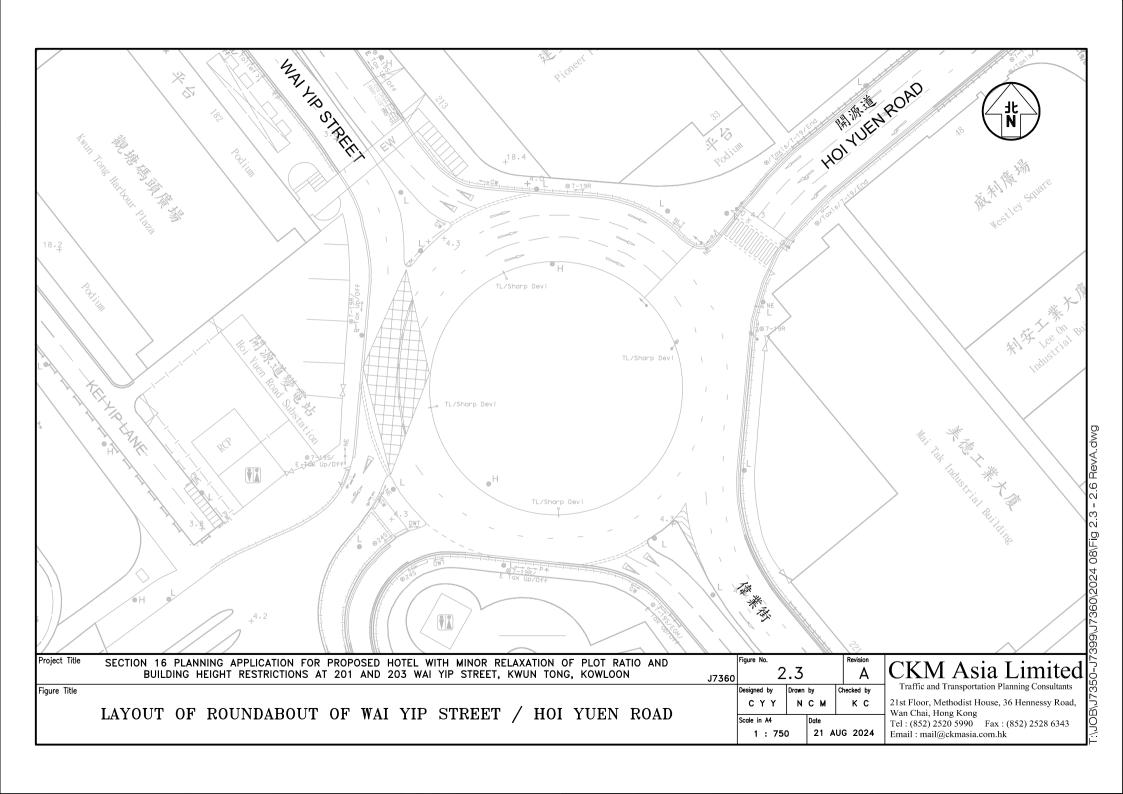
5.0 CONCLUSION

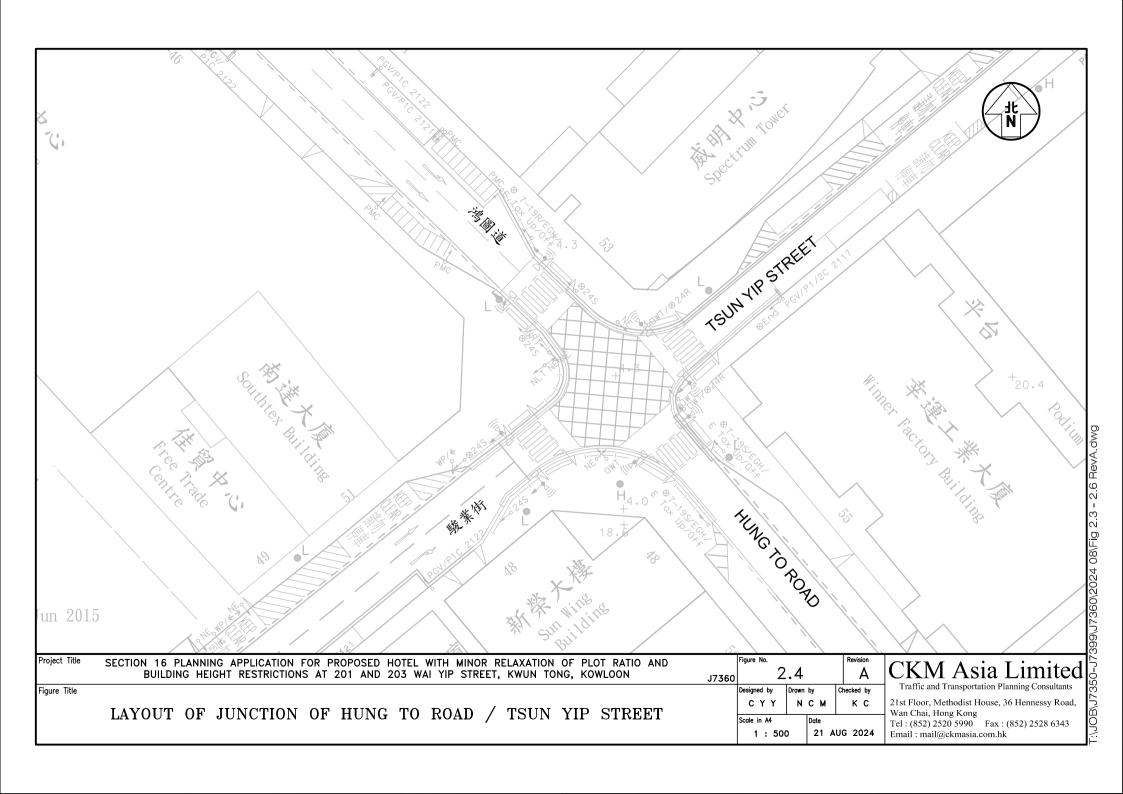
- 5.1 The Subject Site is located at 201 and 203 Wai Yip Street in Kwun Tong. It is currently occupied by the Siu Fu Factory Building and the Tungtex Building.
- 5.2 The Applicant intends to redevelop the 2 Existing Buildings into a hotel with 448 quest rooms and 1,232.237m² GFA of conference or banqueting facilities.
- 5.3 Manual classified counts were conducted at junctions located in the vicinity of the Proposed Redevelopment in order to establish the peak hour traffic flows. Currently, the junctions were found to operate with capacities during the AM and PM peak hours.
- 5.4 The Proposed Redevelopment run-in/out is provided at Wai Yip Street. The internal transport facilities provided comply with recommendations of the HKPSG.
- 5.5 The Proposed Redevelopment is expected to be completed by 2029, and the junction capacity analysis is undertaken for year 2032. For the design year 2032, the junctions analysed are expected to operate with capacities during the peak hours for the case without and with Proposed Redevelopment.
- 5.6 It is concluded that the Proposed Redevelopment will result in <u>no</u> adverse traffic impact to the surrounding road network. From traffic engineering grounds, the Proposed Redevelopment is acceptable.

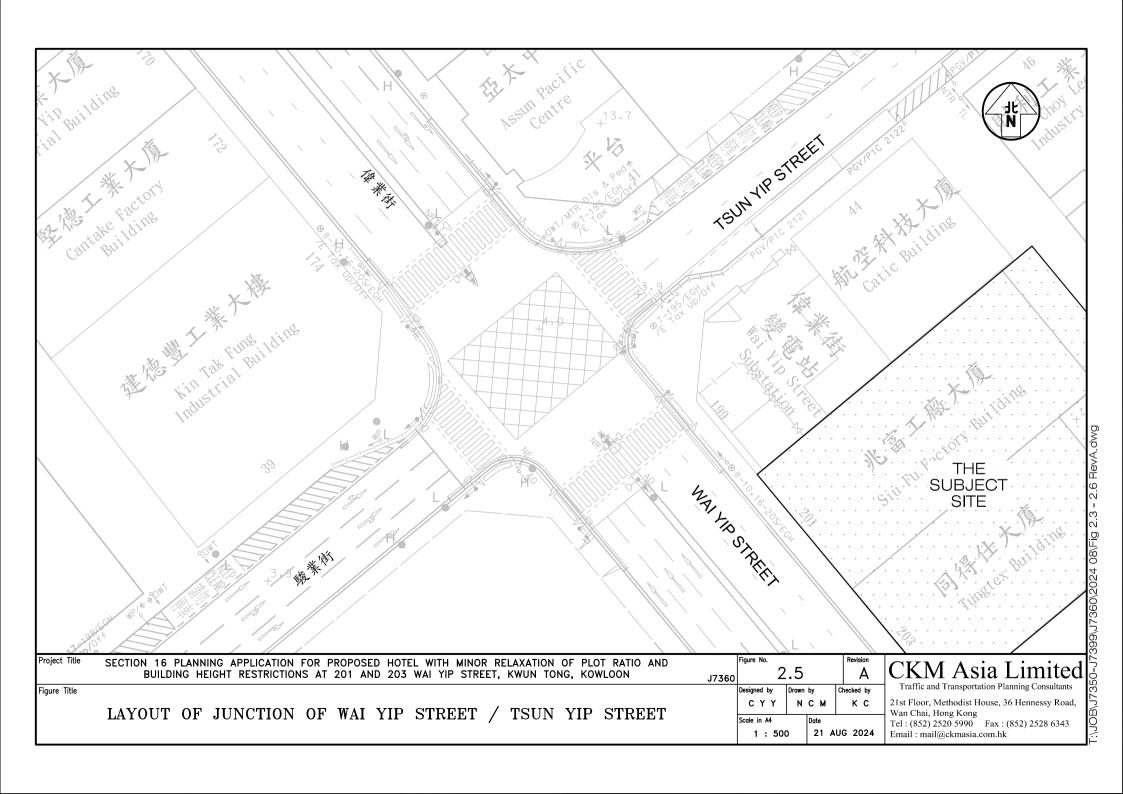


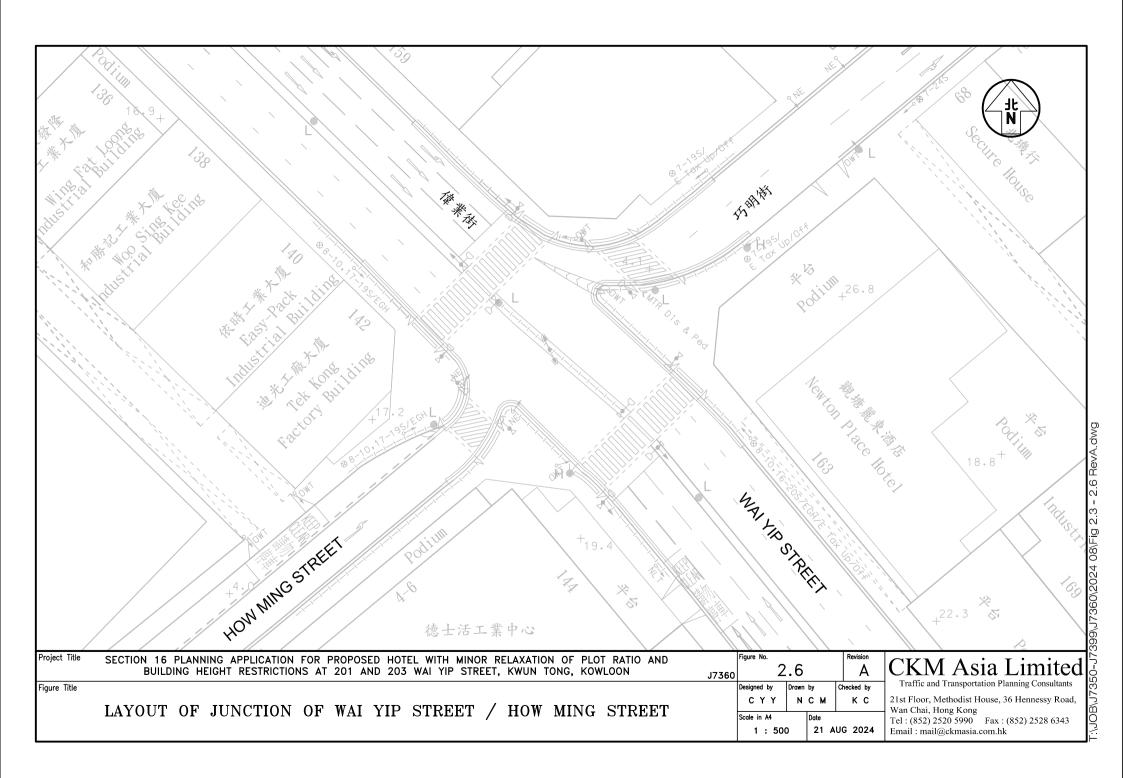


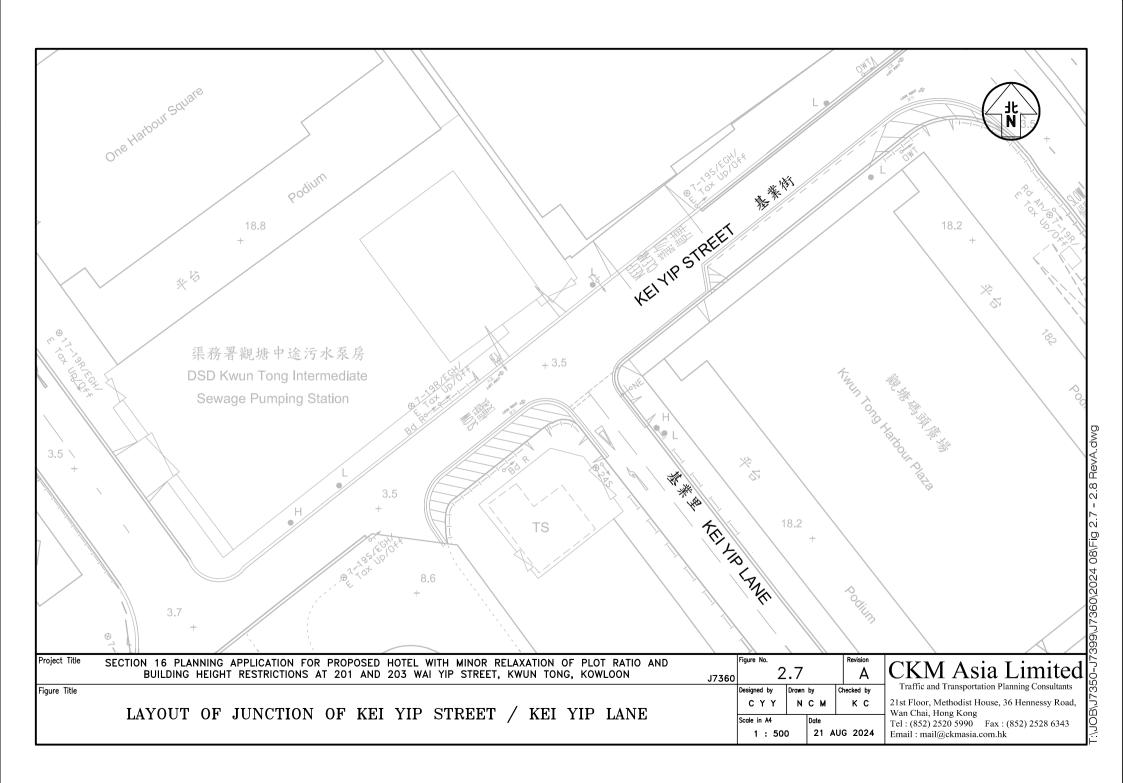


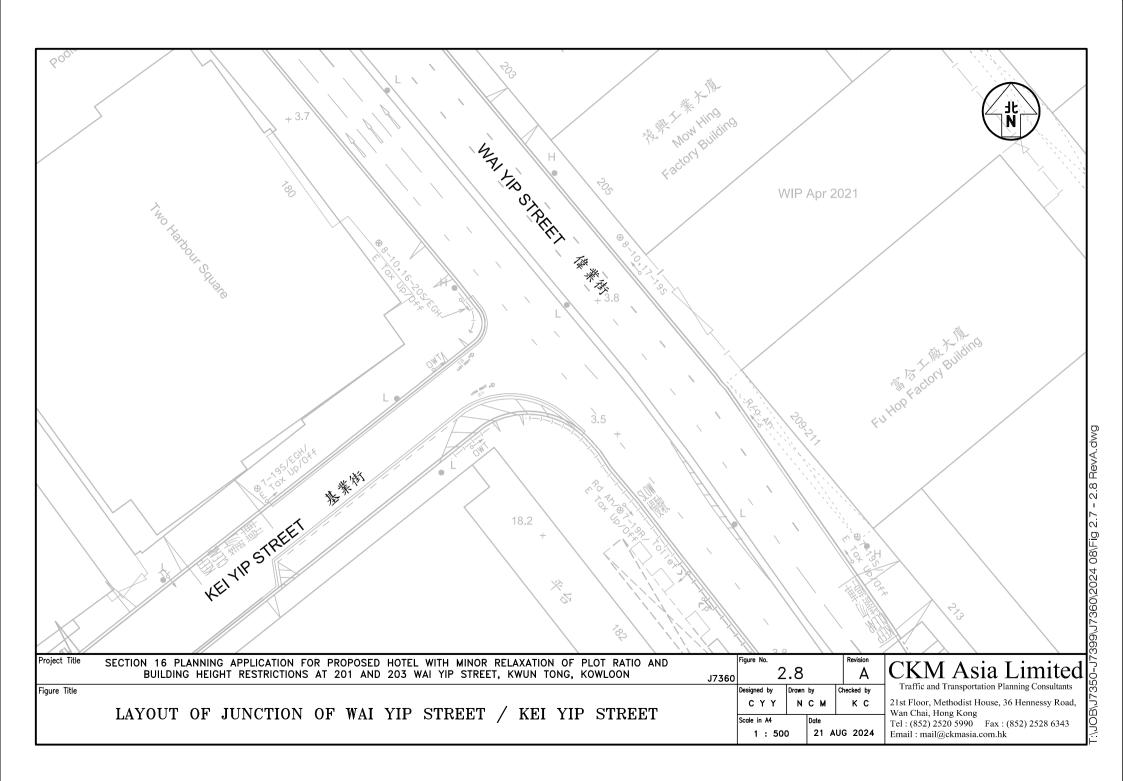


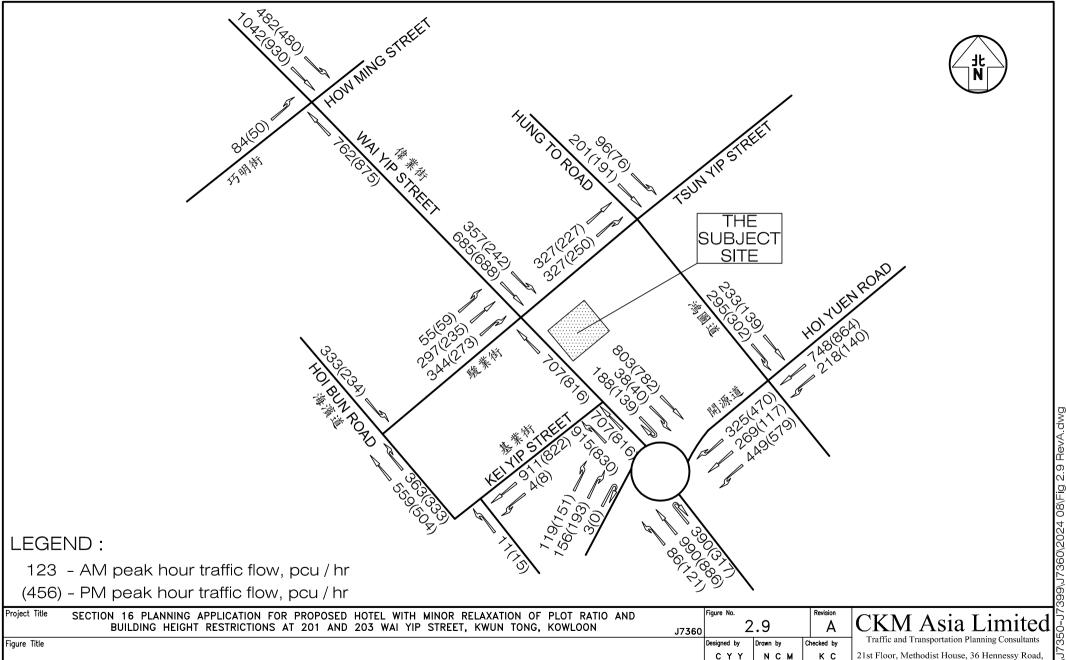












ADJUSTED 2024 PEAK HOUR TRAFFIC FLOWS

Tel: (852) 2520 5990 Fax: (852) 2528 6343

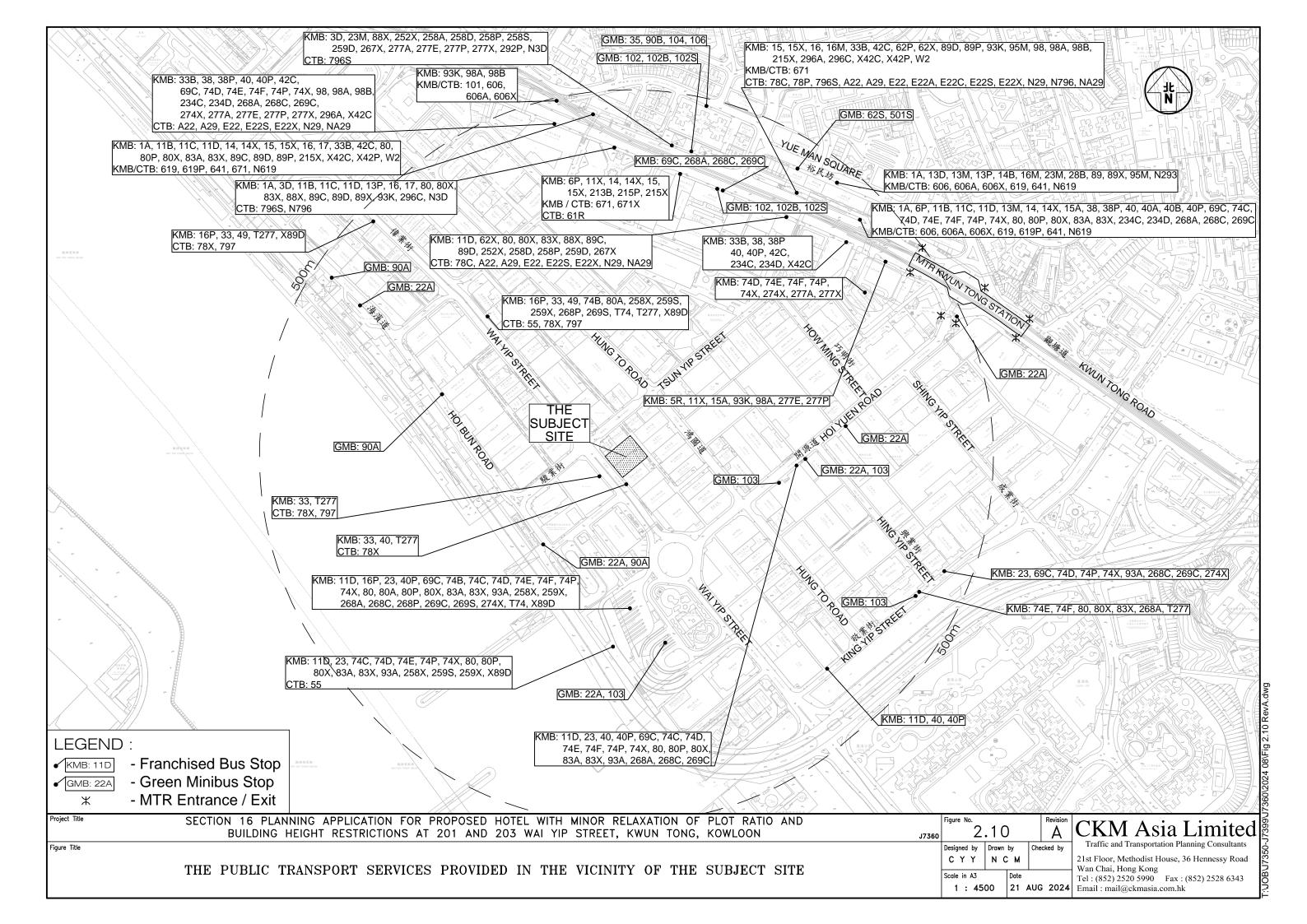
Wan Chai, Hong Kong

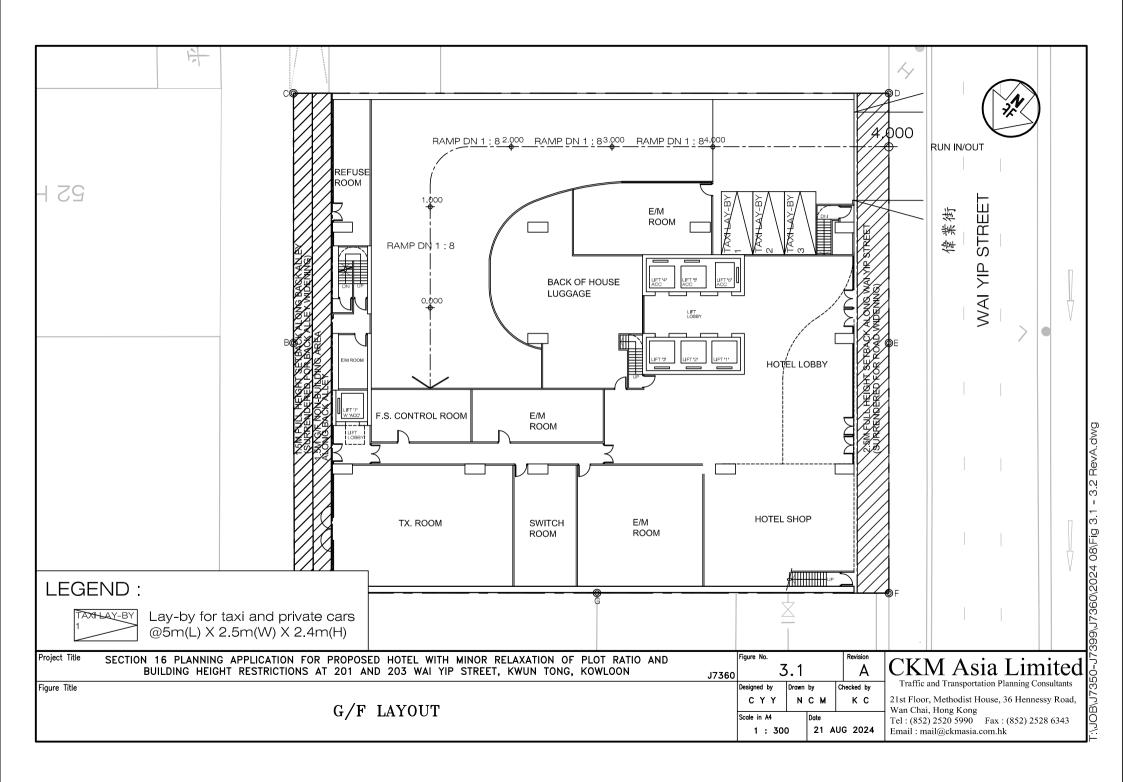
Email: mail@ckmasia.com.hk

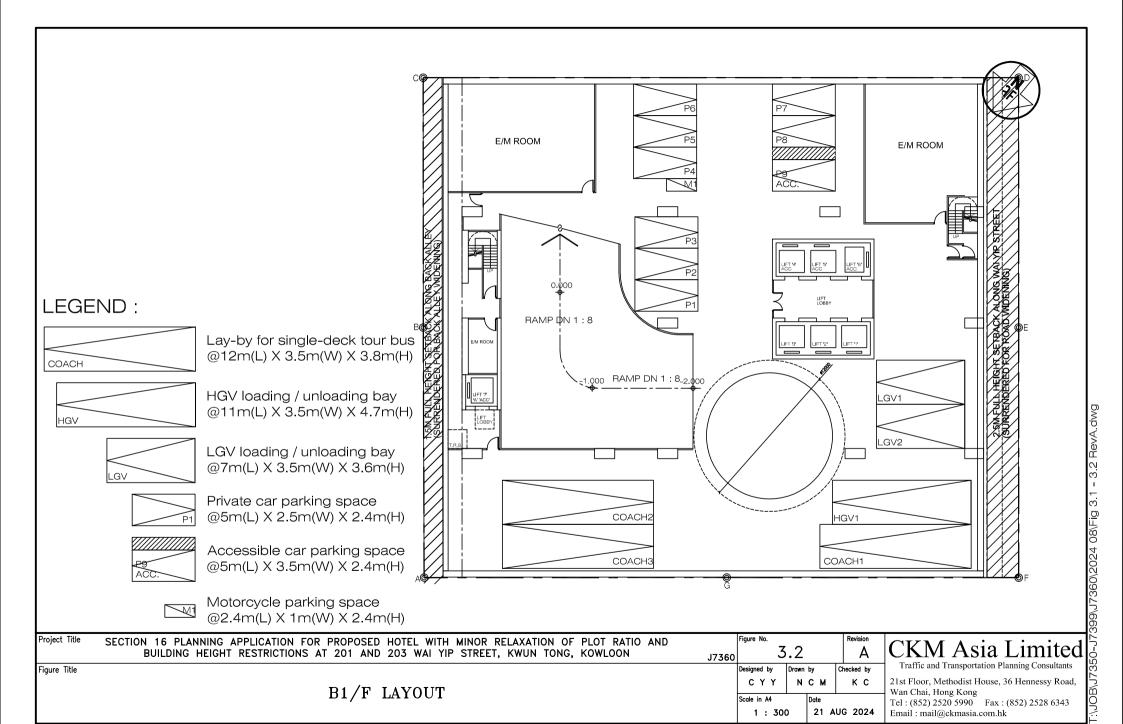
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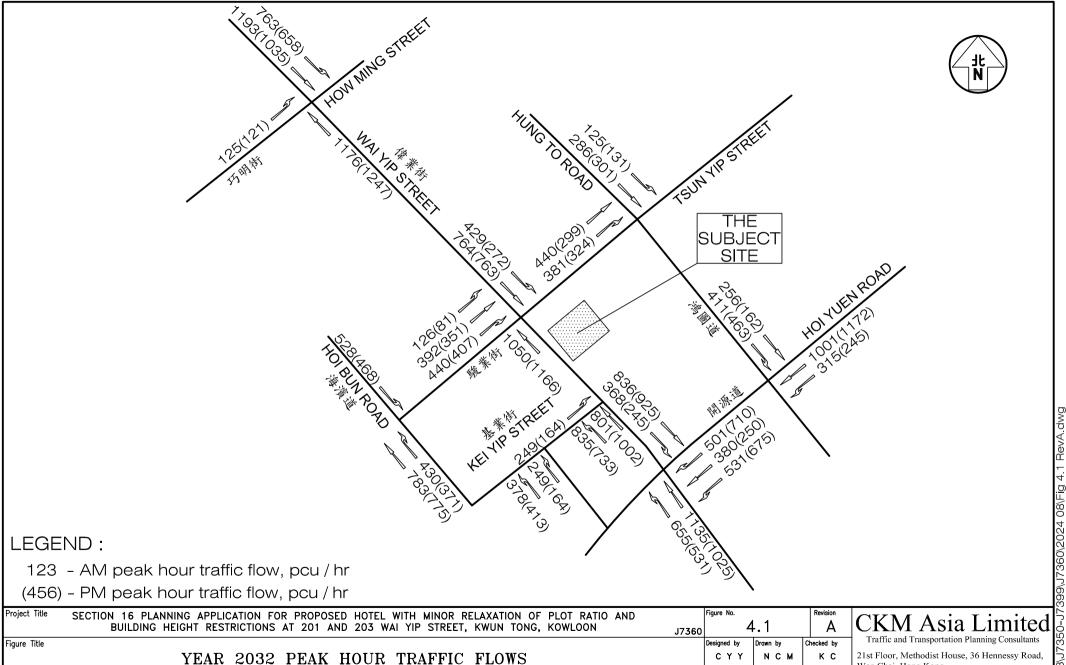
N.T.S.

21 AUG 2024









WITHOUT THE PROPOSED REDEVELOPMENT

Wan Chai, Hong Kong

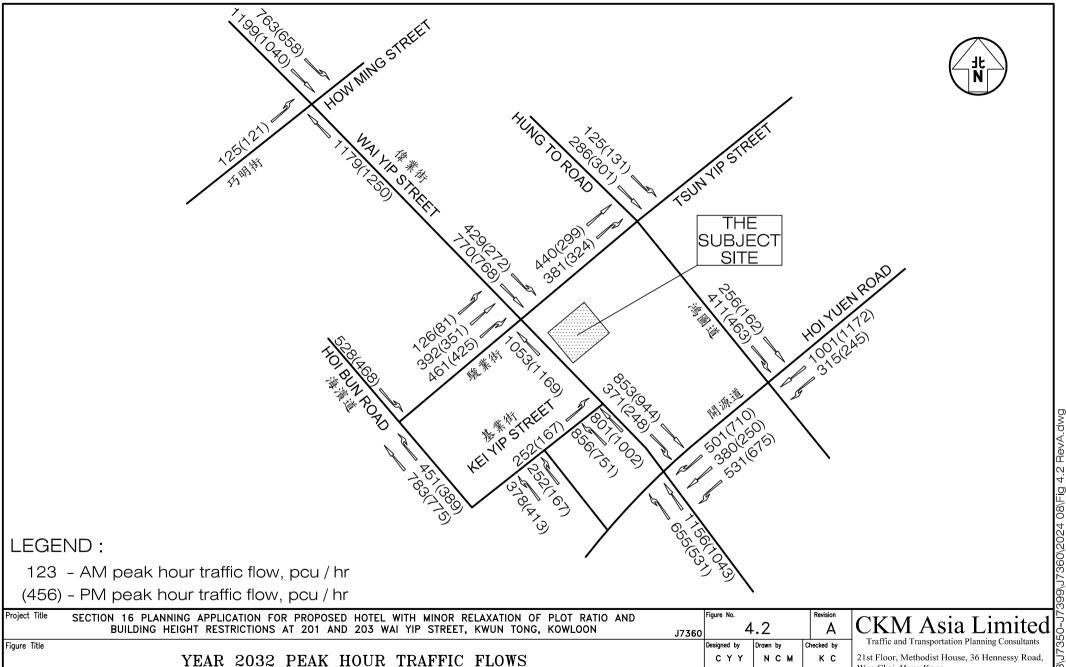
Email: mail@ckmasia.com.hk

Tel: (852) 2520 5990 Fax: (852) 2528 6343

Scale in A4

N.T.S.

21 AUG 2024



WITH THE PROPOSED REDEVELOPMENT

Wan Chai, Hong Kong

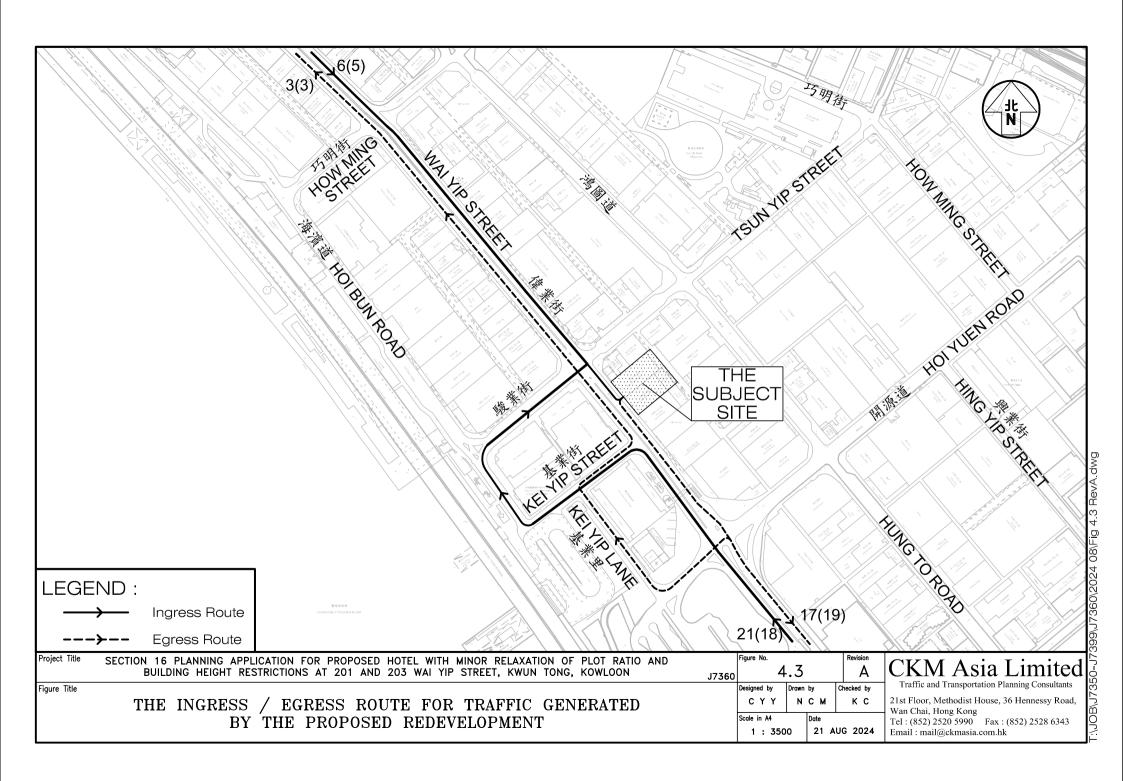
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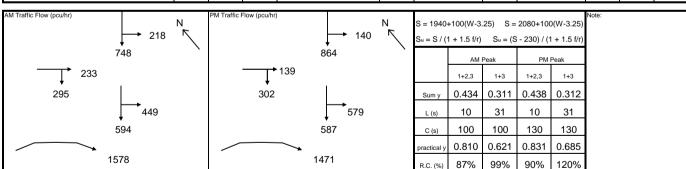
21 AUG 2024



 Junction:
 Hung To Road / Hoi Yuen Road / Wai Yip Street
 Job Number:
 J7360

 Scenario:
 Existing Condition
 Page
 1

| | | | | | | | AM Peak | | | | PM Peak | | | | | |
|--------------------|-------|-------|-------|-----------|------------|-----------------------|-----------|--------------------|------------------|---------|------------|-----------|--------------------|------------------|---------|------------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Wai Yip Street EB | RT | A1 | 2,3 | 5.00 | 30.0 | | 100 | 2014 | 521 | 0.259 | 0.259 | 100 | 2014 | 485 | 0.241 | |
| | RT | A2 | 2,3 | 4.50 | 33.0 | | 100 | 2109 | 545 | 0.258 | | 100 | 2109 | 508 | 0.241 | 0.241 |
| | RT | А3 | 2,3 | 4.50 | 36.0 | | 100 | 1982 | 512 | 0.258 | | 100 | 1982 | 478 | 0.241 | |
| Hung To Road EB | SA+RT | B1 | 3 | 4.00 | 18.0 | | 19 | 2121 | 288 | 0.136 | | 42 | 2082 | 238 | 0.114 | |
| - | RT | B2 | 3 | 3.30 | 15.0 | | 100 | 1768 | 240 | 0.136 | | 100 | 1768 | 203 | 0.115 | |
| Hoi Yuen Road SB | SA+LT | C1 | 1 | 3.50 | 15.0 | | 73 | 1831 | 300 | 0.164 | | 44 | 1882 | 317 | 0.168 | |
| | SA | C2 | 1 | 3.50 | | | | 2105 | 345 | 0.164 | | | 2105 | 355 | 0.169 | |
| | SA | C3 | 1 | 3.50 | | | | 1965 | 321 | 0.163 | | | 1965 | 332 | 0.169 | |
| Hoi Yuen Road SB | LT | D1 | 1 | 3.50 | 40.0 | | 100 | 1894 | 332 | 0.175 | | 100 | 1894 | 372 | 0.196 | |
| TIOI TUOTI NOUG OD | SA+LT | D2 | 1 | 3.50 | 43.0 | | 28 | 2085 | 366 | | 0.176 | 47 | 2071 | 408 | 0.197 | 0.197 |
| | SA | D3 | 1 | 3.50 | .0.0 | | | 1965 | 345 | 0.176 | 00 | | 1965 | 386 | 0.196 | 0.101 |
| | | | | | | | | | | | | | | | | |
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| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| pedestrian phase | | Ep | 2,3 | | min c | rossing | timo – | 7 | 500 | GM + | 10 | sec F | GM - | 17 | sec | |
| pedestriari priase | | Fp | 2 | | | rossing | | 6 | | GM + | 8 | sec F | | 14 | sec | |
| | | Gp | 1,2 | | | rossing | | 9 | | GM + | 13 | sec F | | 22 | sec | |
| | | Нр | 2 | | | rossing | | 7 | | GM + | 11 | sec F | | 18 | sec | |
| | | lp | 2,3 | | min c | rossing | time = | 8 | sec | GM + | 11 | sec F | GM = | 19 | sec | |
| | | | | | | | | | | | | | | | | |
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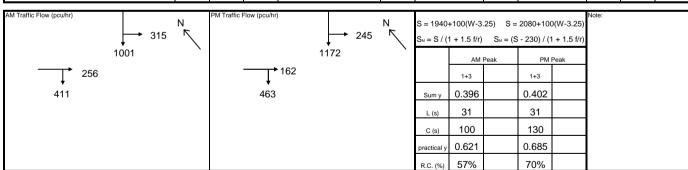


| 1 | Gp ↓ | D1 A' A2 | | Fp | B1 B2 JP A1 A2 A3 | | | | | |
|----|------|----------|--------|---------|-------------------|---------|-----|-------|-----|--|
| AM | G = | I/G = 7 | G = | I/G = | G = | I/G = 5 | G = | I/G = | G = | |
| | G = | I/G = 3 | G = 23 | I/G = 2 | G = | I/G = 5 | G = | I/G = | G = | |
| PM | G = | I/G = 7 | G = | I/G = | G = | I/G = 5 | G = | I/G = | G = | |
| | G = | I/G = 3 | G = 23 | I/G = 2 | G = | I/G = 5 | G = | I/G = | G = | |

 Junction:
 Hung To Road / Hoi Yuen Road
 Job Number:
 J7360

 Scenario:
 Without the Proposed Redevelopment
 Page
 2

| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|--------------------|-------|-------|-------|-----------|------------|-----------------------|-----------|--------------------|------------------|---------|------------|-----------|--------------------|------------------|---------|------------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Hung To Road EB | SA+RT | B1 | 3 | 4.00 | 18.0 | | 29 | 2104 | 362 | 0.172 | 0.173 | 52 | 2065 | 337 | 0.163 | 0.163 |
| | RT | B2 | 3 | 3.30 | 15.0 | | 100 | 1768 | 305 | 0.173 | | 100 | 1768 | 288 | 0.163 | |
| | | | | | | | | | | | | | | | | |
| Hoi Yuen Road SB | SA+LT | C1 | 1 | 3.50 | 15.0 | | 77 | 1825 | 407 | | 0.223 | 55 | 1863 | 445 | 0.239 | |
| | SA | C2 | 1 | 3.50 | | | | 2105 | 470 | 0.223 | | | 2105 | 503 | 0.239 | |
| | SA | C3 | 1 | 3.50 | | | | 1965 | 439 | 0.223 | | | 1965 | 469 | 0.239 | 0.239 |
| | | | | | | | | | | | | | | | | |
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| pedestrian phase | | Ep | 2,3 | | min o | rossing | timo – | 7 | 200 | GM + | 10 | 200 5 | GM = | 17 | sec | |
| pedestriari priase | | Fp | 2,3 | | | rossing | | 6 | | GM + | 8 | | GM = | 14 | sec | |
| | | Gp | 1,2 | | | rossing | | 9 | | GM + | 13 | | GM = | 22 | sec | |
| | | Нр | 2 | | | rossing | | 7 | | GM + | 11 | | GM = | 18 | sec | |
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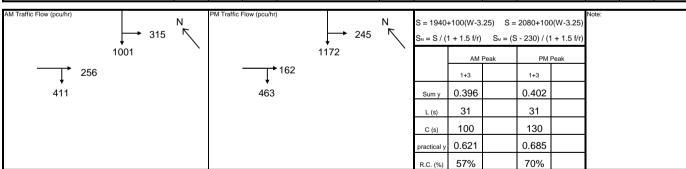


| 1 | Gp ↓ ↓ ↓ ↓ | 2 | Gp Hp | ∳ Fp | B1 | * | | | | |
|----|------------|---------|--------|---------|-----|---------|-----|-------|-----|--|
| АМ | G = | I/G = 3 | G = 23 | I/G = 2 | G = | I/G = 5 | G = | I/G = | G = | |
| | G = | I/G = | G = | I/G = | G = | I/G = | G = | I/G = | G = | |
| PM | G = | I/G = 3 | G = 23 | I/G = 2 | G = | I/G = 5 | G = | I/G = | G = | |
| | G = | I/G = | G = | I/G = | G = | I/G = | G = | I/G = | G = | |

 Junction:
 Hung To Road / Hoi Yuen Road
 Job Number:
 J7360

 Scenario:
 With the Proposed Redevelopment
 Page
 3

| | | | | | | | AM Peak | | | | PM Peak | | | | | |
|------------------|-------|-------|-------|-----------|------------|-----------------------|-----------|--------------------|------------------|---------|------------|-----------|-----------------------|------------------|---------|------------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Hung To Road EB | SA+RT | B1 | 3 | 4.00 | 18.0 | | 29 | 2104 | 362 | 0.172 | 0.173 | 52 | 2065 | 337 | 0.163 | 0.163 |
| | RT | B2 | 3 | 3.30 | 15.0 | | 100 | 1768 | 305 | 0.173 | | 100 | 1768 | 288 | 0.163 | |
| | | | | | | | | | | | | | | | | |
| Hoi Yuen Road SB | SA+LT | C1 | 1 | 3.50 | 15.0 | | 77 | 1825 | 407 | | 0.223 | 55 | 1863 | 445 | 0.239 | |
| | SA | C2 | 1 | 3.50 | | | | 2105 | 470 | 0.223 | | | 2105 | 503 | 0.239 | |
| | SA | C3 | 1 | 3.50 | | | | 1965 | 439 | 0.223 | | | 1965 | 469 | 0.239 | 0.239 |
| | | | | | | | | | | | | | | | | |
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| pedestrian phase | | Ep | 2,3 | | min c | rossing | time = | 7 | sec | GM + | 10 | sec F | GM = | 17 | sec | |
| | | Fp | 2 | | min c | rossing | time = | 6 | sec | GM + | 8 | sec F | GM = | 14 | sec | |
| | | Gp | 1,2 | | min c | rossing | time = | 9 | sec | GM + | 13 | sec F | GM = | 22 | sec | |
| | | Нр | 2 | | min c | rossing | time = | 7 | sec | GM + | 11 | sec F | GM = | 18 | sec | |
| _ | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |



| 1 | C3 C2 | C1 2 | Ep Gp ↓ Hp | ∳ Fp | B1 | * | | | | |
|----|-------|---------|------------------|---------|-----|---------|-----|-------|-----|--|
| AM | G = | I/G = 3 | G = 23 | I/G = 2 | G = | I/G = 5 | G = | I/G = | G = | |
| | G = | I/G = | G = | I/G = | G = | I/G = | G = | I/G = | G = | |
| РМ | G = | I/G = 3 | G = 23 | I/G = 2 | G = | I/G = 5 | G = | I/G = | G = | |
| | G = | I/G = | G = | I/G = | G = | I/G = | G = | I/G = | G = | |

Roundabout Analysis

Location Wai Yip Street / Hoi Yuen Road

| Scenario Existir | ng Condition | | | Page | 4 |
|------------------|--------------|------------------|------|---------|---------|
| Design Year: | 2023 | Job Number J7360 | Date | 20 Augu | st 2024 |

AM Peak

| Arm | To A | To B | To C | To D | Total | q _c |
|--------|------|------|------|------|-------|----------------|
| From A | 188 | 0 | 803 | 38 | 1029 | 549 |
| From B | 325 | 0 | 449 | 269 | 1043 | 1578 |
| From C | 990 | 0 | 390 | 86 | 1466 | 823 |
| From D | 119 | 0 | 156 | 3 | 278 | 1893 |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| Total | 1622 | 0 | 1798 | 396 | 3816 | |

PM Peak

| Arm | To A | То В | To C | To D | Total | q _c |
|--------|------|------|------|------|-------|----------------|
| From A | 139 | 0 | 782 | 40 | 961 | 510 |
| From B | 470 | 0 | 579 | 117 | 1166 | 1471 |
| From C | 886 | 0 | 317 | 121 | 1324 | 766 |
| From D | 151 | 0 | 193 | 0 | 344 | 1812 |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| Total | 1646 | 0 | 1871 | 278 | 3795 | |

Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| Α | Wai Yip Street |
| В | Hoi Yuen Road |
| С | Wai Yip Street |
| D | Bus Terminal Road |
| | |
| | |
| | |
| | |

Geometric Parameters

| CCOIIICUI | o i aramete | ,1 3 | | | | | |
|-----------|-------------|-------|-------|-------|-------|-------|-----|
| Arm | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S |
| From A | 8.5 | 7.3 | 25.0 | 3.0 | 75 | 25 | 0.6 |
| From B | 15.0 | 12.0 | 45.0 | 8.0 | 75 | 20 | 0.6 |
| From C | 10.0 | 7.0 | 20.0 | 10.0 | 75 | 20 | 0.5 |
| From D | 8.0 | 7.0 | 35.0 | 4.0 | 75 | 10 | 0.4 |
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Predictive Equation $Q_E = K(F - f_cq_c)$

| Q_E | Entry Capacity |
|----------------|-------------------------------------|
| $q_{\rm c}$ | Circulating Flow across the Entry |
| K | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F | $= 303x_2$ |
| f _c | $= 0.210t_D(1+0.2x_2)$ |
| t_{D} | = 1+0.5/(1+M) |
| М | $= \exp[(D-60)/10]$ |
| x_2 | = v+(e-v)/(1+2S) |
| S | = 1.6(e-v)/L |

Limitation

| е | Entry Width | 4.0 - 15.0 m |
|---|---------------------------|---------------|
| V | Approach Half Width | 2.0 - 7.3 m |
| r | Entry Radius | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m |
| Ø | Entry Angle | 10° - 60° |
| S | Sharpness of Flare | 0.0 - 3.0 |

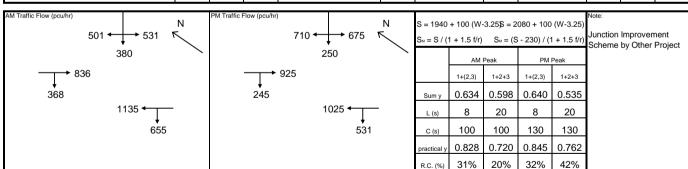
Ratio-of-Flow to Capacity (RFC)

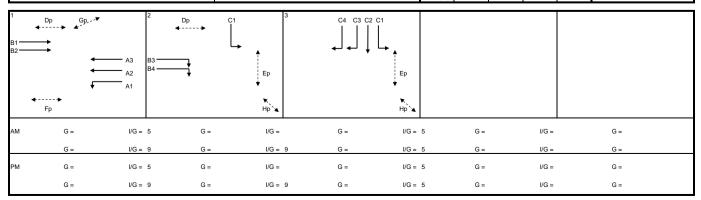
| | | | | | | | Q_E | | Entry Flow | | RFC | |
|--------|--------|-------|-------|-------|----------|----------------|-------|------|------------|------|-------|-------|
| Arm | x_2 | М | t_D | K | F | f _c | AM | PM | AM | PM | AM | PM |
| From A | 7.826 | 4.482 | 1.091 | 1.027 | 2371.374 | 0.588 | 2104 | 2128 | 1029 | 961 | 0.489 | 0.452 |
| From B | 13.364 | 4.482 | 1.091 | 1.062 | 4049.182 | 0.842 | 2889 | 2985 | 1043 | 1166 | 0.361 | 0.391 |
| From C | 8.531 | 4.482 | 1.091 | 1.035 | 2584.776 | 0.620 | 2146 | 2183 | 1466 | 1324 | 0.683 | 0.607 |
| From D | 7.556 | 4.482 | 1.091 | 1.090 | 2289.333 | 0.575 | 1308 | 1359 | 278 | 344 | 0.212 | 0.253 |
| | | | | | | | | | | | | |
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 Junction:
 Wai Yip Street / Hoi Yuen Road
 Job Number:
 J7360

 Scenario:
 Without the Proposed Redevelopment
 Page
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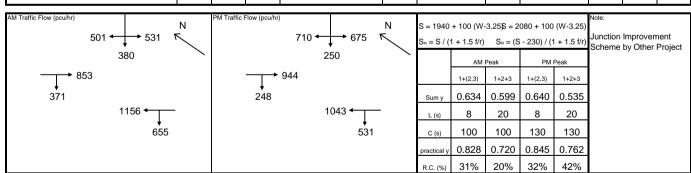
| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|-------------------|-------|--------|-------|-----------|------------|-----------------------|-----------|-----------------------|------------------|---------|------------|-----------|-----------------------|------------------|--|--|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Wai Yip Street WB | LT | A1 | 1 | 3.60 | 17.0 | | 100 | 1815 | 655 | 0.361 | 0.361 | 100 | 1815 | 531 | 0.293 | 0.293 |
| | SA | A2 | 1 | 3.60 | | | | 2115 | 568 | 0.269 | | | 2115 | 513 | 0.243 | |
| | SA | А3 | 1 | 3.60 | | | | 2115 | 567 | 0.268 | | | 2115 | 512 | 0.242 | |
| | | | | | | | | | | | | | | | | |
| Wai Yip Street EB | SA | B1 | 1 | 4.00 | | | | 2015 | 404 | 0.200 | | | 2015 | 447 | 0.222 | |
| | SA | B2 | 1 | 4.00 | | | | 2155 | 432 | 0.200 | | | 2155 | 478 | 0.222 | |
| | RT | В3 | 2 | 3.30 | 20.0 | | 100 | 1940 | 185 | 0.095 | 0.096 | 100 | 1940 | 123 | 0.063 | |
| | RT | B4 | 2 | 3.30 | 17.0 | | 100 | 1916 | 183 | 0.096 | | 100 | 1916 | 122 | 0.064 | |
| Hei Vora Brad OB | | 04 | 0.0 | 4.00 | 40.0 | | 400 | 4040 | 504 | 0.070 | | 400 | 4040 | 075 | 0.040 | 0.040 |
| Hoi Yuen Road SB | LT | C1 | 2,3 | 4.00 | 40.0 | | 100 | 1942 | 531 | 0.273 | 0.440 | 100 | 1942 | 675 | 0.348 | 0.348 |
| | SA | C2 | 3 | 4.40 | 00.0 | | 70 | 2195 | 311 | 0.142 | 0.142 | 400 | 2195 | 250 | 0.114 | |
| | SA+RT | C3 | 3 | 4.00 | 20.0 | | 76 | 2039 | 289 | 0.142 | | 100 | 2005 | 357 | 0.178 | |
| | RT | C4 | 3 | 4.00 | 17.0 | | 100 | 1980 | 281 | 0.142 | | 100 | 1980 | 353 | 0.178 | |
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| pedestrian phase | | Dp | 1,2 | | | rossing | | 11 | | GM + | 13 | | GM = | 24 | sec | |
| | | Ep | 2,3 | | | rossing | | 8 | | GM + | 10 | | GM = | 18 | sec | |
| | | Fp | 1 | | | rossing | | 11 | | GM + | 13 | | GM = | 24 | sec | |
| | | Gp | 1 | | | rossing | | 5 | | GM + | 6 | | GM = | 11 | sec | |
| | | Нр | 2,3 | | min c | rossing | time = | 5 | sec | GM + | 7 | sec F | GM = | 12 | sec | |
| | | | | | | | | | | | | | | | | |
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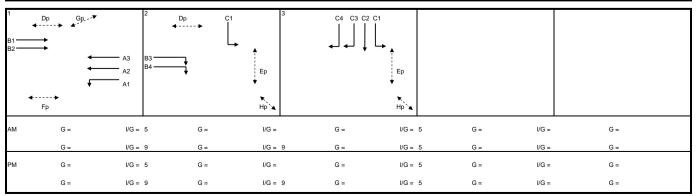




Junction:Wai Yip Street / Hoi Yuen RoadJob Number:J7360Scenario:With the Proposed RedevelopmentPage6

| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|-------------------|-------|----------|-------|-----------|------------|-----------------------|-----------|-----------------------|------------------|---------------------|------------|-----------|-----------------------|------------------|---------|----------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical |
| Wai Yip Street WB | LT | A1 | 1 | 3.60 | 17.0 | | 100 | 1815 | 655 | 0.361 | 0.361 | 100 | 1815 | 531 | 0.293 | 0.293 |
| | SA | A2 | 1 | 3.60 | | | | 2115 | 578 | 0.273 | | | 2115 | 522 | 0.247 | |
| | SA | А3 | 1 | 3.60 | | | | 2115 | 578 | 0.273 | | | 2115 | 521 | 0.246 | |
| Wai Yip Street EB | SA | B1 | 1 | 4.00 | | | | 2015 | 412 | 0.204 | | | 2015 | 456 | 0.226 | |
| | SA | B2 | 1 | 4.00 | | | | 2155 | 441 | 0.205 | | | 2155 | 488 | 0.226 | |
| | RT | В3 | 2 | 3.30 | 20.0 | | 100 | 1940 | 187 | 0.096 | 0.096 | 100 | 1940 | 125 | 0.064 | |
| | RT | B4 | 2 | 3.30 | 17.0 | | 100 | 1916 | 184 | 0.096 | | 100 | 1916 | 123 | 0.064 | |
| Hoi Yuen Road SB | LT | C1 | 2,3 | 4.00 | 40.0 | | 100 | 1942 | 531 | 0.273 | | 100 | 1942 | 675 | 0.348 | 0.348 |
| | SA | C2 | 3 | 4.40 | | | | 2195 | 311 | 0.142 | 0.142 | | 2195 | 250 | 0.114 | |
| | SA+RT | C3 | 3 | 4.00 | 20.0 | | 76 | 2039 | 289 | 0.142 | | 100 | 2005 | 357 | 0.178 | |
| | RT | C4 | 3 | 4.00 | 17.0 | | 100 | 1980 | 281 | 0.142 | | 100 | 1980 | 353 | 0.178 | |
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| | | | 4.0 | | | | | 44 | | 014 | 40 | | | 0.4 | | |
| pedestrian phase | | Dp | 1,2 | | | rossing | | 11 | | GM + | 13 | | GM = | 24 18 | sec | |
| | | Ep Fp | 2,3 | | | rossing rossing | | 8 11 | | <u>GM +</u> GM + | 10 13 | | GM = GM = | 24 | sec | |
| | | Gp | 1 | | | rossing | | 5 | | GM + | 6 | | GM = | 11 | sec | |
| | | Нр | 2,3 | | | rossing | | 5 | | GM + | 7 | | GM = | 12 | sec | |
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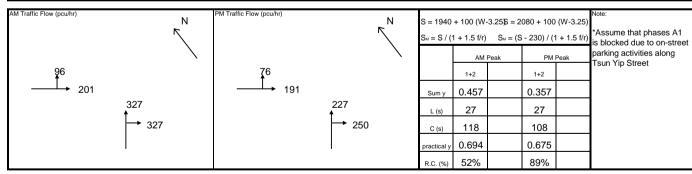


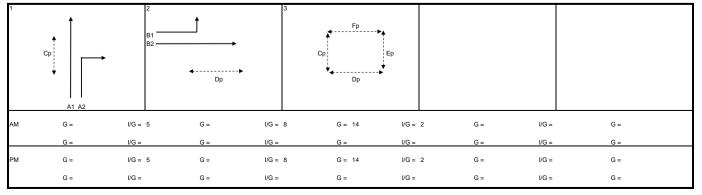


 Junction:
 Hung To Road / Tsun Yip Street
 Job Number:
 J7360

 Scenario:
 Existing Condition
 Page
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| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|--------------------|----|-----------------|------------|-----------|------------|-----------------------|-----------|--------------------|------------------|---------------------|------------|-----------|--------------------|------------------|---------|------------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Tsun Yip Street NB | SA | A1* | 1 | 3.20 | | | | | | | | | | | | |
| | RT | A2 | 1 | 3.20 | 15.0 | | 50 | 1843 | 654 | 0.355 | 0.355 | 52 | 1839 | 477 | 0.259 | 0.259 |
| | | | | | | | | | | | | | | | | |
| Hung To Road EB | LT | B1 | 2 | 3.50 | 10.0 | | 100 | 1709 | 96 | 0.056 | | 100 | 1709 | 76 | 0.044 | |
| | SA | B2 | 2 | 3.50 | | | | 1965 | 201 | 0.102 | 0.102 | | 1965 | 191 | 0.097 | 0.097 |
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| pedestrian phase | | Cp Dp | 1,3 2,3 | | | rossing | | 6 9 | | GM + | 6 9 | sec F | | 12 18 | sec | |
| | | <u>Бр</u> Ер | 3 | | | rossing rossing | | 7 | | <u>GM +</u> GM + | 7 | | GM = GM = | 14 | sec | |
| | | Fp | 3 | | | rossing | | 7 | | GM + | 7 | | GM = | 14 | sec | |
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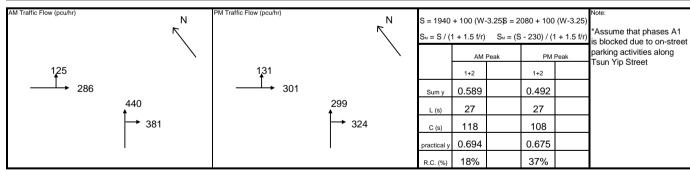


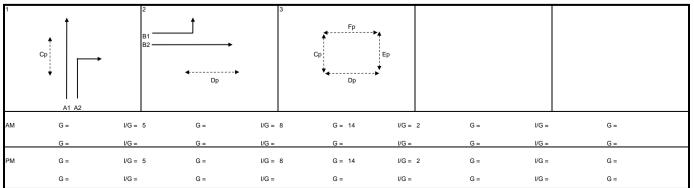


 Junction:
 Hung To Road / Tsun Yip Street
 Job Number:
 J7360

 Scenario:
 Without the Proposed Redevelopment
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| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|--------------------|----|-------|-------|-----------|------------|-----------------------|-----------|--------------------|------------------|---------|------------|-----------|-----------------------|------------------|---------|----------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical |
| Tsun Yip Street NB | SA | A1* | 1 | 3.20 | | | | | | | | | | | | |
| | RT | A2 | 1 | 3.20 | 15.0 | | 46 | 1850 | 821 | 0.444 | 0.444 | 52 | 1839 | 623 | 0.339 | 0.33 |
| | | | _ | | | | | | | | | | | | | |
| Hung To Road EB | LT | B1 | 2 | 3.50 | 10.0 | | 100 | 1709 | 125 | 0.073 | | 100 | 1709 | 131 | 0.077 | |
| | SA | B2 | 2 | 3.50 | | | | 1965 | 286 | 0.146 | 0.146 | | 1965 | 301 | 0.153 | 0.15 |
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| pedestrian phase | | Ср | 1,3 | | min c | rossing | time = | 6 | sec | GM + | 6 | sec F | GM = | 12 | sec | |
| <u>.</u> | | Dp | 2,3 | | | rossing | | 9 | | GM + | 9 | sec F | | 18 | sec | |
| - | | Ep | 3 | | | rossing | | 7 | sec | GM + | 7 | sec F | GM = | 14 | sec | |
| | | Fp | 3 | | min c | rossing | time = | 7 | sec | GM + | 7 | sec F | GM = | 14 | sec | |
| | | | | | | | | | | | | | | | | |
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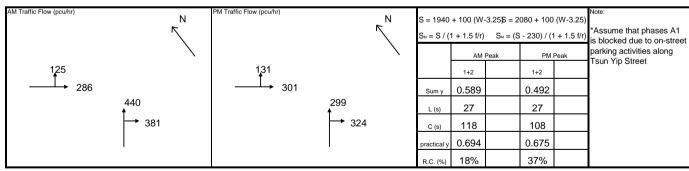


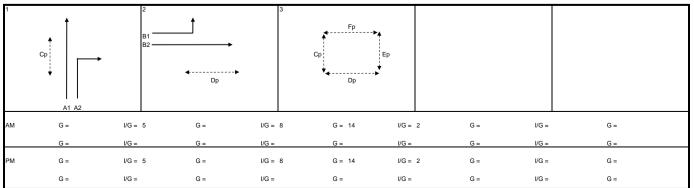


 Junction:
 Hung To Road / Tsun Yip Street
 Job Number:
 J7360

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| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|--------------------|----|----------|-------|-----------|------------|-----------------------|-----------|-----------------------|------------------|--------------|------------|-----------|-----------------------|------------------|---------|------------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Tsun Yip Street NB | SA | A1* | 1 | 3.20 | | | | | | | | | | | | |
| | RT | A2 | 1 | 3.20 | 15.0 | | 46 | 1850 | 821 | 0.444 | 0.444 | 52 | 1839 | 623 | 0.339 | 0.339 |
| Hung To Road EB | LT | B1 | 2 | 3.50 | 10.0 | | 100 | 1709 | 125 | 0.073 | | 100 | 1709 | 131 | 0.077 | |
| riding to Rodd ED | SA | B2 | 2 | 3.50 | 10.0 | | 100 | 1965 | 286 | 0.146 | 0.146 | 100 | 1965 | 301 | 0.153 | 0.153 |
| | | | | | | | | | | 01110 | 01110 | | | | 01100 | |
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| pedestrian phase | | Ср | 1,3 | | | rossing | | 6 | | GM + | 6 | sec F | | 12 | sec | |
| | | Dp Fn | 2,3 | | | rossing | | 9 | | GM + | 9 | sec F | | 18 | sec | |
| | | Ep Fp | 3 | | | rossing rossing | | 7 | | GM + GM + | 7 | sec F | | 14 14 | sec | |
| | | ' ' ' | | | | . 5551119 | | | 550 | Ç.VI ' | • | 0001 | <u> </u> | | 555 | |
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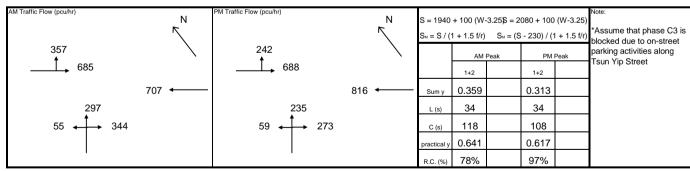


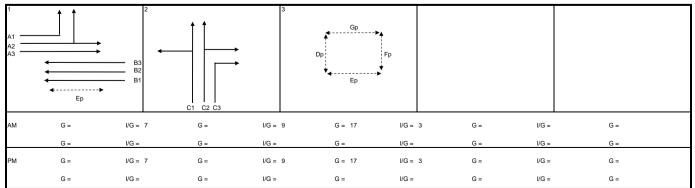


 Junction:
 Wai Yip Street / Tsun Yip Street
 Job Number:
 J7360

 Scenario:
 Existing Condition
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| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|--------------------|-------|-----------|----------|-----------|------------|-----------------------|-----------|--------------------|------------------|---------------------|------------|-----------|--------------------|------------------|---------|------------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Wai Yip Street EB | LT | A1 | 1 | 3.00 | 10.0 | | 100 | 1665 | 302 | 0.181 | 0.182 | 100 | 1665 | 242 | 0.145 | |
| | SA+LT | A2 | 1 | 3.00 | 15.0 | | 15 | 2025 | 367 | 0.181 | | 0 | 2055 | 344 | 0.167 | 0.167 |
| | SA | А3 | 1 | 3.00 | | | | 2055 | 373 | 0.182 | | | 2055 | 344 | 0.167 | |
| Wai Yip Street WB | SA | B1 | 1 | 3.00 | | | | 1915 | 225 | 0.117 | | | 1915 | 259 | 0.135 | |
| | SA | B2 | 1 | 3.00 | | | | 2055 | 241 | 0.117 | | | 2055 | 278 | 0.135 | |
| | SA | В3 | 1 | 3.00 | | | | 2055 | 241 | 0.117 | | | 2055 | 279 | 0.136 | |
| Tsun Yip Street NB | SA+LT | C1 | 2 | 3.80 | 15.0 | | 16 | 1964 | 349 | 0 178 | 0.178 | 21 | 1954 | 283 | 0.145 | 0.145 |
| Tour Tip Offeet No | SA+RT | C2 | 2 | 3.30 | 22.0 | | 99 | 1953 | 347 | 0.178 | 0.170 | 96 | 1957 | 284 | 0.145 | 0.143 |
| | RT | C3* | 2 | 3.30 | 18.0 | | - 00 | 1000 | 011 | 0.170 | | - 00 | 1007 | 201 | 0.110 | |
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| pedestrian phase | | Dp - | 3 1,3 | | | rossing | | 9 | | GM + | 8 14 | sec F | | 17 28 | sec | |
| | | Ep Fp | 3 | | | rossing rossing | | 9 | | <u>GM +</u> GM + | 8 | sec F | | 28 17 | sec | |
| | | -гр Gp | 3 | | | rossing | | 12 | | GM + | 12 | sec F | | 24 | sec | |
| | | | | | | | _ | _ | | • | | _ | • | - | | |
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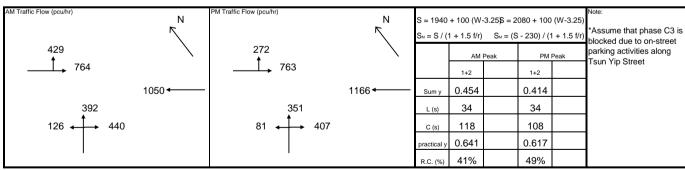


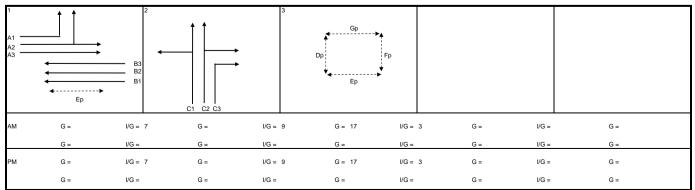


 Junction:
 Wai Yip Street / Tsun Yip Street
 Job Number:
 J7360

 Scenario:
 Without the Proposed Redevelopment
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| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|--------------------|-------|-------|-------|-----------|------------|-----------------------|-----------|--------------------|------------------|---------|------------|-----------|--------------------|------------------|---------|------------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Wai Yip Street EB | LT | A1 | 1 | 3.00 | 10.0 | | 100 | 1665 | 347 | 0.208 | 0.208 | 100 | 1665 | 272 | 0.163 | |
| | SA+LT | A2 | 1 | 3.00 | 15.0 | | 19 | 2017 | 419 | 0.208 | | 0 | 2055 | 382 | 0.186 | |
| | SA | А3 | 1 | 3.00 | | | | 2055 | 427 | 0.208 | | | 2055 | 381 | 0.185 | |
| Wai Yip Street WB | SA | B1 | 1 | 3.00 | | | | 1915 | 334 | 0.174 | | | 1915 | 371 | 0.194 | 0.194 |
| | SA | B2 | 1 | 3.00 | | | | 2055 | 358 | 0.174 | | | 2055 | 398 | 0.194 | |
| | SA | В3 | 1 | 3.00 | | | | 2055 | 358 | 0.174 | | | 2055 | 397 | 0.193 | |
| Tsun Yip Street NB | SA+LT | C1 | 2 | 3.80 | 15.0 | | 26 | 1944 | 477 | 0.245 | 0.245 | 19 | 1958 | 432 | 0.221 | |
| | SA+RT | C2 | 2 | 3.30 | 22.0 | | 91 | 1963 | 481 | 0.245 | | 100 | 1952 | 407 | 0.209 | 0.221 |
| | RT | C3* | 2 | 3.30 | 18.0 | | | | | | | | | | | |
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| | | | | | | | | | | | | | | | | |
| pedestrian phase | | Dp | 3 | | min c | rossing | time = | 9 | sec | GM + | 8 | sec F | GM = | 17 | sec | |
| | | Ep | 1,3 | | min c | rossing | time = | 14 | sec | GM + | 14 | sec F | GM = | 28 | sec | |
| | | Fp | 3 | | min c | rossing | time = | 9 | sec | GM + | 8 | sec F | GM = | 17 | sec | |
| | | Gp | 3 | | min c | rossing | time = | 12 | sec | GM + | 12 | sec F | GM = | 24 | sec | |
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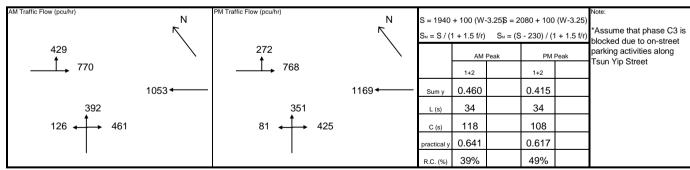


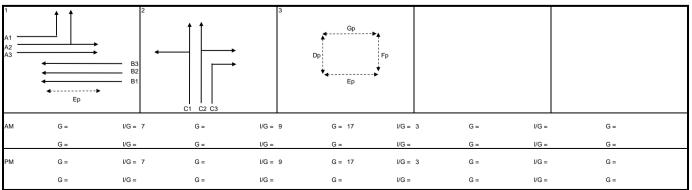


 Junction:
 Wai Yip Street / Tsun Yip Street
 Job Number:
 J7360

 Scenario:
 With the Proposed Redevelopment
 Page
 12

| | | | | | | | | AM Peak | | | | | PM Peak | | |
|-------|-------------------------------|---|---|---|---|--|--|--|---|------------|---|--|---|--|--|
| | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| LT | A1 | 1 | 3.00 | 10.0 | | 100 | 1665 | 348 | 0.209 | 0.209 | 100 | 1665 | 272 | 0.163 | |
| SA+LT | A2 | 1 | 3.00 | 15.0 | | 19 | 2017 | 422 | 0.209 | | 0 | 2055 | 384 | 0.187 | |
| SA | А3 | 1 | 3.00 | | | | 2055 | 429 | 0.209 | | | 2055 | 384 | 0.187 | |
| SA | B1 | 1 | 3.00 | | | | 1915 | 335 | 0.175 | | | 1915 | 372 | 0.194 | |
| SA | B2 | 1 | 3.00 | | | | 2055 | 359 | 0.175 | | | 2055 | 399 | 0.194 | 0.194 |
| SA | В3 | 1 | 3.00 | | | | 2055 | 359 | 0.175 | | | 2055 | 398 | 0.194 | |
| SA+LT | C1 | 2 | 3.80 | 15.0 | | 26 | 1944 | 488 | 0.251 | 0.251 | 19 | 1958 | 432 | 0.221 | |
| SA+RT | C2 | 2 | 3.30 | 22.0 | | 94 | 1959 | 491 | | | 100 | 1952 | 425 | | 0.221 |
| RT | C3* | 2 | 3.30 | 18.0 | | | | | | | | | | | |
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| | Dn | 3 | | min c | rossina | time – | a | 200 | CM + | ρ | sac F | GM - | 17 | 202 | |
| | | | | | | | | | | | | | | | |
| | | , | | | | | | | | | | | | | |
| | Gp | 3 | | | | | 12 | | | 12 | | | 24 | sec | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | SA+LT SA SA SA SA SA+LT SA+RT | LT A1 SA+LT A2 SA A3 SA B1 SA B2 SA B3 SA+LT C1 SA+RT C2 RT C3* Dp Ep Fp | LT A1 1 SA+LT A2 1 SA A3 1 SA B1 1 SA B2 1 SA B3 1 SA+LT C1 2 SA+RT C2 2 RT C3* 2 Dp 3 Ep 1,3 Fp 3 | LT A1 1 3.00 SA+LT A2 1 3.00 SA A3 1 3.00 SA B1 1 3.00 SA B2 1 3.00 SA B3 1 3.00 SA B3 1 3.00 SA+LT C1 2 3.80 SA+RT C2 2 3.30 RT C3* 2 3.30 DD 3 Ep 1,3 Fp 3 | LT A1 1 3.00 10.0 SA+LT A2 1 3.00 15.0 SA A3 1 3.00 SA B1 1 3.00 SA B2 1 3.00 SA B3 1 3.00 SA+LT C1 2 3.80 15.0 SA+RT C2 2 3.30 22.0 RT C3* 2 3.30 18.0 Dp 3 min c Ep 1,3 min c Fp 3 min c | LT A1 1 3.00 10.0 SA+LT A2 1 3.00 15.0 SA A3 1 3.00 SA B1 1 3.00 SA B2 1 3.00 SA B3 1 3.00 SA+LT C1 2 3.80 15.0 SA+RT C2 2 3.30 22.0 RT C3* 2 3.30 18.0 Dp 3 min crossing Ep 1,3 min crossing Fp 3 min crossing | LT A1 1 3.00 10.0 100 SA+LT A2 1 3.00 15.0 19 SA A3 1 3.00 SA B1 1 3.00 SA B2 1 3.00 SA B3 1 3.00 SA+LT C1 2 3.80 15.0 26 SA+RT C2 2 3.30 22.0 94 RT C3* 2 3.30 18.0 Dp 3 min crossing time = Ep 1,3 min crossing time = Fp 3 min crossing time = | LT A1 1 3.00 10.0 100 1665 SA+LT A2 1 3.00 15.0 19 2017 SA A3 1 3.00 50 50 1915 SA B1 1 3.00 50 50 1915 SA B2 1 3.00 50 50 50 50 50 50 50 50 50 50 50 50 5 | Phase Stage Width (m) Radius (m) % Up-hill Turning % Sat. Flow (pcu/hr) Flow (pcu/hr) | Phase | Phase Stage Width (m) Radius (m) % Up-hill Turning % Sat. Flow (pcuhhr) (pcuhhr) | Phase Stage Width (m) Radius (m) % Up-hill Turning % Godent Turning % (pouhh) (p | Phase Stage Width (m) Radius (m) % Up-hill Turning % Sat. Flow (pouhr) y value Critical y Turning % Sat. Flow (pouhr) | Phase Slage Width (m) Radius (m) % Up-hill Turning % Sat. Flow Gradent Gradent Flow (purch) (p | Phase Stage Width (m) Radius (m) Sub-hill Tuming % Sat. Flow (gouth) (|

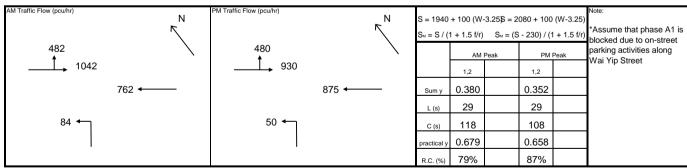


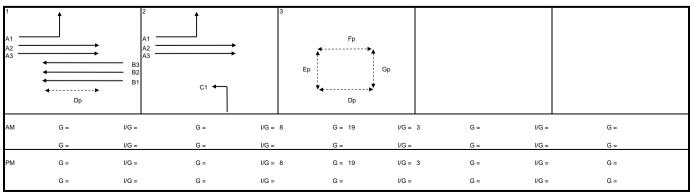


 Junction:
 Wai Yip Street / How Ming Street
 Job Number:
 J7360

 Scenario:
 Existing Condition
 Page
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| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|---|----|----------|-------|-----------|------------|-----------------------|-----------|--------------------|------------------|--------------|------------|-----------|--------------------|------------------|---------|----------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical |
| Wai Yip Street EB | LT | A1* | 1,2 | 3.00 | 20.0 | | | | | | | | | | | |
| | SA | A2 | 1,2 | 3.00 | 20.0 | | 65 | 1959 | 744 | 0.380 | 0.380 | 70 | 1952 | 687 | 0.352 | 0.352 |
| | SA | А3 | 1,2 | 3.00 | | | | 2055 | 780 | 0.380 | | | 2055 | 723 | 0.352 | |
| Wai Yip Street WB | SA | B1 | 1 | 2.60 | | | | 1875 | 238 | 0.127 | | | 1875 | 275 | 0.147 | |
| 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | SA | B2 | 1 | 3.00 | | | | 2055 | 262 | 0.127 | | | 2055 | 300 | 0.146 | |
| | SA | В3 | 1 | 3.00 | | | | 2055 | 262 | 0.127 | | | 2055 | 300 | 0.146 | |
| How Ming Street NB | LT | C1 | 2 | 3.50 | 20.0 | | 100 | 1828 | 84 | 0.046 | | 100 | 1828 | 50 | 0.027 | |
| | | | | | | | | | | | | | | | | |
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| pedestrian phase | | Dp | 1,3 | | | rossing | | 5 | | GM + | 7 | | GM = | 12 | sec | |
| | | Ep | 3 | | | rossing | | 10 | | GM + | 9 | | GM = | 19 | sec | |
| | | Fp Gp | 3 | | | rossing | | 5 9 | | GM + GM + | 7 8 | | GM = GM = | 12 17 | sec | |
| | | . Gp | 3 | | HIIIIC | iossing | ume = | 9 | Sec | GIVI + | 0 | Secr | GIVI = | 17 | Sec | |
| | | | | | | | | | | | | | | | | |
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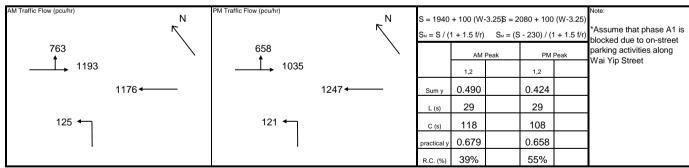


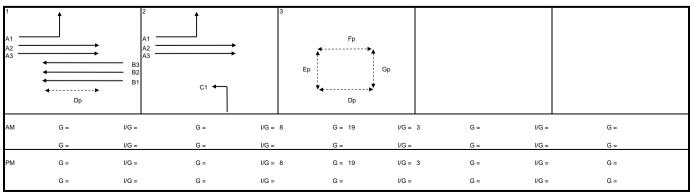


 Junction:
 Wai Yip Street / How Ming Street
 Job Number:
 J7360

 Scenario:
 Without the Proposed Redevelopment
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| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|--------------------|----|-------|-------|-----------|------------|-----------------------|-----------|-----------------------|------------------|---------|------------|-----------|--------------------|------------------|---------|------------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Wai Yip Street EB | LT | A1* | 1,2 | 3.00 | 20.0 | | | | | | | | | | | |
| | SA | A2 | 1,2 | 3.00 | 20.0 | | 80 | 1939 | 950 | 0.490 | 0.490 | 80 | 1939 | 822 | 0.424 | 0.424 |
| | SA | А3 | 1,2 | 3.00 | | | | 2055 | 1006 | 0.490 | | | 2055 | 871 | 0.424 | |
| Wai Yip Street WB | SA | B1 | 1 | 2.60 | | | | 1875 | 368 | 0.196 | | | 1875 | 391 | 0.209 | |
| | SA | B2 | 1 | 3.00 | | | | 2055 | 404 | 0.197 | | | 2055 | 428 | 0.208 | |
| | SA | В3 | 1 | 3.00 | | | | 2055 | 404 | 0.197 | | | 2055 | 428 | 0.208 | |
| How Ming Street NB | LT | C1 | 2 | 3.50 | 20.0 | | 100 | 1828 | 125 | 0.068 | | 100 | 1828 | 121 | 0.066 | |
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| pedestrian phase | | Dp | 1,3 | | min c | rossing | time = | 5 | sec | GM + | 7 | sec F | GM = | 12 | sec | |
| | | Ep | 3 | | min c | rossing | time = | 10 | sec | GM + | 9 | sec F | GM = | 19 | sec | |
| | | Fp | 3 | | min c | rossing | time = | 5 | sec | GM + | 7 | sec F | GM = | 12 | sec | |
| | | Gp | 3 | | min c | rossing | time = | 9 | sec | GM + | 8 | sec F | GM = | 17 | sec | |
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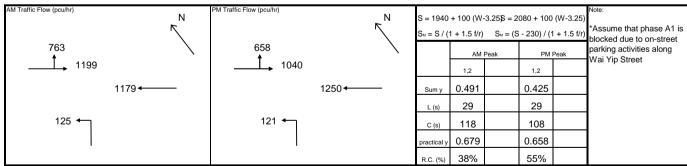


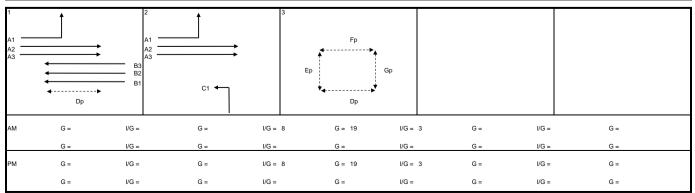


 Junction:
 Wai Yip Street / How Ming Street
 Job Number:
 J7360

 Scenario:
 With the Proposed Redevelopment
 Page
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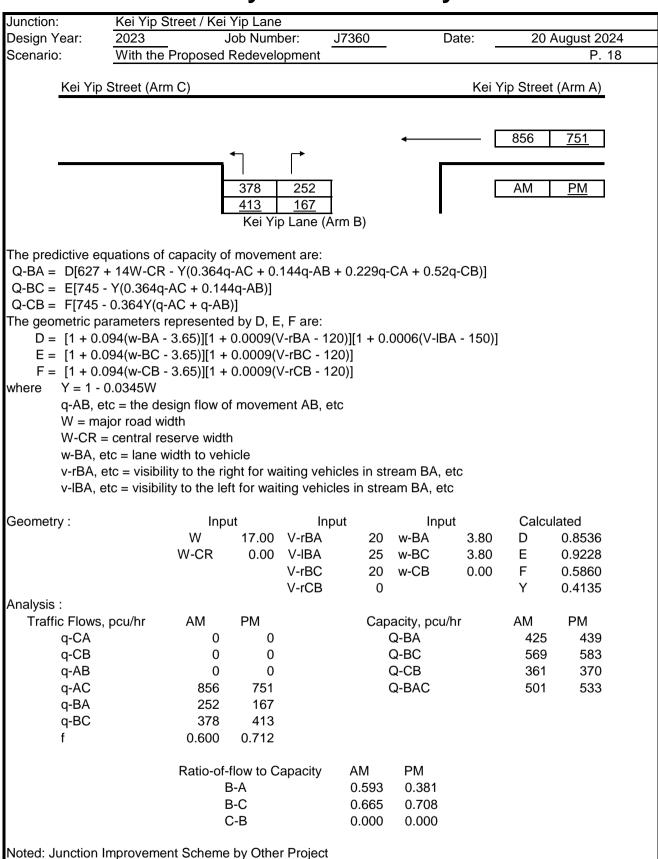
| | | | | | | | | | AM Peak | | | | | PM Peak | | |
|---------------------------|----|-------|-------|-----------|------------|-----------------------|-----------|--------------------|------------------|---------|------------|-----------|-----------------------|------------------|---------|------------|
| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | Flow (pcu/hr) | y value | Critical y |
| Wai Yip Street EB | LT | A1* | 1,2 | 3.00 | 20.0 | | | | | | | | | | | |
| · | SA | A2 | 1,2 | 3.00 | 20.0 | | 80 | 1939 | 953 | 0.491 | 0.491 | 80 | 1939 | 824 | 0.425 | 0.425 |
| | SA | А3 | 1,2 | 3.00 | | | | 2055 | 1009 | 0.491 | | | 2055 | 874 | 0.425 | |
| | | | | | | | | | | | | | | | | |
| Wai Yip Street WB | SA | B1 | 1 | 2.60 | | | | 1875 | 369 | 0.197 | | | 1875 | 392 | 0.209 | |
| | SA | B2 | 1 | 3.00 | | | | 2055 | 405 | 0.197 | | | 2055 | 429 | 0.209 | |
| | SA | В3 | 1 | 3.00 | | | | 2055 | 405 | 0.197 | | | 2055 | 429 | 0.209 | |
| Harri Mira er Chan an NID | | C4 | 0 | 2.50 | 20.0 | | 400 | 4000 | 405 | 0.000 | | 100 | 4000 | 404 | 0.000 | |
| How Ming Street NB | LT | C1 | 2 | 3.50 | 20.0 | | 100 | 1828 | 125 | 0.068 | | 100 | 1828 | 121 | 0.066 | |
| | | | | | | | | | | | | | | | | |
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| pedestrian phase | | Dp | 1,3 | | min c | rossing | time = | 5 | sec | GM + | 7 | sec F | GM = | 12 | sec | |
| | | Ep | 3 | | min c | rossing | time = | 10 | sec | GM + | 9 | sec F | GM = | 19 | sec | |
| | | Fp | 3 | | min c | rossing | time = | 5 | sec | GM + | 7 | sec F | GM = | 12 | sec | |
| | | Gp | 3 | | min c | rossing | time = | 9 | sec | GM + | 8 | sec F | GM = | 17 | sec | |
| | | | | | | | | | | | | | | | | |
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Junction: Kei Yip Street / Kei Yip Lane Design Year: 2023 J7360 20 August 2024 Job Number: Date: Scenario: **Existing Condition** Kei Yip Street (Arm C) Kei Yip Street (Arm A) 911 822 4 8 11 AM PM 15 Kei Yip Lane (Arm B) The predictive equations of capacity of movement are: Q-BA = D[627 + 14W-CR - Y(0.364q-AC + 0.144q-AB + 0.229q-CA + 0.52q-CB)]Q-BC = E[745 - Y(0.364q-AC + 0.144q-AB)]Q-CB = F[745 - 0.364Y(q-AC + q-AB)]The geometric parameters represented by D, E, F are: D = [1 + 0.094(w-BA - 3.65)][1 + 0.0009(V-rBA - 120)][1 + 0.0006(V-lBA - 150)]E = [1 + 0.094(w-BC - 3.65)][1 + 0.0009(V-rBC - 120)]F = [1 + 0.094(w-CB - 3.65)][1 + 0.0009(V-rCB - 120)]where Y = 1 - 0.0345Wq-AB, etc = the design flow of movement AB, etc W = major road width W-CR = central reserve width w-BA, etc = lane width to vehicle v-rBA, etc = visibility to the right for waiting vehicles in stream BA, etc v-IBA, etc = visibility to the left for waiting vehicles in stream BA, etc Geometry: Calculated Input Input Input W 13.00 V-rBA 0 w-BA 0.00 0.5332 D Ε W-CR 0.00 V-IBA 0 w-BC 3.80 0.9320 V-rBC 30 w-CB 0.00 F 0.5860 V-rCB 0 Υ 0.5515 Analysis: Traffic Flows, pcu/hr PM Capacity, pcu/hr AM РМ ΑM Q-BA q-CA 0 0 237 246 q-CB 0 Q-BC 524 540 0 q-AB 4 8 Q-CB 329 339 822 Q-BAC 524 q-AC 911 540 q-BA 0 0 q-BC 11 15 1.000 1.000 Ratio-of-flow to Capacity PMAM B-A 0.000 0.000 B-C 0.021 0.028 C-B 0.000 0.000

| | Rei Tip Street / I | (ei Yip Lane | | | | | |
|---|---|--|--|--|----------------------|---|---|
| Design Year: | 2023 | Job Numb | | Da | ite: | 20 A | August 2024 |
| Scenario: | Without the Prop | osed Redev | elopment | | | | P. 17 |
| Kei Yip | Street (Arm C) | | | | Kei Y | ip Street | (Arm A) |
| <u></u> | 3.1.331 (1.1111 3) | | | | | ., 0001 | (* / .) |
| | | | | | _ | | |
| | | _ | | • | <u> </u> | 835 | <u>733</u> |
| | | ק` | | | | | |
| | | 378 | 249 | | Г | AM | PM |
| | | <u>413</u> | <u>164</u> | | <u> </u> | | |
| | | Kei Yip | Lane (Arm B) | - | | | |
| The prodictive of | quations of consoits | , of moveme | ant ara: | | | | |
| | quations of capacity + 14W-CR - Y(0.36 | | | -CA + 0 52a | -CB)1 | | |
| - | - Y(0.364q-AC + 0. | • | | <i>5.</i> 0.029 | J = //1 | | |
| - | - 0.364Y(q-AC + q- | . ,- | | | | | |
| - | arameters represer | / - | , F are: | | | | |
| • | 094(w-BA - 3.65)][1 | | | .0006(V-IBA | - 150)] | | |
| - | 094(w-BC - 3.65)][1 | , | / | ` | /- | | |
| - | 094(w-CB - 3.65)][1 | , | , - | | | | |
| where $Y = 1$ | 0.0345W | | | | | | |
| | | | | | | | |
| q-AB, e | etc = the design flow | v of moveme | ent AB, etc | | | | |
| | etc = the design flow ajor road width | v of moveme | ent AB, etc | | | | |
| W = ma | _ | | ent AB, etc | | | | |
| W = ma W-CR = w-BA, e | ajor road width = central reserve w etc = lane width to v | idth rehicle | | | | | |
| W = ma W-CR = w-BA, e v-rBA, e | ajor road width = central reserve w etc = lane width to v etc = visibility to the | idth /ehicle e right for wa | iiting vehicles in s | | С | | |
| W = ma W-CR = w-BA, e v-rBA, e | ajor road width = central reserve w etc = lane width to v | idth /ehicle e right for wa | iiting vehicles in s | | С | | |
| Ŵ = ma W-CR = w-BA, ∈ v-rBA, ∈ | ajor road width = central reserve w etc = lane width to v etc = visibility to the etc = visibility to the | idth /ehicle e right for wa e left for waiti | iiting vehicles in si ing vehicles in stre | eam BA, etc | | Calcu | lated |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e | ajor road width = central reserve w etc = lane width to v etc = visibility to the etc = visibility to the | idth /ehicle e right for wa | iiting vehicles in si ing vehicles in stre Input | eam BA, etc Input | | Calcu D | lated 0.8536 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e | ajor road width = central reserve w etc = lane width to v etc = visibility to the etc = visibility to the | idth vehicle e right for wa left for waiti nput 17.00 | iiting vehicles in si ing vehicles in stre Input V-rBA 20 | eam BA, etc Input | | _ | |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the | idth vehicle e right for wa left for waiti nput 17.00 | iiting vehicles in si ing vehicles in stre Input V-rBA 20 | eam BA, etc Input w-BA w-BC | 3.80 | D | 0.8536 |
| W = ma W-CR = w-BA, e v-rBA, e v-IBA, e | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the | idth vehicle e right for wa left for waiti nput 17.00 | iiting vehicles in st ing vehicles in stre Input V-rBA 20 V-IBA 25 | eam BA, etc Input w-BA w-BC w-CB | 3.80 3.80 | D E | 0.8536 0.9228 |
| W = ma W-CR = w-BA, e v-rBA, e v-IBA, e Geometry : | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the W W W-CR | idth vehicle e right for wa e left for waiti nput 17.00 0.00 | iting vehicles in streeting vehicles veh | eam BA, etc Input w-BA w-BC w-CB | 3.80 3.80 0.00 | D E F Y | 0.8536 0.9228 0.5860 0.4135 |
| W = ma W-CR = w-BA, e v-rBA, e v-IBA, e Geometry : Analysis : Traffic Flows, | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the W W-CR | idth vehicle e right for wa e left for waiti nput 17.00 0.00 | iting vehicles in streeting vehicles veh | Input w-BA w-BC w-CB pacity, pcu/h | 3.80 3.80 0.00 | D E F Y | 0.8536 0.9228 0.5860 0.4135 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e Geometry : Analysis : Traffic Flows, q-CA | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the W W-CR | idth vehicle e right for wa left for waiti nput 17.00 0.00 PM 0 0 | iting vehicles in streeting vehicles veh | Input w-BA w-BC w-CB pacity, pcu/h Q-BA | 3.80 3.80 0.00 | D E F Y AM 428 | 0.8536 0.9228 0.5860 0.4135 PM 441 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e Geometry : Analysis : Traffic Flows, q-CA q-CB | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the WW-CR | idth vehicle right for wa left for waiti nput 17.00 0.00 PM 0 0 0 | iting vehicles in streeting vehicles veh | Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC | 3.80 3.80 0.00 | D E F Y AM 428 572 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e rolled v-RA, e | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the WW-CR | idth vehicle e right for wa helft for waiti nput 17.00 0.00 PM 0 0 0 0 0 | iting vehicles in streeting vehicles veh | Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC Q-CB | 3.80 3.80 0.00 | D E F Y AM 428 572 363 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 372 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e r-lBA, e v-lBA, e | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the WW-CR | idth vehicle right for wa left for waiti nput 17.00 0.00 PM 0 0 0 0 0 0 5 733 | iting vehicles in streeting vehicles veh | Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC | 3.80 3.80 0.00 | D E F Y AM 428 572 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e r-lBA, e Reometry : Analysis : Traffic Flows, q-CA q-CB q-AB q-AC q-BA | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the WW-CR , pcu/hr AM 83 | idth vehicle right for wa left for waiti nput 17.00 0.00 PM 0 0 0 0 0 0 5 733 9 164 | iting vehicles in streeting vehicles veh | Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC Q-CB | 3.80 3.80 0.00 | D E F Y AM 428 572 363 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 372 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e r-lBA, e r-lBA, e | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the WW-CR , pcu/hr AM 83 24 37 | idth vehicle right for wa left for waiti nput 17.00 0.00 PM 0 0 0 0 0 0 5 733 9 164 8 413 | iting vehicles in streeting vehicles veh | Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC Q-CB | 3.80 3.80 0.00 | D E F Y AM 428 572 363 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 372 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e r-lBA, e W-CB q-CA q-CB q-AB q-AC q-BA | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the WW-CR , pcu/hr AM 83 | idth vehicle right for wa left for waiti nput 17.00 0.00 PM 0 0 0 0 0 0 5 733 9 164 8 413 | iting vehicles in streeting vehicles veh | Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC Q-CB | 3.80 3.80 0.00 | D E F Y AM 428 572 363 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 372 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e r-lBA, e v-lBA, e | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the www. WW-CR Apocu/hr AM 83 24 37 0.60 | idth vehicle e right for was left for waitinput 17.00 0.00 PM 0 0 0 0 0 0 5 733 9 164 8 413 3 0.716 | iiting vehicles in streing vehicles vehic | Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC Q-CB Q-BAC | 3.80 3.80 0.00 | D E F Y AM 428 572 363 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 372 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e r-lBA, e v-lBA, e | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the www. WW-CR Apocu/hr AM 83 24 37 0.60 | idth vehicle right for wa left for waiti nput 17.00 0.00 PM 0 0 0 0 0 5 733 9 164 8 413 3 0.716 | ilting vehicles in streeting vehicles veh | eam BA, etc Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC Q-CB Q-BAC | 3.80 3.80 0.00 | D E F Y AM 428 572 363 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 372 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e r-lBA, e v-lBA, e | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the www. WW-CR Apocu/hr AM 83 24 37 0.60 | idth vehicle right for wa left for waiti nput 17.00 0.00 PM 0 0 0 0 5 733 9 164 8 413 3 0.716 of-flow to Ca B-A | iting vehicles in straing vehicles vehicl | eam BA, etc Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC Q-CB Q-BAC PM 0.372 | 3.80 3.80 0.00 | D E F Y AM 428 572 363 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 372 |
| W = ma W-CR = w-BA, e v-rBA, e v-lBA, e r-lBA, e v-lBA, e | ajor road width = central reserve wetc = lane width to vetc = visibility to the etc = visibility to the www. WW-CR Apocu/hr AM 83 24 37 0.60 | idth vehicle right for wa left for waiti nput 17.00 0.00 PM 0 0 0 0 0 5 733 9 164 8 413 3 0.716 | ilting vehicles in streeting vehicles veh | Input w-BA w-BC w-CB pacity, pcu/h Q-BA Q-BC Q-CB Q-BAC PM 0.372 0.705 | 3.80 3.80 0.00 | D E F Y AM 428 572 363 | 0.8536 0.9228 0.5860 0.4135 PM 441 586 372 |



| Daataa V | Wai Yip Street / Ke | | | | | | | |
|--|--|---|--|--|--|----------------------|---|---|
| _ | | Job Numb | |) | Da | te: | 20 / | August 2024 |
| Scenario: <u>\</u> | Without the Propo | sed Redev | velopment | | | | | P. 19 |
| Wai Yip S | treet (Arm C) | | | | | Wai \ | 'ip Street | (Arm A) |
| | · , , | | | | | | • | · · |
| | | | | | | <u> </u> | 801 | <u>1002</u> |
| | ī | . 🗂 | | | | | 835 | <u>733</u> |
| | | 249 | | | * | г | AM | PM |
| | | 164 | | | | L | Aivi | <u>1 1V1</u> |
| | | | Street (Arm B) |) | ı | | | |
| The predictive equa | ations of capacity | of moveme | ent are: | | | | | |
| Q-BA = D[627 + 1] | 14W-CR - Y(0.364 | q-AC + 0. | | 29q-C <i>F</i> | 4 + 0.52q- | CB)] | | |
| Q-BC = E[745 - Y] | • | . /- | | | | | | |
| Q-CB = F[745 - 0] | ` ' ' | , - | E oro: | | | | | |
| The geometric para | ameters represente 4(w-BA - 3.65)][1 - | • | | T U VV | ∩6(\/_I₽ ^ | _ 150\1 | | |
| _ | 4(w-BC - 3.65)][1 - 4(w-BC - 3.65)][1 - | • | , | - 0.00 | OO(V-IDA | - 130)] | | |
| - | 4(w-BC - 3.65)][1 - 4(w-CB - 3.65)][1 - | , | , - | | | | | |
| where $Y = 1 - 0.0$ | , , | . 3.3000(V | | | | | | |
| | = the design flow | of moveme | ent AB, etc | | | | | |
| - | r road width | | | | | | | |
| | | | | | | | | |
| W- $CR = c$ | entral reserve wid | th | | | | | | |
| w-BA, etc | = lane width to ve | hicle | | | | | | |
| w-BA, etc v-rBA, etc | = lane width to ve = visibility to the r | hicle ight for wa | - | | | ; | | |
| w-BA, etc v-rBA, etc | = lane width to ve | hicle ight for wa | - | | | ; | | |
| w-BA, etc v-rBA, etc v-lBA, etc | = lane width to ve = visibility to the r = visibility to the le | hicle ight for wa | - | | | ; | Calcu | llated |
| w-BA, etc v-rBA, etc | = lane width to ve = visibility to the r = visibility to the le Inp W | hicle right for wa eft for wait out 17.90 | ing vehicles in Input V-rBA | stream 0 v | n BA, etc Input v-BA | 0.00 | D | 0.5332 |
| w-BA, etc v-rBA, etc v-lBA, etc | = lane width to ve = visibility to the r = visibility to the le | hicle right for wa eft for wait out 17.90 | ing vehicles in Input V-rBA V-IBA | stream 0 v 0 v | Input V-BA V-BC | 0.00 3.80 | D E | 0.5332 0.9593 |
| w-BA, etc v-rBA, etc v-lBA, etc | = lane width to ve = visibility to the r = visibility to the le Inp W | hicle right for wa eft for wait out 17.90 | Input V-rBA V-IBA V-rBC | o v o w 60 v | n BA, etc Input v-BA | 0.00 | D E F | 0.5332 0.9593 0.5860 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : | = lane width to ve = visibility to the r = visibility to the le Inp W | hicle right for wa eft for wait out 17.90 | ing vehicles in Input V-rBA V-IBA | stream 0 v 0 v | Input V-BA V-BC | 0.00 3.80 | D E | 0.5332 0.9593 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : | = lane width to ve = visibility to the r = visibility to the le Inp W W-CR | hicle right for wa eft for wait out 17.90 1.00 | Input V-rBA V-IBA V-rBC V-rCB | o v 0 v 0 v 60 v | Input v-BA v-BC v-CB | 0.00 3.80 0.00 | D E F Y | 0.5332 0.9593 0.5860 0.3825 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : Analysis : Traffic Flows, po | = lane width to ve = visibility to the r = visibility to the le Inp W W-CR | hicle ight for wa eft for wait out 17.90 1.00 | Input V-rBA V-IBA V-rBC V-rCB | 0 v 0 v 60 v 0 | Input v-BA v-BC v-CB | 0.00 3.80 0.00 | D E F Y | 0.5332 0.9593 0.5860 0.3825 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : Analysis : Traffic Flows, po q-CA | = lane width to ve = visibility to the r = visibility to the le Inp W W-CR cu/hr AM 0 | chicle right for wa eft for wait out 17.90 1.00 PM 0 | Input V-rBA V-IBA V-rBC V-rCB | 0 v 0 v 60 v 0 | Input v-BA v-BC v-CB sity, pcu/hr | 0.00 3.80 0.00 | D E F Y AM 258 | 0.5332 0.9593 0.5860 0.3825 PM 246 |
| w-BA, etc v-rBA, etc v-lBA, etc Geometry : Analysis : Traffic Flows, po q-CA q-CB | = lane width to ve = visibility to the r = visibility to the le Inp W W-CR cu/hr AM 0 0 | chicle right for wa eft for wait out 17.90 1.00 PM 0 | Input V-rBA V-IBA V-rBC V-rCB | 0 v 0 v 60 v 0 Capac Q- Q- | Input v-BA v-BC v-CB sity, pcu/hr BA BC | 0.00 3.80 0.00 | D E F Y AM 258 564 | 0.5332 0.9593 0.5860 0.3825 PM 246 542 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : Analysis : Traffic Flows, po q-CA q-CB q-AB | = lane width to ve = visibility to the r = visibility to the long W W-CR cu/hr AM 0 0 835 | ehicle right for wa eft for wait out 17.90 1.00 PM 0 0 733 | Input V-rBA V-IBA V-rBC V-rCB | 0 v 0 v 60 v 0 Capac Q- Q- Q- | Input v-BA v-BC v-CB sity, pcu/hr BA BC CB | 0.00 3.80 0.00 | D E F Y AM 258 564 303 | 0.5332 0.9593 0.5860 0.3825 PM 246 542 295 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : Analysis : Traffic Flows, po q-CA q-CB q-AB q-AC | = lane width to ve = visibility to the r = visibility to the le Inp W W-CR cu/hr AM 0 0 | chicle right for wa eft for wait out 17.90 1.00 PM 0 | Input V-rBA V-IBA V-rBC V-rCB | 0 v 0 v 60 v 0 Capac Q- Q- Q- | Input v-BA v-BC v-CB sity, pcu/hr BA BC | 0.00 3.80 0.00 | D E F Y AM 258 564 | 0.5332 0.9593 0.5860 0.3825 PM 246 542 |
| w-BA, etc v-rBA, etc v-lBA, etc v-lBA, etc Geometry: Analysis: Traffic Flows, po q-CA q-CB q-AB q-AC q-BA | = lane width to ve = visibility to the r = visibility to the le Inp W W-CR cu/hr AM 0 0 835 801 | ehicle right for wa eft for wait out 17.90 1.00 PM 0 0 733 1002 | Input V-rBA V-IBA V-rBC V-rCB | 0 v 0 v 60 v 0 Capac Q- Q- Q- | Input v-BA v-BC v-CB sity, pcu/hr BA BC CB | 0.00 3.80 0.00 | D E F Y AM 258 564 303 | 0.5332 0.9593 0.5860 0.3825 PM 246 542 295 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : Analysis : Traffic Flows, po q-CA q-CB q-AB q-AC | = lane width to ve = visibility to the r = visibility to the le Inp W W-CR cu/hr AM 0 0 835 801 0 | Phicle right for wait out 17.90 1.00 PM 0 733 1002 0 | Input V-rBA V-IBA V-rBC V-rCB | 0 v 0 v 60 v 0 Capac Q- Q- Q- | Input v-BA v-BC v-CB sity, pcu/hr BA BC CB | 0.00 3.80 0.00 | D E F Y AM 258 564 303 | 0.5332 0.9593 0.5860 0.3825 PM 246 542 295 |
| w-BA, etc v-rBA, etc v-lBA, etc v-lBA, etc v-lBA, etc Geometry: Analysis: Traffic Flows, po q-CA q-CB q-AB q-AC q-BA q-BC | = lane width to ve = visibility to the r = visibility to the le lnr W W-CR cu/hr AM 0 0 835 801 0 249 1.000 | Phicle right for wait right for wait out 17.90 1.00 PM 0 733 1002 0 164 1.000 | ing vehicles in Input V-rBA V-IBA V-rBC V-rCB | 0 v 0 v 60 v 0 Capac Q- Q- Q- Q- | Input v-BA v-BC v-CB sity, pcu/hr BA BC CB | 0.00 3.80 0.00 | D E F Y AM 258 564 303 | 0.5332 0.9593 0.5860 0.3825 PM 246 542 295 |
| w-BA, etc v-rBA, etc v-lBA, etc v-lBA, etc v-lBA, etc Geometry: Analysis: Traffic Flows, po q-CA q-CB q-AB q-AC q-BA q-BC | = lane width to ve = visibility to the r = visibility to the le lnr W W-CR cu/hr AM 0 0 835 801 0 249 1.000 | Phicle right for wait out 17.90 1.00 PM 0 733 1002 0 164 | ing vehicles in Input V-rBA V-IBA V-rBC V-rCB | o v 0 v 60 v 0 Capac Q- Q- Q- | Input v-BA v-BC v-CB sity, pcu/hr BA BC CB BAC | 0.00 3.80 0.00 | D E F Y AM 258 564 303 | 0.5332 0.9593 0.5860 0.3825 PM 246 542 295 |
| w-BA, etc v-rBA, etc v-lBA, etc v-lBA, etc v-lBA, etc analysis: Traffic Flows, po q-CA q-CB q-AB q-AC q-BA q-BC | = lane width to ve = visibility to the r = visibility to the le lnr W W-CR cu/hr AM 0 0 835 801 0 249 1.000 | Phicle right for wait eft for wait out 17.90 1.00 PM 0 733 1002 0 164 1.000 f-flow to Ca | ing vehicles in Input V-rBA V-IBA V-rBC V-rCB Apacity AM | O v 0 v 60 v 0 Capac Q- Q- Q- | Input v-BA v-BC v-CB sity, pcu/hr BA BC CB BAC | 0.00 3.80 0.00 | D E F Y AM 258 564 303 | 0.5332 0.9593 0.5860 0.3825 PM 246 542 295 |
| w-BA, etc v-rBA, etc v-lBA, etc v-lBA, etc v-lBA, etc Analysis: Traffic Flows, po q-CA q-CB q-AB q-AC q-BA q-BC | = lane width to ve = visibility to the r = visibility to the le lnr W W-CR cu/hr AM 0 0 835 801 0 249 1.000 | Phicle right for wait out 17.90 1.00 PM 0 733 1002 0 164 1.000 f-flow to Care | ing vehicles in Input V-rBA V-IBA V-rBC V-rCB apacity AM 0.0 | 0 v 0 v 60 v 0 Capac Q- Q- Q- 1 | Input v-BA v-BC v-CB sity, pcu/hr BA BC CB BAC PM 0.000 | 0.00 3.80 0.00 | D E F Y AM 258 564 303 | 0.5332 0.9593 0.5860 0.3825 PM 246 542 295 |

CKM Asia Limited J7New

| | | Kei Yip Stree | | | | | | |
|---|--|---|---|--------------------------|--|----------------------|---|---|
| ٠. | 2032 | Job Numb | | 360 | Da | ite: | 20 / | August 2024 |
| Scenario: | With the Propos | sed Redevelo | pment | | | | | P. 20 |
| Wai Yip S | Street (Arm C) | | | | | Wai \ | ∕ip Street | (Arm A) |
| | 2 ii 2 2 i (i ii ii i 2 j | | | | | | | (7 7 .) |
| | | | | | | | 801 | 1002 |
| | | ◆¬ | | | | | 856 | <u>751</u> |
| | | | | | ↓ | | • | |
| | | 252 | | | | | AM | <u>PM</u> |
| | | 167 Kai Vin | Street (Arm | B) | | | | |
| | | itei rip | Olleet (Allii | D) | | | | |
| The predictive equ | | | | | | | | |
| $Q-BA = D[627 + C_{-}BC - E[745 - X_{-}]$ | • | • | 44q-AB + 0 | .229q- | CA + 0.52q | -CB)] | | |
| Q-BC = E[745 - Y] Q-CB = F[745 - Q] | • | . /- | | | | | | |
| The geometric para | ` . | / - | F are: | | | | | |
| • | 94(w-BA - 3.65)][| • | | [1 + 0.0 | 0006(V-IBA | - 150)] | | |
| E = [1 + 0.09] | 94(w-BC - 3.65)][| 1 + 0.0009(V | -rBC - 120)] | _ | • | - | | |
| - | 94(w-CB - 3.65)][| 1 + 0.0009(V | -rCB - 120)] | | | | | |
| where $Y = 1 - 0$. | | | 4 A D 4 | | | | | |
| · · | c = the design flo or road width | w of moveme | nt AB, etc | | | | | |
| | n road widin | | | | | | | |
| W-CR = 0 | central reserve v | vidth | | | | | | |
| | central reserve v c = lane width to | | | | | | | |
| w-BA, etc | central reserve w c = lane width to c = visibility to th | vehicle | iting vehicles | s in str | eam BA, et | C | | |
| w-BA, etc v-rBA, etc | c = lane width to | vehicle e right for wai | - | | | С | | |
| w-BA, etc v-rBA, etc v-IBA, etc | c = lane width to c = visibility to th c = visibility to the | vehicle e right for wai e left for waiti | - | | | | Calcu | lated |
| w-BA, etc v-rBA, etc | c = lane width to c = visibility to th c = visibility to the | vehicle e right for wai | ng vehicles Input | | am BA, etc | | Calcu D | lated 0.5332 |
| w-BA, etc v-rBA, etc v-lBA, etc | c = lane width to c = visibility to th c = visibility to the | vehicle e right for wai e left for waitii Input 17.90 R 1.00 | Input V-rBA V-IBA | in stream | am BA, etc Input w-BA w-BC | 0.00 3.80 | D E | 0.5332 0.9593 |
| w-BA, etc v-rBA, etc v-lBA, etc | c = lane width to c = visibility to the c = visibility to the W | vehicle e right for wai e left for waitii Input 17.90 R 1.00 | Input V-rBA V-IBA V-rBC | 0 0 0 60 | am BA, etc Input w-BA | 0.00 | D E F | 0.5332 0.9593 0.5860 |
| w-BA, etc v-rBA, etc v-lBA, etc Geometry : | c = lane width to c = visibility to the c = visibility to the W | vehicle e right for wai e left for waitii Input 17.90 R 1.00 | Input V-rBA V-IBA | in stream | am BA, etc Input w-BA w-BC | 0.00 3.80 | D E | 0.5332 0.9593 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : | c = lane width to c = visibility to the c = visibility to the W W-CF | vehicle e right for wai e left for waitii Input 17.90 R 1.00 | Input V-rBA V-IBA V-rBC | 0 0 0 60 0 | am BA, etc Input w-BA w-BC w-CB | 0.00 3.80 0.00 | D E F Y | 0.5332 0.9593 0.5860 0.3825 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : Analysis : Traffic Flows, p | c = lane width to c = visibility to the c = visibility to the W W-CF | vehicle e right for wai e left for waitii Input 17.90 R 1.00 | Input V-rBA V-IBA V-rBC | 0 0 60 0 | am BA, etc Input w-BA w-BC w-CB acity, pcu/h | 0.00 3.80 0.00 | D E F Y | 0.5332 0.9593 0.5860 0.3825 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : | c = lane width to c = visibility to the c = visibility to the W W-CF | vehicle e right for wai e left for waitii Input 17.90 R 1.00 | Input V-rBA V-IBA V-rBC | 0 0 60 0 Cap | am BA, etc Input w-BA w-BC w-CB | 0.00 3.80 0.00 | D E F Y | 0.5332 0.9593 0.5860 0.3825 |
| w-BA, etc v-rBA, etc v-lBA, etc Geometry : Analysis : Traffic Flows, p q-CA | c = lane width to c = visibility to the c = visibility to the W W-CF | vehicle e right for wai e left for waiti Input 17.90 R 1.00 PM 0 0 | Input V-rBA V-IBA V-rBC | 0 0 60 0 Cap | am BA, etc Input w-BA w-BC w-CB acity, pcu/h Q-BA | 0.00 3.80 0.00 | D E F Y AM 257 | 0.5332 0.9593 0.5860 0.3825 PM 245 |
| w-BA, etc v-rBA, etc v-lBA, etc Geometry : Analysis : Traffic Flows, p q-CA q-CB | c = lane width to c = visibility to the c = visibility to the W W-CF | vehicle e right for waite e left for waite Input 17.90 R 1.00 PM 0 0 0 0 56 751 | Input V-rBA V-IBA V-rBC | 0 0 60 0 Cap | am BA, etc Input w-BA w-BC w-CB acity, pcu/h Q-BA Q-BC | 0.00 3.80 0.00 | D E F Y AM 257 563 | 0.5332 0.9593 0.5860 0.3825 PM 245 541 |
| w-BA, etc v-rBA, etc v-lBA, etc Geometry : Analysis : Traffic Flows, p q-CA q-CB q-AB | c = lane width to c = visibility to the c = visibility to the W W-CF | vehicle e right for waite e left for waite Input 17.90 R 1.00 PM 0 0 0 0 56 751 | Input V-rBA V-IBA V-rBC | 0 0 60 0 Cap | am BA, etc Input w-BA w-BC w-CB acity, pcu/h Q-BA Q-BC Q-CB | 0.00 3.80 0.00 | D E F Y AM 257 563 301 | 0.5332 0.9593 0.5860 0.3825 PM 245 541 294 |
| w-BA, etc v-rBA, etc v-IBA, etc Geometry : Analysis : Traffic Flows, p q-CA q-CB q-AB q-AC | c = lane width to c = visibility to the c = visibility to the W W-CF | vehicle e right for waite e left for waite Input 17.90 R 1.00 PM 0 0 0 0 56 751 01 1002 | Input V-rBA V-IBA V-rBC | 0 0 60 0 Cap | am BA, etc Input w-BA w-BC w-CB acity, pcu/h Q-BA Q-BC Q-CB | 0.00 3.80 0.00 | D E F Y AM 257 563 301 | 0.5332 0.9593 0.5860 0.3825 PM 245 541 294 |
| w-BA, etc v-rBA, etc v-lBA, etc Geometry : Traffic Flows, p q-CA q-CB q-AB q-AC q-BA | c = lane width to c = visibility to the c = visibility to the W W-CF | vehicle e right for waite e left for waite Input 17.90 R 1.00 PM 0 0 0 0 56 751 01 1002 0 0 52 167 | Input V-rBA V-IBA V-rBC | 0 0 60 0 Cap | am BA, etc Input w-BA w-BC w-CB acity, pcu/h Q-BA Q-BC Q-CB | 0.00 3.80 0.00 | D E F Y AM 257 563 301 | 0.5332 0.9593 0.5860 0.3825 PM 245 541 294 |
| w-BA, etc v-rBA, etc v-lBA, etc Geometry : Traffic Flows, p q-CA q-CB q-AB q-AC q-BA q-BC | c = lane width to c = visibility to the c = visibility to the W W-CF | vehicle e right for waite left for waite lnput 17.90 R 1.00 PM 0 0 0 0 56 751 01 1002 0 0 52 167 00 1.000 | Input V-rBA V-IBA V-rBC V-rCB | 0 0 60 0 Cap | am BA, etc Input w-BA w-BC w-CB acity, pcu/h Q-BA Q-BC Q-CB Q-BAC | 0.00 3.80 0.00 | D E F Y AM 257 563 301 | 0.5332 0.9593 0.5860 0.3825 PM 245 541 294 |
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