



Date: 16th July 2024

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Secretary, Town Planning Board 15/F, North Point Government Offices 333 Java Road, North Point, Hong Kong

Dear Sir/Madam,

SECTION 16 APPLICATION TOWN PLANNING ORDINANCE (CHAPTER 131)

PROPOSED RELIGIOUS INSTITUTION (REDEVELOPMENT OF BETHEL BIBLE SEMINARY (BBS) WITH IN-SITU PRESERVATION OF SUN HOK BUILDING) AT 45 - 47 GRAMPIAN ROAD (PART), KOWLOON CITY, KOWLOON, NEW KOWLOON

INLAND LOT NO.1382 (PART)

Planning Application No. A/K18/347

Further Information (6) – Technical Clarifications

Reference is made to the captioned Section 16 planning application. In order to address Transport Department's comments regarding the captioned application, attached please the table of responses-tocomments (R to C) with the following attachment:

Replacement pages of Traffic Impact Assessment

Please be advised that this FI(6) should be exempted from the publication requirement and/or the recounting requirement in accordance with TPB PG-No. 32B since the it does not involve major changes in the assumptions and methodologies, findings and proposed mitigation measures and involves technical clarifications only.

Should you have any queries, please feel free to contact Mr. Endy CHENG at

or myself at

Yours faithfully, FOR AND ON BEHALF OF DeSPACE (INTERNATIONAL) LIMITED

Greg Lam



Proposed "Religious Institution" (Redevelopment of Bethel Bible Seminary with in-situ preservation of Sun Hok Building) at 45-47 Grampian Road, Kowloon City, Kowloon (Planning Application No. A/K18/347)

Proposed "Religious Institution" (Redevelopment of Bethel Bible Seminary with in-situ preservation of Sun Hok Building) at 45-47 Grampian Road, Kowloon City, Kowloon Town Planning Application No. A/K18/347

Response-to-Comment Table (Departmental Comments)

| Departmental Comments | Responses |
|--|---|
| Memo dated 24 June 2024 refers: | |
| (Commissioner For Transport: Mr. LI Hon-yeung, Simon; Tel: 2399 | 2512) |
| Please find below our further comments on the subject FI and RTC from traffic engineering perspective: 1) R-to-C item no. 5 and Para. 4.8.4 - The applicant shall clarify the exact figures of the calculated gueue lengths at the concerned | Table 4.12 of the TIA is updated. Both calculated queue lengths at the concerned section of Nga Tsin Wai Road are 42m for reference and design |
| exact figures of the calculated queue lengths at the concerned section of Nga Tsin Wai Road instead of putting ">30"m on Table 4.12 for reference and design scenarios. Furthermore, the applicant shall also review if other possible improvement measures, say by adjustment of the traffic green times / linkage of | scenarios. Therefore, the impact caused by the proposed development on the queue length is negligible. This section of Nga Tsin Wai Road is bounded by Grampian Road, Junction Road, Man Yuen Mansion and 49-49A Nga Tsin Wai Road, it cannot be |
| the junction concerned and upstream junctions, can potentially alleviate the excessive queue length; | elongated nor widened. By adjusting the green time, the vehicles could queue within the allowable queue length. Please refer to Table 4.13 of the TIA report. |
| 2) Table 6.9 - the pedestrian flows generated / attracted by the | The pedestrian flows were less than 109/103/127 as some people will come |
| proposed development during the peak times at critical section 7 do | to the proposed development by private car and taxi based on the modal |
| not tally with the assumption as stated in para. 6.2.9 where | split. |

Proposed "Religious Institution" (Redevelopment of Bethel Bible Seminary with in-situ preservation of Sun Hok Building) at 45-47 Grampian Road, Kowloon City, Kowloon (Planning Application No. A/K18/347)

| | maximum of 109/103/127 people will come/leave the subject site within 15 minutes during day/noon/evening time; | Anyway, for conservative, assume 100% of people will use bus/PLB and walk to/ from the proposed development. Chapter 6 is updated accordingly. |
|----|---|--|
| 3) | R-to-C item no. 8, the applicant shall supplement swept path analysis to demonstrate the proposed permanent location of the on- street metered parking spaces will not affect the passage of buses / coaches due to close proximity to the existing refuge island, the applicant shall commit to follow up the proposed permanent relocation of the affected on-street metered spaces and undertake all the necessary local consultation, by adding a paragraph under appropriate section of the TIA report. | Swept path are shown in Figures SP-04 to SP-05 . It is noted that the proposed on-street metered parking spaces will not affect the passage of 12m buses / coaches from Dumbarton Road and 11m HGV left turn from Grampian Road. It is noted that as shown in Figure SP-06 , 12m buses / coaches cannot be left turn from Grampian Road to Dumbarton Road at present due to the existing traffic refuge island (even without relocate the parking spaces). Thus, our proposal will not affect the passage of other vehicles. Section 3.5 is added to the TIA to describe the relocation of on-street parking spaces and the applicant will follow up the proposed permanent relocation of the affected on-street metered spaces and undertake all the necessary local consultation. |

3.4.2 It reveals that the proposed development is currently well served by the comprehensive public transport services in the vicinity.

3.5 Relocation of On-street Parking Spaces

- 3.5.1 Due to the provision of new run-in/out at Dumbarton Road, 3 nos. of on-street meter parking spaces will be affected. It is proposed to shift the parking spaces to the right as shown in **Figure RtC 1**.
- 3.5.2 As shown in **Figures SP-01** to **SP-05**, the manoeuvring of the vehicles will not be affect by relocation of the parking spaces. **Figures SP-06** shows that 12m buses / coaches cannot be left turn from Grampian Road to Dumbarton Road at present due to the existing traffic refuge island (even without relocate the parking spaces). Thus, our proposal will not affect the passage of other vehicles.
- 3.5.3 The applicant will follow up the proposed permanent relocation of the affected onstreet metered spaces and undertake all the necessary local consultation.



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| Table 4.12 | Queue Length Analysis of Identified Junctions in 2029 (Design |
|-------------------|---|
|-------------------|---|

| Year) |
|-------|
|-------|

| | | | | | Length of | Calculated Queue Length (m) | | |
|------|-------------------------------------|----------------------|------------------------------------|-------------------|--------------|-----------------------------|------------|--|
| Ref. | Junction | Method of | Direction | | Road Segment | Design S | Scenario | |
| | | Control | | | (m) | AM Peak | PM Peak | |
| | | | Inverness Road (SB) (SRT+RT) | | 288 | 0 | 0 | |
| А | A Dumbarton Road/ Inverness Road | Priority | Dumbarton Road (WI | B)(LR+RT) | 88 | 2 | 2 | |
| | | | Inverness Road (NB) | (SRT+LT) | 80 | 2 | 1 | |
| | | | Dumbarton Road (EE | B)(LR+RT) | 15 | 0 | 0 | |
| В | Dumbarton Road/ Grampian Road | Priority | Dumbarton Road (WI | B)(LR+RT) | 88 | 1 | 1 | |
| | | | Grampian Road (NB |)(LT+RT) | 284 | 6 | 6 | |
| | | | Dumbarton Road (EB |) (LR+RT) | 119 | 30 | 12 | |
| С | Dumbarton Road/ Junction Road | Road/ Road Signal | Junction Road (NE | B) (SRT) | 75 | 54 | 48 | |
| | | | Junction Road (SB)(| SRT+RT) | 55 | 24 | 18 | |
| | | | Carpenter Road (SB) | (LT+RT) | 68 | 36 | 36 | |
| D | Junction Road/ Signal | | Junction Road (NB) | (SRT+RT) | 46 | 36 | 36 | |
| | Carpenter Koau | | Junction Road (SB) | (SRT+LT) | 74 | 60 | 42 | |
| | I D 1/ | | Inverness Road (SB) | (LT+RT) | 288 | 11 | 6 | |
| Е | Nga Tsin Wai | Priority | Nga Tsin Wai Roa (SRT+LT) | ad (EB) | 57 | 0 | 0 | |
| | Koad | | Nga Tsin Wai Road | (SRT+RT) | 75 | 5 | 6 | |
| | | | Grampian Road (SB |)(LT+RT) | 41 | 18 | 12 | |
| | Grampian Road/ | | Grampian Ro (NB)(LT+RT+S | ad SRT) | 84 | 30 | 24 | |
| F | Nga Tsin Wai Road | Vai Signal | Nga Tsin Wai Road (WB) (SRT+RT) | | 30 | 24 | 24 | |
| | | | Nga Tsin Wai Roa (SRT+LT) | ad (EB) | 61 | 30 | 30 | |
| | | | Junction Road (SB) | (LT+RT) | 81 | 42 | 30 | |
| | | | Junction Road (NB) | (LT+SRT) | 50 | 24 | 24 | |
| G | Junction Road/ Nga Tsin Wai | Signal | Nga Tsin Wai Roa (SRT+RT) | d (WB) | 40 | 24 | 30 | |
| | Road | | Nga Tsin Wai Road | Reference Case | 30 | <mark>42</mark> | 30 | |
| | | | (EB) (SRT) | Design Case | 50 | <mark>42</mark> | 30 | |

4.8.4 The assessment results in **Table 4.12** indicate that all queues are queuing within the allowable road segments *except* for the Junction G (East Bound).

- 4.8.5 The queue length for Junction G (East Bound) for the reference case (i.e. without the proposed development) is the same as the queue length for design case. Therefore, the impact caused by the proposed development on the queue length is negligible.
- 4.8.6 In addition, this section of Nga Tsin Wai Road is bounded by Grampian Road, Junction Road, Man Yuen Mansion and 49-49A Nga Tsin Wai Road, it cannot be elongated nor widened. Therefore, the applicant is unable to carry out any mitigation measures that can reduce the queue length.

4.8.7 By adjusting the green time, the vehicles could queue within the allowable queue length.

Table 4.13Queue Length Analysis of Identified Junctions in 2029 withAdjusted Green Time (Design Year)

| | | | | Longth of | Calculated Queue Length (m) | | |
|--------------|--|-----------|------------------------------------|---------------------------|-----------------------------|-------------------------|--|
| D.C. Trutter | Tunation | Method of | Direction | Length of Dood Segment | Design Scenario | | |
| Kel. | Control | | Direction | (m) | AM <mark>Peak</mark> | PM <mark>Peak</mark> | |
| G) | Junction Road/ Nga Tsin Wai Road | Signal | Junction Road (SB) (LT+RT) | <mark>81</mark> | <mark>54</mark> | <mark>36</mark> | |
| | | | Junction Road (NB) (LT+SRT) | <mark>50</mark> | <mark>30</mark> | <mark>30</mark> | |
| | | | Nga Tsin Wai Road (WB) (SRT+RT) | <mark>40</mark> | <mark>24</mark> | <mark>30</mark> | |
| | | | Nga Tsin Wai Road (EB) (SRT) | 30 | 30 | <mark>24</mark> | |



6.2.10 As the nearest MTR stations including both Lok Fu Station and Song Wong Toi Station are out of 500m radius, hence, we assumed the travelers will take either GMB or bus to the MTR station. Hence, the model split is adjusted. The adjusted model split is summarized in the **Table 6.7**.

| | TCS | | | | | | | | | |
|-------------------------|------|-------------------|------------------|--------------------|-----|------|------|-------|--|--|
| | Rail | Franchised Bus | PLB | Private Vehicle | SPB | Taxi | Tram | Ferry | | |
| Modal Split | 30% | 27% | 13% | 12% | 9% | 6% | 2% | 1% | | |
| Adjusted Modal Split | - | <mark>68%</mark> | <mark>33%</mark> | - | - | - | - | • | | |

Table 6.7 Adjusted Model Split

6.2.11 The expected peak hour pedestrian flow to/ from the proposed development, bus and GMB stop are estimated and summarized in is summarized in the below Table 6.8.

| Proposed Development | Period | Peak Hour Pedestrian Flow | Passenger trip related to Bus in AM Peak (68%) | Passenger trip related to GMB in AM Peak (33%) |
|---|-----------|------------------------------|---|---|
| | AM Peak | <mark>109</mark> | 74 (two- way) | 35 (two- way) |
| Bethel Bible Seminary at 45-47 Grampian Road | Noon Peak | 103 | 70 (two- way) | 33 (two- way) |
| | PM Peak | 127 | 86 (two- way) | 41 (two- way) |

Table 6.8 Expected Peak Hour Pedestrian Flow to Bus/ GMB Stops

6.2.12 A separated pedestrian flow table shows the pedestrian generated and attracted by the proposed development only. The detail is also provided and is shown in the **Table 6.9**.

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| Critical Sections | Pedestrian Flow Generated and Attracted by the Proposed Development | | | | | | |
|-------------------|---|-------------------------|-----------------------|--|--|--|--|
| Critical Sections | AM Peak (ped/15 mins) | Noon Peak (ped/15 mins) | PM Peak (ped/15 mins) | | | | |
| 4 | 5 | 5 | 10 | | | | |
| <mark>5</mark> | <mark>5</mark> | <mark>5</mark> | 10 | | | | |
| 6 | <mark>5</mark> | <mark>5</mark> | 10 | | | | |
| 7 | 110 | <mark>105</mark> | <mark>125</mark> | | | | |
| 8 | <mark>30</mark> | 25 | <mark>35</mark> | | | | |
| <mark>9</mark> | <mark>5</mark> | <mark>5</mark> | <mark>10</mark> | | | | |
| <mark>12</mark> | <mark>35</mark> | <mark>30</mark> | <mark>40</mark> | | | | |
| 13 | 20 | 20 | 25 | | | | |
| <mark>14</mark> | <mark>55</mark> | <mark>50</mark> | <mark>65</mark> | | | | |
| <mark>15</mark> | <mark>10</mark> | <mark>10</mark> | <mark>15</mark> | | | | |
| <mark>16</mark> | <mark>5</mark> | <mark>5</mark> | <mark>10</mark> | | | | |
| <mark>17</mark> | <mark>5</mark> | 5 | <mark>10</mark> | | | | |
| <mark>18</mark> | 5 | <mark>5</mark> | <mark>10</mark> | | | | |
| <mark>19</mark> | <mark>5</mark> | <mark>5</mark> | <mark>10</mark> | | | | |
| 20 | 5 | <mark>5</mark> | <mark>10</mark> | | | | |
| 21 | 5 | <mark>5</mark> | <mark>10</mark> | | | | |
| 22 | <mark>5</mark> | <mark>5</mark> | <mark>10</mark> | | | | |
| 23 | 5 | <mark>5</mark> | <mark>10</mark> | | | | |
| 25 | 20 | <mark>15</mark> | <mark>20</mark> | | | | |
| <mark>26</mark> | 5 | <mark>5</mark> | <mark>10</mark> | | | | |
| 27 | 5 | 5 | <mark>10</mark> | | | | |
| 28 | 5 | <mark>5</mark> | <mark>10</mark> | | | | |
| <mark>29</mark> | <mark>5</mark> | <mark>5</mark> | <mark>10</mark> | | | | |
| <mark>30</mark> | 5 | 5 | <mark>10</mark> | | | | |
| 31 | 0 | 0 | 0 | | | | |
| 32 | 20 | <mark>15</mark> | <mark>20</mark> | | | | |
| <mark>34</mark> | 5 | 5 | 5 | | | | |
| 35 | 5 | 5 | 5 | | | | |
| <mark>36</mark> | 5 | 5 | 5 | | | | |
| <mark>40</mark> | 5 | 5 | 5 | | | | |
| 41 | 5 | 5 | 5 | | | | |
| 42 | 5 | 5 | 5 | | | | |
| <mark>48</mark> | 5 | 5 | 10 | | | | |
| 51 | 5 | 5 | 10 | | | | |
| <mark>53</mark> | 5 | 5 | <mark>10</mark> | | | | |
| 55 | 20 | 15 | <mark>20</mark> | | | | |
| <mark>56</mark> | <mark>10</mark> | <mark>10</mark> | <mark>15</mark> | | | | |
| <mark>58</mark> | <mark>20</mark> | 20 | <mark>25</mark> | | | | |

Table 6.9 Pedestrian Flow Generated and Attracted by the Proposed Development

Note :

(1) The pedestrian flow results are demonstrated to the nearest units of 5, 0.



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Table 6.10 Pedestrian Flow Generated and Attracted by the ProposedDevelopment for the Pedestrian Crossing

| Critical Sections | Pedestrian Flow Generated and Attracted by the Proposed Development | | | | | | |
|-------------------|---|-------------------------|-----------------------|--|--|--|--|
| Cifical Sections | AM Peak (ped/15 mins) | Noon Peak (ped/15 mins) | PM Peak (ped/15 mins) | | | | |
| <mark>C2</mark> | <mark>5</mark> | <mark>5</mark> | 10 | | | | |
| <mark>C8</mark> | <mark>5</mark> | <mark>5</mark> | 10 | | | | |
| <mark>C9</mark> | <mark>5</mark> | <mark>5</mark> | <mark>10</mark> | | | | |
| C12 | <mark>5</mark> | <mark>5</mark> | <mark>10</mark> | | | | |
| C13 | <mark>5</mark> | <mark>5</mark> | <mark>5</mark> | | | | |
| <mark>C14</mark> | <mark>5</mark> | <mark>5</mark> | <mark>10</mark> | | | | |
| C17 | 5 | 5 | 10 | | | | |
| <mark>C19</mark> | <mark>5</mark> | 5 | 10 | | | | |
| <mark>C24</mark> | <mark>5</mark> | <mark>5</mark> | <mark>10</mark> | | | | |
| C25 | <mark>10</mark> | <mark>10</mark> | <mark>15</mark> | | | | |
| <mark>C26</mark> | 20 | <mark>20</mark> | <mark>25</mark> | | | | |
| C27 | 20 | <mark>15</mark> | 20 | | | | |

Note :

(1) The pedestrian flow results are demonstrated to the nearest units of 5, 0.

6.2.13 The estimated trips are superimposed to the network, the future pedestrian design flow could be estimated and summarized in **Table 6.11 and Table 6.12**.

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| | | | Design Scenario (with the Proposed Development) in Year 2029 | | | | | | | | |
|----------------------|--|--|--|--|--------|-------------------------------|------------------------------------|-----|-------------------------------|------------------------------------|--------|
| | | | AM Peak Noon Peak PM Peak | | | | | | | | |
| Critical Sections | Total Footpath Width (m) ⁽¹⁾ | Effective Width (m) ⁽²⁾ | Two-way Pedestrian Flow | Two-way Pedestria n Flow Rate | LOS | Two-way Pedestrian Flow | Two-way Pedestrian Flow Rate | LOS | Two-way Pedestrian Flow | Two-way Pedestrian Flow Rate | LOS |
| | . , | | (ped/15 mins) | (ped/min/ m) ⁽³⁾ | | (ped/15 mins) | (ped/min/ m) ⁽³⁾ | | (ped/15 mins) | (ped/min/m) ⁽³⁾ | |
| 1 | 3.1 | 2.6 | 10 | 0.26 | Α | 10 | 0.26 | Α | <mark>10</mark> | <mark>0.26</mark> | Α |
| 2 | 3.3 | 2.8 | <mark>25</mark> | <mark>0.60</mark> | Α | <mark>25</mark> | <mark>0.60</mark> | Α | <mark>30</mark> | <mark>0.71</mark> | Α |
| 3 | 2.9 | 2.4 | 100 | <mark>2.78</mark> | Α | <mark>35</mark> | <mark>0.97</mark> | Α | <mark>25</mark> | <mark>0.69</mark> | Α |
| 4 | 2.6 | 2.1 | 105 | <mark>3.33</mark> | Α | <mark>45</mark> | 1.43 | Α | <mark>45</mark> | <mark>1.43</mark> | Α |
| 5 | 3.3 | 2.3 | 105 | 3.04 | Α | 130 | 3.77 | Α | <mark>55</mark> | 1.59 | Α |
| 6 | 3.3 | 2.8 | 125 | 2.98 | A | 170 | 4.05 | A | 75 | 1.79 | A |
| 7 | 2.9 | 1.9 | 185 | 6.49 | A | 120 | 4.21 | A | 145 | 5.09 | A |
| 8 | 2.6 | 1.0 | 105 | 4.38 | A | 60 60 | 2.50 | A | 85 40 | 3.54 0.05 | A |
| 9 | 3.5 | 2.8 | 70 | 2.38 | A | 55 | 1.45 | A | 40 70 | 0.95 | A |
| 10 | 2.0 | 2.0 | <u>70</u> 40 | 1.07 | A | 25 | 0.60 | A | 10 | 0.28 | A |
| 11 | 2.9 | 2.4 | 145 | 1.11 | A | 170 | 0.09 5.40 | A | 80 | 2.54 | A |
| 12 | 2.0 | 2.1 | 145 | 4.00 5.36 | A | 85 | 2.40 | A | 60 60 | 1.74 | A |
| 13 | 3.3 | 2.3 | 70 | 2.03 | Α Δ | 235 | <u>6.81</u> | Δ | 160 | 4 64 | Α Δ |
| 15 | 2.9 | 1.9 | 165 | 5 79 | A | 75 | 2.63 | A | 80 | 2.81 | A |
| 16 | 2.6 | 1.6 | 165 | 6.88 | A | 80 | 3.33 | A | 60 | 2.50 | A |
| 17 | 3.3 | 2.3 | 150 | 4.35 | A | 60 | 1.74 | A | 85 | 2.46 | A |
| 18 | 3.3 | 2.3 | 130 | 3.77 | Α | <mark>40</mark> | <mark>1.16</mark> | Α | <mark>45</mark> | 1.30 | Α |
| 19 | 2.9 | 1.9 | <mark>165</mark> | <mark>5.79</mark> | Α | 120 | 4.21 | Α | <mark>140</mark> | <mark>4.91</mark> | Α |
| 20 | 2.6 | 1.6 | 110 | <mark>4.58</mark> | Α | <mark>60</mark> | <mark>2.50</mark> | Α | <mark>80</mark> | <mark>3.33</mark> | Α |
| 21 | 3.3 | 2.3 | <mark>150</mark> | <mark>4.35</mark> | Α | <mark>75</mark> | 2.17 | Α | <mark>80</mark> | 2.32 | Α |
| 22 | 3.3 | 2.3 | <mark>190</mark> | 5.51 | Α | <mark>95</mark> | <mark>2.75</mark> | Α | <mark>115</mark> | <mark>3.33</mark> | Α |
| 23 | 2.9 | 1.9 | <mark>75</mark> | 2.63 | Α | 25 | 0.88 | Α | <mark>55</mark> | 1.93 | Α |
| 24 | 2.6 | 2.1 | 55 | 1.75 | Α | 265 | 8.41 | Α | 150 | 4.76 | Α |
| 25 | 3.3 | 2.3 | 60 115 | 1.74 | A | <u>90</u> | 2.61 | A | 105 | 3.04 | A |
| 26 | 3.3 | 2.3 | 115 | 3.33 | A | 210 | 6.09 | A | 210 | 6.09 | A |
| 27 | 2.9 | 1.9 | 130 | 4.50 | A | 230 | 8.07 | A | 240 | 8.42 | A |
| 28 | 2.0 | 1.0 | 95 | 4.38 | A | 105 | 0.75 5.65 | A | 203 | <u>8.34</u> | A |
| 30 | 3.3 | 2.3 | 80 | 2.75 | Α Δ | 195 | 5.65 | Δ | 200 | 5.80 | Α Δ |
| 31 | 2.9 | 1.9 | 115 | 4.04 | A | 145 | 5.09 | A | 50 | 1 75 | A |
| 32 | 2.6 | 1.6 | 130 | 5.42 | A | 190 | 7.92 | A | 135 | 5.63 | A |
| 33 | 3.3 | 2.3 | 190 | 5.51 | Α | 145 | 4.20 | A | 110 | 3.19 | A |
| 34 | 3.3 | 2.3 | 130 | 3.77 | A | 200 | 5.80 | A | <u>160</u> | <mark>4.64</mark> | A |
| 35 | 2.9 | 1.9 | 120 | 4.21 | A | <mark>245</mark> | <mark>8.60</mark> | Α | <mark>330</mark> | 11.58 | A |
| 36 | 2.6 | 1.6 | <mark>195</mark> | <mark>8.13</mark> | A | <mark>355</mark> | 14.79 | A | <mark>425</mark> | 17.71 | B |
| 37 | 3.3 | 2.3 | <mark>95</mark> | <mark>2.75</mark> | Α | 120 | <mark>3.48</mark> | Α | 110 | <mark>3.19</mark> | Α |
| 38 | 3.3 | 2.3 | 190 | 5.51 | Α | 315 | 9.13 | Α | 155 | 4.49 | Α |
| 39 | 2.9 | 1.9 | 115 | 4.04 | A | 220 | 7.72 | A | 300 | 10.53 | A |
| 40 | 2.6 | 1.6 | 190 | 7.92 | A | 210 | 8.75 | A | 185 | 7.71 | A |
| 41 | 3.3 | 2.3 | 200 | 5.80 | A | 370 255 | 10.72 | A | 400 245 | 11.59 | A |
| 42 | 2.5 | 2.3 | 105 | 3.69 | A | 165 | 10.29 5 70 | A | 343 155 | <u>10.00</u> | A |
| 44 | 2.9 | 1.9 | 140 | 5.00 | A | 365 | 15.79 | A | 210 | 8 75 | A A |
| 45 | 3.3 | 2.3 | 45 | 1.30 | A | 165 | 4.78 | A | 155 | 4.49 | Δ |
| 46 | 3.3 | 2.3 | 365 | 10.58 | A | 355 | 10.29 | A | 605 | 17,54 | B |
| 47 | 2.9 | 1.9 | 155 | 5.44 | A | 255 | 8.95 | A | 285 | 10.00 | A |
| 48 | 2.6 | 2.1 | 90 | 2.86 | A | 95 | 3.02 | A | 90 | 2.86 | A |
| 49 | 3.3 | 2.8 | <mark>70</mark> | <mark>1.67</mark> | Α | <mark>75</mark> | <mark>1.79</mark> | Α | 100 | <mark>2.38</mark> | Α |
| 50 | 3.3 | 2.8 | 205 | <mark>4.88</mark> | Α | <mark>90</mark> | <mark>2.14</mark> | Α | <mark>115</mark> | <mark>2.74</mark> | Α |
| 51 | 2.9 | 2.4 | 210 | <mark>5.83</mark> | Α | <mark>155</mark> | <mark>4.31</mark> | Α | <mark>190</mark> | <mark>5.28</mark> | Α |

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| 52 | 2.6 | 1.6 | <mark>180</mark> | <mark>7.50</mark> | Α | <mark>150</mark> | 6.25 | Α | <mark>185</mark> | 7.71 | Α |
|----|-----|-----|------------------|-------------------|---|------------------|-------------------|---|------------------|-------------------|---|
| 53 | 3.3 | 2.8 | <mark>70</mark> | <mark>1.67</mark> | Α | <mark>70</mark> | 1.67 | Α | <mark>65</mark> | 1.55 | Α |
| 54 | 3.3 | 2.3 | 105 | 3.04 | Α | <mark>345</mark> | 10.00 | Α | 235 | <mark>6.81</mark> | Α |
| 55 | 2.9 | 1.9 | 155 | <mark>5.44</mark> | Α | <mark>75</mark> | 2.63 | Α | <mark>90</mark> | <mark>3.16</mark> | Α |
| 56 | 2.6 | 1.6 | <mark>65</mark> | 2.71 | Α | <mark>40</mark> | 1.67 | Α | <mark>35</mark> | <mark>1.46</mark> | Α |
| 57 | 3.3 | 2.8 | <mark>55</mark> | 1.31 | Α | <mark>50</mark> | 1.19 | Α | <mark>60</mark> | 1.43 | Α |
| 58 | 3.3 | 2.3 | <mark>90</mark> | 2.61 | Α | <mark>40</mark> | <mark>1.16</mark> | Α | <mark>55</mark> | <mark>1.59</mark> | Α |
| 59 | 2.9 | 1.9 | <mark>70</mark> | <mark>2.46</mark> | Α | <mark>80</mark> | 2.81 | Α | <mark>70</mark> | <mark>2.46</mark> | Α |
| 60 | 2.6 | 1.6 | <mark>60</mark> | 2.50 | Α | <mark>80</mark> | 3.33 | Α | <mark>60</mark> | 2.50 | Α |
| 61 | 3.3 | 2.3 | <mark>65</mark> | 1.88 | Α | <mark>150</mark> | <mark>4.35</mark> | A | 120 | <mark>3.48</mark> | Α |

Note:

- (1) Clear Width of Street = Street Width between walls and hoardings. For conservative, assume no pedestrian could walk under the hoardings.
- (2) Effective Width = Clear Width Dead Width (There is no shopping frontages along the footpath, and hence assume 0.5m for dead areas for both side T.P.D.M Vol 2 Chapter 3.4 Table 3.4.11.1)
- (3) Pedestrian Flow Rate (ped/min/m) = Peak Hour Pedestrian Flow / 15 min. / Effective Width
- (4) The pedestrian flow results are demonstrated to the nearest units of 5, 0.

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| Year 2029 | | | | | | | | | | | |
|-----------|----------------------|---|-----------------------------|-------------------|---------------------------|-----------------------------|-------------------|---------------------------|-----------------------------|-------------------|--|
| | | Design Scenario(with the Proposed Development) in Year 2029 | | | | | | | | | |
| | Method of Control | AM | Peak (ped/ | /hr) | Noon Peak (ped/hr) | | | PM Peak (ped/hr) | | | |
| Crossing | | Crossing Demand (V) | Crossing Capacity (C) | V/C | Crossing Demand (V) | Crossing Capacity (C) | V/C | Crossing Demand (V) | Crossing Capacity (C) | V/C | |
| C1 | Signalized | <mark>180</mark> | <mark>3475</mark> | 0.05 | <mark>590</mark> | <mark>3420</mark> | 0.17 | <mark>510</mark> | <mark>3475</mark> | 0.15 | |
| C2 | Signalized | <mark>515</mark> | <mark>6490</mark> | <mark>0.08</mark> | 1120 | <mark>6460</mark> | 0.17 | 1225 | <mark>6490</mark> | <mark>0.19</mark> | |
| C3 | Signalized | <mark>400</mark> | <mark>3475</mark> | 0.12 | <mark>800</mark> | <mark>3515</mark> | 0.23 | <mark>690</mark> | <mark>3475</mark> | 0.20 | |
| C4 | Signalized | <mark>495</mark> | <mark>3475</mark> | 0.14 | 1045 | <mark>3515</mark> | 0.30 | <mark>960</mark> | <mark>3475</mark> | 0.28 | |
| C5 | Signalized | <mark>470</mark> | <mark>3730</mark> | 0.13 | 1005 | <mark>3760</mark> | 0.27 | 1515 | <mark>3730</mark> | 0.41 | |
| C6 | Signalized | <mark>280</mark> | <mark>6840</mark> | 0.04 | <mark>850</mark> | <mark>6610</mark> | 0.13 | 1050 | <mark>6840</mark> | 0.15 | |
| C7 | Signalized | <mark>530</mark> | <mark>8500</mark> | 0.06 | <mark>1190</mark> | <mark>8550</mark> | 0.14 | 1430 | <mark>8500</mark> | 0.17 | |
| C8 | Signalized | <mark>140</mark> | <mark>2365</mark> | <mark>0.06</mark> | <mark>75</mark> | <mark>2430</mark> | 0.03 | <mark>90</mark> | <mark>2365</mark> | 0.04 | |
| C9 | Signalized | <mark>230</mark> | 2120 | 0.11 | <mark>405</mark> | <mark>2660</mark> | 0.15 | <mark>305</mark> | 2120 | 0.14 | |
| C10 | Signalized | <mark>90</mark> | <mark>2615</mark> | 0.03 | <mark>70</mark> | <mark>2660</mark> | 0.03 | <mark>55</mark> | <mark>2615</mark> | 0.02 | |
| C11 | Signalized | <mark>455</mark> | <mark>5980</mark> | 0.08 | <mark>365</mark> | <mark>5930</mark> | 0.06 | 325 | <mark>5980</mark> | 0.05 | |
| C12 | Signalized | <mark>140</mark> | <mark>2895</mark> | 0.05 | 120 | <mark>2890</mark> | 0.04 | <mark>160</mark> | <mark>2895</mark> | 0.06 | |
| C13 | Signalized | 200 | <mark>4885</mark> | 0.04 | <mark>360</mark> | <mark>4865</mark> | 0.07 | <mark>350</mark> | <mark>4885</mark> | 0.07 | |
| C14 | Signalized | 120 | <mark>2895</mark> | 0.04 | <mark>140</mark> | <mark>2890</mark> | 0.05 | 205 | <mark>2895</mark> | 0.07 | |
| C15 | Signalized | <mark>375</mark> | <mark>2895</mark> | 0.13 | <mark>490</mark> | <mark>2915</mark> | 0.17 | <mark>405</mark> | <mark>2895</mark> | 0.14 | |
| C16 | Signalized | <mark>165</mark> | 2000 | 0.08 | 120 | 2025 | 0.06 | 130 | 2000 | 0.07 | |
| C17 | Signalized | <mark>290</mark> | <mark>3835</mark> | 0.08 | <mark>340</mark> | <mark>3880</mark> | 0.09 | 280 | <mark>3835</mark> | 0.07 | |
| C18 | Signalized | 225 | 4275 | 0.05 | <mark>705</mark> | 4275 | 0.16 | <mark>635</mark> | 4275 | 0.15 | |
| C19 | Signalized | 205 | <mark>3090</mark> | 0.07 | <mark>665</mark> | <mark>2470</mark> | 0.27 | 625 | <mark>3090</mark> | 0.20 | |
| C20 | Signalized | 250 | 3325 | 0.08 | <mark>710</mark> | 3325 | 0.21 | <mark>660</mark> | <mark>3325</mark> | 0.20 | |
| C21 | Signalized | <mark>285</mark> | 7335 | 0.04 | 110 | 3135 | 0.04 | <mark>90</mark> | 7335 | 0.01 | |
| C22 | Signalized | 275 | <mark>5000</mark> | <mark>0.06</mark> | <mark>310</mark> | <mark>7315</mark> | 0.04 | 325 | <mark>5000</mark> | 0.07 | |
| C23 | Signalized | 235 | <mark>2620</mark> | <mark>0.09</mark> | <mark>75</mark> | <mark>3230</mark> | 0.02 | <mark>110</mark> | <mark>2620</mark> | 0.04 | |
| C24 | Signalized | 200 | <mark>2620</mark> | 0.08 | <mark>170</mark> | <mark>3230</mark> | 0.05 | <mark>190</mark> | <mark>2620</mark> | 0.07 | |
| C25 | Signalized | 215 | <mark>2620</mark> | 0.08 | <mark>190</mark> | <mark>3230</mark> | <mark>0.06</mark> | <mark>130</mark> | <mark>2620</mark> | 0.05 | |
| C26 | Signalized | <mark>50</mark> | <mark>2600</mark> | 0.02 | <mark>140</mark> | <mark>2660</mark> | 0.05 | <mark>90</mark> | <mark>2600</mark> | 0.03 | |
| C27 | Signalized | <mark>255</mark> | <mark>4800</mark> | 0.05 | <mark>770</mark> | <mark>2585</mark> | <mark>0.30</mark> | <mark>430</mark> | <mark>4800</mark> | <mark>0.09</mark> | |
| C28 | Signalized | <mark>115</mark> | <mark>2485</mark> | 0.05 | <mark>55</mark> | <mark>2535</mark> | 0.02 | <mark>55</mark> | <mark>2485</mark> | 0.02 | |
| C29 | Signalized | 170 | <mark>2340</mark> | 0.07 | <mark>35</mark> | <mark>2365</mark> | 0.01 | <mark>65</mark> | <mark>2340</mark> | 0.03 | |

Table 6.12Performance of Critical Pedestrian Crossing in Design Scenario in
Year 2029

6.2.14 From the assessment results in **Tables 6.11 and 6.12**, it is revealed that the concerned sections of footpaths and pedestrian crossings would all operate with LOS A, B and with ample V/C Ratio in peak periods. Therefore, the application is acceptable from the traffic points of view.













| JUNCTION DELAY CA | LCULATION | | Job No: | 23041HK | | C | TA Consul | tants Ltd. | |
|-------------------------------|------------------------------------|---|---|---|--|---|---|------------|--|
| Junction: (G) Nga Tsin Wa | i Road / Junction l | Road | | | | | | | |
| Description: 2029 Design Scen | nario (Peak Hour) | | (With Improve | ment) | | | | | |
| TRRL Method (Transpor | t Road Resear | ch Laboratory | ') | | | | | | |
| | $d = \frac{c}{2(}$ | $\frac{(1 \lambda)^2}{1 \lambda X} + \frac{1}{2}$ | $\frac{X}{2q(1-X)} -0.6$ | 55 (c) $\frac{1}{3}$ X $\overline{q}^{2^{-}}$ | ⁽²⁺⁵ λ) | | | | |
| | where | $d = average \lambda = proport$ | e delay per v tion of the cy | ehicle on the cle which is | e particular a effectively g | rm green for the | phase under | | |
| | : | x = Cycle t $x = Cycle t$ $y = Cycle t$ | eration i.e.f g gree of satur um possible Es where S ime in secor | g/c ation. This flow under t = saturation ids e in seconds | is the ratio of the given sett flow in veh/l | f actual flow ing of signa hour | to the ls and equals | | |
| | q should | be the flow | in vehicles | per second to | o give delay i | n seconds | | | |
| | | | | | | | | | |
| Approach: | Approach Junction Road (SE | | B) (LT+RT) Juntion Roa | | Nga Tsin Wai Road (WB) | | Nga Tsin Wai Road (EB) (SRT) | | |
| rippioaen. | A.M. Peak | P.M. Peak | A.M. Peak | P.M. Peak | A.M. Peak | P.M. Peak | A.M. Peak | P.M. Peak | |
| q (veh/s) | 829 | 638 | 454 | 513 | 371 | 433 | 542 | 429 | |
| g (sec) | 41 | 43 | 41 | 43 | 47 | 35 | 47 | 35 | |
| c (sec) | 120 | 110 | 120 | 110 | 120 | 110 | 120 | 110 | |
| s (veh/hr) | 3,333 | 3,333 | 1,679 | 1,679 | 3,308 | 3,308 | 3,267 | 3,267 | |
| λ | 0.34 | 0.39 | 0.34 | 0.39 | 0.39 | 0.32 | 0.39 | 0.32 | |
| Х | 0.73 | 0.49 | 0.79 | 0.78 | 0.29 | 0.41 | 0.42 | 0.41 | |
| M=qc | 27.64 | 19.48 | 15.14 | 15.66 | 12.36 | 13.24 | 18.06 | 13.11 | |
| Delay | | | (2.24 | | 27.15 | 20.00 | 25.25 | 20.12 | |
| d Investion Dalay (cos) | 36.22 | 25.97 | 42.21 | 34.84 | 25.46 | 30.09 | 21.27 | 30.12 | |
| From TPDM | Vold Table 4.2 | 5 | | | | | | | |
| Average Qu N=q(r/2+d) c | eue N calculate or qr,whichever | ed by the greater | | | where | r = effective req = flow (in sad = average de | ed time me units as r and lay per vehicle | d) | |
| Approach: | Junction Road (SB) (LT+RT) | | Juntion Road (NB) (SRT+LT) | | Nga Tsin Wai Road (WB) (SRT+LT) | | Nga Tsin Wai Road (EB) (SRT) | | |
| / `` | A.M. Peak | P.M. Peak | A.M. Peak | P.M. Peak | A.M. Peak | P.M. Peak | A.M. Peak | P.M. Peak | |
| r (sec) | /9 19 | 67 | /9 10 | 67/ 10 | /3 Q | 15 | /3 | /5 | |
| IN (Ven) | 10 | 14 | 10 | 10 | 0 | y | 1 11 | y | |
| Average Queue length | _ | | | | _ | | | | |