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PLANNING APPLICATION FOR PROPOSED COMPREHENSIVE DEVELOPMENT SCHEME TO INCLUDE WETLAND RESTORATION PROPOSAL AND PROPOSED FILLING OF PONDS/LAND AND EXCAVATION OF LAND IN "OU(CDWRA)" ZONE AT VARIOUS LOTS IN D.D. 104, NORTH OF KAM POK ROAD EAST, POK WAI, YUEN LONG, NEW TERRITORIES

ENVIRONMENTAL ASSESSMENT



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1. INTRODUCTION

1.1 Background

- 1.1.1 Ramboll Hong Kong Ltd. (the Consultant) has been commissioned by the Applicant to conduct this Environmental Assessment (EA) in support of the S16 Planning Application for Proposed Residential Development, North of Kam Pok Road, Nam Sang Wai.
- 1.1.2 The Subject Site is also the subject of a previous planning application under the application no. A/YL-NSW/290 and an EA report (R7229_v6.0) was previously submitted in support of that planning application (Previous EA). Since then, the layout plan of proposed development has been further reviewed taking into account the concerns of AFCD with respect to the layout of proposed wetland restoration area. Compared to the previous scheme in Previous EA, the application boundary in current application remains the same. Thus, this EA serves as an update to the abovementioned previous submitted EA report based on the current revised development scheme as requested by AFCD.

1.2 The Project Location

- 1.2.1 The Subject Site comprises various lots in D.D. 104, north of Kam Pok Road East, Yuen Long, N.T. It is bounded by other residential developments such as Man Yuen Chuen, Merry Garden, Meister House, and existing abandoned ponds and open storage activities (**Figure 1.1** refers). The area of the Subject Site is about 5 ha.
- 1.2.2 The Subject Site currently consists of abandoned ponds, grassland and a few temporary house structures.

1.3 The Project Description

- 1.3.1 The original proposed development scheme comprises 114 units in 108 housing blocks of 3- to 5-storey high (i.e. 89 in the form of 2- to 4-storey on top of 1-level of communal basement carpark and 25 in 2-storey on top of 1-level of carport), two 2storeys clubhouses, vehicle and pedestrian entrance access road, an underground sewage pumping station (SPS) and a proposed wetland restoration area (WRA). Asides from the above, there will be sewers proposed along Kam Pok Road East and Pok Wai South Road for connection to existing Nam Sang Wai SPS, proposed stormwater drains and along Kam Pok Road East and Kam Pok Road, relevant manholes, etc. (Figure **5.2** and **5.3**, refer). The exact alignment and provision of these facilities will be subject to detailed design stage. To respond to AFCD's comments, amendments to the original MLP are hence required. As a result, a net reduction in total no. of units have been reduced to 90 units in 84 housing blocks varying from 2-storeys to 4-storeys on top of 1-level of carport. The revised master layout plan of the proposed development is presented in Figure 1.2, and the schematic floor layouts of the residential houses are presented in Appendix 1.1. The locations and orientation of proposed houses in current MLP and their separation distance to nearby road edge, basically follow that in the original scheme.
- 1.3.2 The entire development is compatible with the existing or planned uses on the adjacent sites.
- 1.3.3 Possible environmental mitigation measures have been explored and recommended for the proposed development, where appropriate. For instance, various measures have been incorporated into the design of current scheme, such as adequate setback distance from site boundary line in accordance with HKPSG requirement; setback distance from proposed on-site sewage pumping station; various noise barriers, single



aspect design, fixed glazing/ blank facade, and parapet walls to alleviate road traffic noise and/ or fixed noise impacts; proper site drainage system with screening facility to control surface runoff from proposed development; on-site sewage pumping station and proposed sewer to convey domestic sewage to existing Nam Sang Wai Sewage Pumping Station during operation stage, etc. Please refer to respective chapters for more details of the proposed mitigation measures.

1.3.4 With the domestic nature and scale of development, small amount of general refuse will be generated during operation phase. With proper storage and daily collection of waste, no adverse environmental impact associated with waste management is anticipated. Standard approach that is widely adopted in other parts of Hong Kong will be adopted for the handling and disposal of any domestic waste generated from proposed development. Proper refuse collection points will be provided, and collection of waste will be arranged by a licensed contractor on regular basis. It is noted that part of the Subject Site may potentially fall within the area of high natural background level of Arsenic in soil. The current proposed development will be a designated project under the Environmental Impact Assessment (EIA) Ordinance under Item P.1 Part 1, Schedule 2 of the EIAO (i.e. a residential development or recreational development, other than New Territories exempted houses within Deep Bay Buffer Zone 2) (Figure 1.1 refers) and a separate EIA study will also be conducted later on. Also, the proposed sewers and manholes under the proposed development would encroach onto an area zoned as Conservation Area on the Nam Sang Wai OZP. Thus, it may constitute another designated element under Item Q.1 Part 1, Schedule 2 of the EIAO in case of open trench excavation. If so, it should be covered in the relevant EIA study. The exact alignment and provision of sewers and manholes will be further reviewed in later detailed design stage. An environmental permit under the EIAO is required before the construction and operation of the proposed development. The presence of high natural background level of Arsenic will be reviewed in later EIA stage.

1.4 Scope

- 1.4.1 The scope of this EA study includes the assessment of the key potential environmental impacts of the proposed development:
 - Air quality impact;
 - Road traffic noise impact;
 - Industrial noise impact; and
 - Water quality impact.

2. AIR QUALITY

2.1 Summary

2.1.1 This Chapter assesses and addresses the potential air quality impacts on the proposed residential development at the Subject Site. The Assessment Area for air quality impact assessment is defined by a distance of 500m from the boundary of the Subject Site. As discussed in Section 1.3.1, the current amendments to MLP only concerns proposed total no. of proposed units, while the separation distance from air sensitive receivers to nearby road edge, remains unchanged as compared with last submitted report.

2.2 Legislation, Standards, Guidelines and Criteria

Hong Kong Planning Standards and Guidelines

2.2.1 Table 3.1 of Chapter 9 (Environment) of Hong Kong Planning Standards and Guidelines (HKPSG) (extracted as **Table 2.1** below) set out the minimum horizontal buffer distance required between kerb side of roads and sensitive uses for different types of road, and the buffer distance required between industrial areas with chimneys and sensitive uses.

Table 2.1 Guidelines on Usage of Open Space Site

Pollution Source	Parameter	Buffer Distance	Permitted Uses	
	Type of Road			
	Trunk Road and	>20m	Active and passive recreation uses	
	Primary	3-20m	Passive recreational uses	
Road and	Distributor	<3m	Amenity areas	
Highways	District Distributor	>10m	Active and passive recreation uses	
Tilgiiways	District Distributor	<10m	Passive recreational uses	
	Local Distributor	>5m	Active and passive recreation uses	
		<5m	Passive recreational uses	
	Under Flyovers		Passive recreational uses	
	Difference in Height between Industrial Chimney Exit and the Site			
	<20m	>200m	Active and passive recreation uses	
		5-200m	Passive recreational uses	
Industrial Areas	20-30m (*)	>100m	Active and passive recreation uses	
industrial Arcas		5-100m	Passive recreational uses	
	30-40m	>50m	Active and passive recreation uses	
		5-50m	Passive recreational uses	
	>40m	>10m	Active and passive recreation uses	
Construction and earth moving	-	<50m	Passive recreational uses	
Activities	-	>50m	Active and passive recreation uses	

Remarks:

- (a) In situations where the height of chimneys is not known, use the set of guidelines marked with an asterisk for preliminary planning purpose and refine as and when more information is available.
- (b) The buffer distance is the horizontal, shortest distance from the boundary of the industrial lot, the position of existing chimneys or the edge of road kerb, to the boundary of open space sites.
- (c) The guidelines are generally applicable to major industrial areas but NOT individual large industrial establishments which are likely to be significant air pollution



- sources. Consult EPD when planning open space sites close to such establishments.
- (d) Amenity areas are permitted in any situation.

Air Pollution Control Ordinance (Cap. 311)

2.2.2 The Air Pollution Control Ordinance (APCO) and its subsidiary regulations provide the statutory control on air pollutants from a variety of sources. The APCO makes provision for abating, prohibiting and controlling emissions of any solid, particulate, liquid, vapour, objectionable odours or gaseous substances into the atmosphere. The whole of the HKSAR has been covered by Air Control Zones. The Hong Kong Air Quality Objectives (AQOs) stipulate maximum acceptable concentration of air pollutants. The Air Pollution Control (Amendment) Ordinance 2021 has come into operation since 1 January 2022 to tighten three AQOs. The prevailing AQOs is shown in **Table 2.2**.

Table 2.2 Hong Kong Air Quality Objectives (AQOs)

Pollutant	Averaging time	Concentration limit [1] (µg/m³)	Number of exceedances allowed per year
Sulphur dioxide, SO ₂	10-minute	500	3
Sulpitul dioxide, 302	24-hour	50	3
Respirable suspended	24-hour	100	9
particulates, RSP (PM ₁₀) [2]	Annual	50	Not applicable
Fine suspended	24-hour	50	35 (18) ^[4]
Particulates, FSP (PM _{2.5}) [3]	Annual	25	Not applicable
Nitrogon diovido NO	1-hour	200	18
Nitrogen dioxide, NO ₂	Annual	40	Not applicable
Ozone, O ₃	8-hour	160	9
Carban manayida CO	1-hour	30,000	0
Carbon monoxide, CO	8-hour	10,000	0
Lead	Annual	0.5	Not applicable

Notes:

- [1] All measurements of the concentration of gaseous air pollutants, i.e., sulphur dioxide, nitrogen dioxide, ozone and carbon monoxide, are to be adjusted to a reference temperature of 293 Kelvin and a reference pressure of 101.325 kilopascal.
- [2] Respirable suspended particulates means suspended particles in air with a nominal aerodynamic diameter of 10 μ m or less.
- [3] Fine suspended particulates means suspended particles in air with a nominal aerodynamic diameter of 2.5 μm or less.
- [4] The number of exceedances allowed per year is revised to 35 under the amended AQOs for 24-hour FSP. However, for Government projects, a more stringent standard shall be applied with the number of allowable exceedances of 18 days per year. The current proposed development is not a government project, thus number of exceedances allowed per year is 35.

Air Pollution Control (Construction Dust) Regulation

2.2.3 According to Section 43 of the APCO, the *Air Pollution Control (Construction Dust)*Regulation has clearly defined the notifiable and regulatory works for achieving the purpose of dust control for a number of activities. The Regulation requires that any notifiable work shall give advance notice to EPD, and the Contractors shall ensure that the notifiable and regulatory works are carried out in accordance with the Schedule of the Regulation. Dust control and suppression measures are also provided in the Schedule.



2.2.4 The proposed construction works for the Project are both regulatory and notifiable works due to activities including material stockpiling and dusty material handling as potential sources of fugitive dust emissions as detailed under Parts I to IV of the Schedule on Dust Control Requirements.

Air Pollution Control (Non-road Mobile Machinery) (Emission) Regulation

2.2.5 The Air Pollution Control (Non-road Mobile Machinery) (Emission) Regulation came into operation on 1 June 2015. Under the Regulation, non-road mobile machinery (NRMMs), except those exempted, are required to comply with the prescribed emission standards. From 1 September 2015, all regulated machines sold or leased for use in Hong Kong must be approved or exempted with a proper label in a prescribed format issued by EPD. Starting from 1 December 2015, only approved or exempted NRMMs with a proper label are allowed to be used in specified activities and locations including construction sites. The Contractor is required to ensure the adopted machines or non-road vehicle under the Project could meet the prescribed emission standards and requirement.

2.3 Baseline Condition

- 2.3.1 The recorded air pollutants concentrations between 2018 and 2022 at EPD's Yuen Long Air Quality Monitoring Station were referenced to provide an indication on past ambient air pollutants level at the Proposed Development. For the purpose of evaluating the operational phase ambient air quality levels, background contributions based on EPD's PATH v2.1 concentration output file are also extracted and presented. The proposed development under current Application falls within Grids (28, 49); and (28, 50) of the PATH system, thus concentration output data in year 2025, which is available in PATH model, is presented. The extracted information is provided in **Appendix 2.1**.
- 2.3.2 The recorded past ambient air pollutants levels complied with the AQO limit except for 8-hour O_3 level in 2018 to 2019 and 2021 to 2022, and the annual NO_2 level from 2018 to 2019. NO_2 is mainly formed from the oxidation of nitric oxide (NO) emitted from fuel combustion. Road traffic emissions may be one of the sources for NO_2 level in Yuen Long. However, the predicted PATH future ambient air quality level including NO_2 would be lower than the AQO limit, except for 8-hour ozone. The operation of the current proposed residential development under this Application will not be an emission source.

2.4 Air Quality Impact Assessment

2.4.1 Since the proposed development is for residential use, there will be no particular air pollution sources anticipated during operation of the proposed development. Standard refuse collection point(s) will be provided and located away from residential dwellings , any existing and planned air sensitive uses of the proposed development as far as possible to minimize any potential odour nuisance. Collection of refuse will be done by licensed contractor on regular basis. Since the proposed residential development is still in early planning stage, the exhaust location of the carpark has not yet been determined. The proposed carpark will be designed and operated to meet the requirements in EPD's ProPECC PN 2/96 on Control of Air Pollution in Car Parks. The exhaust (if any) of the proposed car park shall be located away from any nearby ASRs including the air-sensitive uses of the proposed development as far as possible. The potential air quality impacts affecting the proposed development are identified and discussed below.



Vehicular Emissions

- 2.4.2 Vehicular emissions from the adjacent roads could be a potential source of air pollution affecting the proposed development.
- 2.4.3 The road network in the vicinity of the Subject Site includes only Local Distributor (LD) (e.g. Kam Pok Road East), and rural road (e.g. Kam Pok Road and Castle Peak Road Tam Mei). Confirmation from TD concerning the road types are provided in **Appendix 2.2** for reference. According to the Annual Traffic Census 2022 published by Transport Department (TD), San Tin Highway is an Expressway.
- 2.4.4 According to **Table 2.1**, a buffer distance of >20m is required between the kerb side of an expressway/primary distributor/trunk road and the air sensitive uses. For District Distributor (DD) and LD, the required buffer distances are >10m and >5m, respectively.
- 2.4.5 As discussed above, San Tin Highway is an Expressway. As the proposed development is located more than 20m from San Tin Highway (an Expressway), there shouldn't be any air quality concern. Castle Peak Road - Tam Mi and Kam Pok Road are both classified as a rural road based on TD's view. According to Chapter 3, Volume 2 of Transport Planning and Design Manual (TPDM) issued by Transport Department (TD), District Distributors (DDs) are Roads Linking Districts to the Primary Distributor Roads. In light of this, the nature of Castle Peak Road - Tam Mei is more or less similar to a DD road as it is connecting to San Tin Highway, which is an Expressway. As for Kam Pok Road, according to the TPDM, Local Distributors (LDs) are Roads within Districts linking developments to the District Distributor Roads. Kam Pok Road is connecting to Castle Peak Road - Tam Mei (RR/DD road type) via Kam Pok Road East (which is a LD road type), and that Kam Pok Road has similar road hierarchy unction with Kam Pok Road East (LD road type). In addition, the peak hour traffic flow data (2-ways) at Kam Pok Road is about 240 veh./hr only (Road 5B in Appendix 3.1, refers). Given such low traffic flow, it is considered that the nature of Kam Pok Road is more or less similar to a LD road type from traffic engineering point of view. As the proposed development is located more than 10m away from Castle Peak Road - Tam Mi (DD) and more than 5m away from Kam Pok Road (LD) (which is also physically separated by other uses), these buffer distances have already complied with the requirement set out in the HKPSG. The Subject Site is adjacent to existing Kam Pok Road East as well as an access road connecting to the vehicular entry of the proposed development to west. A setback of more than 5m from edge of Kam Pok Road East (the nearest local distributor) and from the road edge of the access road, has been incorporated into the design to avoid adverse air quality impact due to vehicular emissions (Figure 2.1 refers). Please also refer to **Appendix 2.2** for the road classification confirmed with Transport Department. It is understood that the concerned access road will be a private road thus there is no particular road classification. However, the access road is for access to the Subject Site. According to Chapter 3, Volume 2 of Transport Planning and Design Manual (TPDM) issued by Transport Department (TD), Rural Roads are defined as roads connecting the smaller centres of population or popular recreation areas with major road networks. As advised by Project Traffic Consultant, since the concerned access road will be connecting to Kam Pok Road East, which has been classified as a LD road by TD, and the proposed development (with small centres of population), and the access road connecting to the vehicular entry of the proposed development has similar road function with Kam Pok Road East, it is considered as LD road from traffic engineering point of view. 5m buffer distance is required between the kerb side of Kam Pok Road and the proposed development, as well as between the kerb side of the concerned access road and the proposed development. The access road located to the west of the Subject Site is a no-through road with dead end near the vehicular entry



- of the proposed development. Since adequate setback distance has been allowed from this access road as discussed above, there will be no adverse vehicular emission impact as a result.
- 2.4.6 In view of the above, the vehicular emissions impact from the respective roads is considered insignificant. The Subject Site has incorporated adequate setback distance and can satisfy the above-mentioned buffer distance requirement set out in HKPSG, no adverse air quality impact on the proposed development is therefore anticipated.

Other Odour Sources

- 2.4.7 Based on the desktop review and site surveys conducted in July 2022 and September 2023, no particular air and odour emission sources were identified within 200m radius from the proposed development. The site survey route is indicated in **Figure 2.4**. During the site visit, no particular odour source was detected, and no odour source from the nearby nullahs, including Ngau Tam Mei Drainage Channel and its subsidiary nullahs, and nearby ponds was identified. Ngau Tam Mei Drainage Channel and the nearest nullah are ~140 m and ~4 m respectively from the Subject Site. There are existing ponds within adjacent to the Subject Site. It is noted that a separate EIA study including air and odour impact assessment will also be carried out for the proposed development later on. Since the proposed development constitutes a designated project under the EIAO, a site survey on the area within 500 m from the proposed project site boundary will also be conducted during the EIA stage, as well as a detailed AQIA.
- 2.4.8 A sewage pumping station (SPS) is proposed at the southeast of the Subject Site as shown in Figure 2.2. It may give rise to odour impact. Details of the design of the SPS are not available at this stage, which will be subject to the detailed design stage. The proposed SPS will be underground in the basement and within an enclosed building structure. Thus, no adverse odour impact is anticipated from the SPS. The exhaust point will be equipped with a deodorizer to ensure the exhaust will be deodorized before entering the atmosphere. The exhaust point of the SPS should be designed to direct away from nearby sensitive users. The current design has allowed a separation distance of not less than 15m between the exhaust point of SPS and the nearby sensitive users, as shown in Figure 2.2. Reference has been made to previous approved project, "Outlying Island Sewerage Stage 2 - Upgrading of Cheung Chau Sewage Collection, Treatment and Disposal Facilities (Application No. EIA-219/2013)" $^{\left[1
 ight]}$. According to that project, the odour impact assessment conducted for the Pak She SPS (with a capacity of 42,336 m³/day) has revealed that sensitive receivers with a separation distance varying from 1m up to 68m could meet the relevant criteria for odour level after the implementation of odour removal filtering system (with efficiency Furthermore, according to the Project Profile for "Public Housing Development at Lin Cheung Road Site - Temporary Sewage Pumping Station and Associated Sewer Pipes" (Application No. DIR-239/2014), an odour survey was conducted at existing Cheung Sha Wan Sewage Pumping Station (with design capacity of 456,863 m³/day), which was reported to be equipped with odour removal filtering system with a removal efficiency of 95%. The survey found that no odour could be detected at a location ~10m away from the exhaust vent of that SPS. The exhaust height for the Pak She SPS, according to the above-mentioned EIA report, is at ground floor (\sim 1.5m above ground level), while the above-mentioned Project Profile for Cheung Sha Wan SPS has indicated its exhaust located on G/F as well. Given the similar

^[1] Outlying Island Sewerage Stage 2 - Upgrading of Cheung Chau Sewage Collection, Treatment and Disposal Facilities (EIA-219/2013)", Sections 3.4, 3.9.4 to 3.9.6, Figure 3.4.



nature of the current proposed SPS and the relatively small capacity of the proposed SPS (less than 1,000 m³/day), the separation distance of about 15m from the exhaust point of the proposed SPS to nearby ASRs is considered adequate. The exhaust of current proposed SPS is also expected to be located on ground floor. With the environmental conscious design, adequate separation distance, and recommended odour removal filtering system at the exhaust (with an odour removal efficiency not less than 95%) (removal efficiency of above-mentioned SPS EIA refers), no adverse odour impact from the SPS to the proposed development and other nearby air sensitive receivers is expected. The design of the SPS shall follow the guidelines stipulated in *Environmental Guidance Note for Sewage Pumping Stations which is not a Designated Project* published by EPD.

Industrial Emissions

2.4.9 A review of chimney locations based on EPD's register was carried out. No chimneys were identified within the assessment area. Additional chimney surveys were also conducted in July 2019, August 2019, September 2019, March 2020, June 2020, July 2022 and September 2023 to verify the findings. As no chimneys were identified within the assessment area, no adverse air quality impact on the proposed development related to chimney emissions is anticipated. It is noted that a separate EIA study including air and odour impact assessment will also be carried out for the proposed development later on. A site survey on the area within 500 m from the proposed project site boundary will also be conducted during the EIA stage, as well as a detailed AQIA.

2.5 Construction Dust Impact

- 2.5.1 During construction phase of proposed development, there may be potential construction dust impact. The nearest sensitive receivers will be surrounding village houses/ residential developments such as existing village houses to the east, Merry Garden, Man Yuen Chuen, Royal Camellia, Greenery Garden, Meister House (Figure 2.3 refers). The separation distances between site boundary to the nearest air sensitive receivers (ASRs) at above-mentioned locations varied from 8m to over 116m.
- 2.5.2 The major air quality impact of concern during the construction phase will be the potential fugitive dust emission during site formation stage of proposed development such as excavation and filling works to the proposed formation level as well as construction of proposed wetland area. The major dust emission sources during the construction phase of the proposed development are expected to arise from construction activities such as:
 - Excavation resulting in exposed ground vulnerable to air erosion;
 - Earth moving, loading and unloading of excavated material; and
 - Vehicle movements on haul roads and over the construction site.
- 2.5.3 The current concerned development site is still at its very early planning stage, many construction details are not yet available. It is expected that phased construction should be considered during the earth works in site formation stage with a view to minimize the active works area, although details of construction and its phasing will only available in later detailed design stage. Thus, construction works should be under control and significant construction dust impact is not anticipated. It is noted the proposed development will be subject to a separate Environmental Impact Assessment (EIA) study including a construction phase impact assessment under the EIA Ordinance later on. Concurrent projects, if any, will also be identified and assessed accordingly. Subject to the said assessment results, relevant mitigation measures will be proposed



for implementation to alleviate construction dust impact. The need for the implementation of a construction dust monitoring and audit program is subject to the findings of the EIA study to be conducted in future. Subject to recommendations in the EIA study, this project will follow statutory requirement and an EM&A program during the construction stage will be considered in later detailed design stage to ensure that the nearby ASRs will not be subject to adverse constructional air quality impact. As such, no adverse construction phase impact on the local area due to the proposed development is anticipated.

Other Pollutants Sources

2.5.4 The Air Pollution Control (Fuel Restriction) Regulation controls the fuel to be used by the construction plants such as liquid fuel with a sulphur content not exceeding 0.005% by weight and a viscosity not more than 6 centistokes at 40°C, such as Ultra Low Sulphur Diesel should be used. In addition, emissions from all the regulated machines within construction site will be controlled under the Air Pollution Control (Non-road Mobile Machinery) (Emission) Regulation. Only approved or exempted Non-road Mobile Machinery with a proper label will be allowed to be used at construction site. As such, emissions due to construction equipment will be under control and are unlikely to be significant.

Mitigation Measures for Fugitive Dust Emission

2.5.5 Fugitive dust emission arising from construction activities can be effectively suppressed by incorporating proper mitigation measures into work procedures through contractual clauses, good site management, and close monitoring by the resident engineers. The contractor shall be required to follow the requirements of the Air Pollution Control (Construction Dust) Regulations. The recommended dust mitigation measures are described below.

General Site Management

- 2.5.6 Appropriate working methods should be devised and arranged to minimise dust emissions and to ensure any installed control system and/or measures are operated and/or implemented in accordance with their design merits. No free falling of construction debris should be allowed, which should be let down by hoist or enclosed tunnel to the ground; immediately before leaving the construction site, all vehicles shall be washed to remove any dust materials from its body and wheels; provide site hoarding along site boundary which is next to a road or other public area; higher site hoardings shall be provided for works areas in close proximity to the nearby ASRs (e.g. residential dwelling near Man Yuen Chuen); relocate / arrange dusty construction activities away from the areas close to the ASRs as far as possible; provide effective dust screens, sheeting, or netting to enclose any scaffolding built around the perimeter of a building; prevent placing dusty material storage piles near ASRs; minimizing exposed surface and properly cover stockpile as far as possible and apply frequent watering when working close to the ASRs to supress dust emission; and to explore the flexibility of providing electric power supply for on-site machinery as far as practicable to minimized aerial emissions.
- 2.5.7 Frequent mist/ water spraying should be applied on dusty areas. The frequency of spraying will depend upon local conditions such as rainfall, temperature, wind speed and humidity. The amount of water spraying should be just enough to dampen the material without over-watering which could result in surface water runoff.

Vehicles and Unpaved Site Roads



2.5.8 Dust emission from unpaved roads comes predominantly from travelling of vehicles. Areas within the site where there are regular vehicle movements should have a hard surface such as crushed stone, gravel or other granular materials. Speed controls at an upper limit of 10 km/hr should be imposed and their movements should be confined to designed roadways within the site. All dusty vehicle loads should have side and tail boards covered by tarpaulin sheeting. Wheel-wash troughs and hoses should be provided at exit points of the site.

Material Stockpiling and Handling

2.5.9 The amount of stockpiling should be minimised where possible. Construction material or debris should be covered and stored inside enclosed areas. Other control measures such as enclosed or semi-enclosed windboard should be used, where applicable, to minimise dust emission. Regular watering is needed at areas such as storage piles, where there could be potential dust emission.

Concrete Batching Plant

- 2.5.10 It should be noted that no concrete batching plant is anticipated to be required for the construction of the proposed development at this stage. Should a concrete batching plant be required, in advance of the operation of the plant, a separate assessment shall be conducted and a specified process licence shall be obtained from the authority, which will give guidelines on dust mitigation measures required as terms and conditions, and its implementation will be controlled through the specified process licence.
- 2.5.11 With the adaptation of good practices as mentioned above, it is expected that emission of fugitive construction dust can be minimized and kept at an acceptable level, and adverse air quality impact is unlikely to occur. The proposed development will be the subject of a separate EIA study under the EIA Ordinance, relevant monitoring and audit requirement will be reviewed accordingly. Subject to recommendations of the EIA study, this project will follow statutory requirement and an EM&A programme will be considered in later detailed design stage.

2.6 Conclusion

2.6.1 Adequate peripheral setback from the site boundary should be incorporated into the layout of the proposed development to alleviate the potential vehicular emissions impacts. The proposed development should meet the buffer distance requirements set out in the HKPSG for the proposed uses within the Subject Site. No unacceptable air quality impacts due to vehicular emission are then expected. The proposed SPS will be designed to incorporate mitigation measures such as deodorizers, with a 15m buffer distance between the exhaust point of the SPS and the ASRs. In addition, as no industrial chimney emission sources were identified within 200m from the Subject Site boundary, no unacceptable air quality impacts due to industrial emissions are anticipated. Best practices have been proposed to mitigate construction phase fugitive dust emission. Since the proposed development constitutes a DP, an AQIA is required separately to demonstrate the compliance of the criteria stipulated in the EIAO-TM.



3. TRAFFIC NOISE IMPACT ASSESSMENT

3.1 Introduction

3.1.1 In this assessment, operational phase road traffic noise impact from roads within 300m radius on the proposed development has been assessed. Practicable environmental mitigation measures have been recommended as appropriate.

3.2 Assessment Criteria

3.2.1 Noise standards are recommended in Chapter 9 of the HKPSG for planning against possible road traffic noise impacts. For new dwellings, as in the case of the proposed development within the Subject Site, the maximum allowable road traffic noise level expressed in terms of $L_{10}(1 \text{ hr})$ at the typical façades of the proposed development is recommended to be 70 dB(A).

3.3 Determination of Traffic Noise Sensitive Receivers

3.3.1 The planned residential blocks within the Subject Site are noise sensitive receivers (NSRs) of road traffic noise impact. The proposed residential blocks located closest to the roads would be worst affected, thus selected as the representative NSRs for this road traffic noise impact assessment as the worst-case scenario. The locations and details of the representative NSRs are provided in **Figures 3.1** to **3.4**, and **Table 3.1** below, respectively.

Table 3.1 Representative NSRs for Operational Phase Road Traffic Noise Assessment

NCD	NSD No of Storous	Assessmen	t Level, mPD
NSK	NSR No. of Storeys		evel +1.2m)
A01	4	G/F	6.3
		1/F	9.8
		2/F	13.3
		3/F	16.8
A02	4	G/F	6.3
		1/F	9.8
		2/F	13.3
		3/F	16.8
A03	4	G/F	6.3
		1/F	9.8
		2/F	13.3
		3/F	16.8
A04	4	G/F	6.3
		1/F	9.8
		2/F	13.3
		3/F	16.8
A05	4	G/F	6.3
		1/F	9.8
		2/F	13.3
		3/F	16.8
A06	4	G/F	6.3
		1/F	9.8
		2/F	13.3
		3/F	16.8
B01	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B02	3	G/F	6.3
		1/F	10.8



NCD	No. of Storoug	Assessmen	t Level, mPD
NSR	No. of Storeys	(Ground le	evel +1.2m)
		2/F	15.3
B03	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B04	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B05	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B06	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B07	3	G/F	6.3
		1/F	10.8
	_	2/F	15.3
B08	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B09	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B10	3	G/F	6.3
		1/F	10.8
B11		2/F	15.3
B11	3	G/F	6.3
		1/F	10.8
B.1.0		2/F	15.3
B12	3	G/F	6.3
		1/F	10.8
D12	3	2/F	15.3
B13	3	G/F	6.3
		1/F 2/F	10.8 15.3
D14	3		
B14	3	G/F 1/F	6.3 10.8
		2/F	15.3
B15	3		6.3
D13	3	G/F 1/F	10.8
		2/F	15.3
B16	3	G/F	6.3
D10	3	1/F	10.8
		2/F	15.3
B17	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B18	3	G/F	6.3
	_	1/F	10.8
		2/F	15.3
B20	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B21	3	G/F	6.3
		1/F	10.8
		2/F	15.3
B22	3	Ġ/F	6.3
		1/F	10.8
		2/F	15.3
B23	3	2/F G/F	6.3
•	•		



NCD	No. of Chauses	Assessmen	t Level, mPD
NSR	No. of Storeys	(Ground le	vel +1.2m)
		1/F 2/F	10.8 15.3
B24	3	G/F	6.3
		1/F	10.8
		2/F	15.3
C01	3 [1]	1/F 2/F 1/F	9.8
		2/F 1/F	14.3
C02	3 [1]	1/F	9.8
C03	3 [1]	2/F 1/F	14.3 9.8
COS		2/F	14.3
C04	3 [1]	2/F 1/F	9.8
		2/F 1/F	14.3
C05	3 [1]	1/F	9.8
606	3 [1]	2/F 1/F	14.3
C06	3 [1]	1/F 2/F	9.8 14.3
C07	3 [1]	2/F 1/F	9.8
207		2/F	14.3
C08	3 [1]	2/F 1/F	9.8
		2/F 1/F	14.3
C09	3 [1]	1/F	9.8
010	0 [1]	2/F 1/F	14.3
C10	3 [1]	1/F	9.8
C11	3 [1]	2/F	14.3 9.8
CII	311	2/F	14.3
C12	3 [1]	1/F 2/F 1/F	9.8
		2/F 1/F	14.3
C13	3 [1]	1/F	9.8
C1.4	3 [1]	2/F 1/F	14.3
C14	3 (-1)	1/F 2/F	9.8 14.3
C15	3 [1]	1/F	9.8
013			14.3
C16	3 [1]	2/F 1/F	9.8
		2/F	14.3
C17	3 [1]	1/F	9.8
C18	3 [1]	2/F 1/F	14.3 9.8
C16	3 1-1	2/F	14.3
C19	3 [1]	2/F 1/F	9.8
		2/F	14.3
C20	3 [1]	2/F 1/F	9.8
	0.111	2/F	14.3
C21	3 [1]	1/F	9.8
C22	3 [1]	2/F 1/F	14.3 9.8
C22		2/F	14.3
C23	3 [1]	2/F 1/F	9.8
		2/F 1/F	14.3
C24	3 [1]	1/F	9.8
635	3 [1]	2/F 1/F	14.3
C25	3 1-1	1/F	9.8 14.3
D01	2	2/F G/F	6.3
	_	1/F	10.8
D02	2	1/F G/F	6.3
		1/F	10.8



NSR	No. of Storeys		t Level, mPD evel +1.2m)
E01	2	G/F	6.3
		1/F	10.8
E02	2	G/F	6.3
		1/F	10.8
E03	2	G/F	6.3
		G/F 1/F G/F 1/F	10.8
E04	2	G/F	6.3
		1/F	10.8
E05	2	G/F	6.3
		1/F	10.8
E06	2	1/F G/F	6.3
		1/F	10.8
E07	2	1/F G/F	6.3
		1/F G/F	10.8
E08	2	G/F	6.3
		1/F G/F	10.8
E09	2	G/F	6.3
		1/F	10.8
E10	2	G/F	6.3
		1/F	10.8
E11	2	G/F	6.3
		1/F	10.8
E12	2	1/F G/F	6.3
		1/F G/F	10.8
E13	2	G/F	6.3
		1/F	10.8
E14	2	G/F	6.3
		1/F	10.8
E15	2	G/F	6.3
		1/F	10.8
E16	2	G/F	6.3
		1/F	10.8

Notes:

[1] For Unit Type C residential blocks, there are three storeys, but the ground floor is a carport which is not of noise sensitive use. Thus, the ground floor of Unit Type C residential blocks is not considered as a NSR in this assessment.

3.4 Assessment Methodology

- 3.4.1 As discussed in **Section 3.1**, according to HKPSG, the maximum allowable road traffic noise level expressed in terms of $L_{10}(1 \text{ hr})$ at the typical façades of the proposed development is recommended to be 70 dB(A). In this regard, the traffic noise impact assessment below involves the prediction of the maximum hourly L_{10} level at the noise sensitive receivers (NSRs) of the proposed development due to the projected traffic flow from the major roads within 300m from the proposed development (e.g. Kam Pok Road East, Kam Pok Road East, Castle Peak Road Tam Mi and San Tin Highway).
- 3.4.2 The projected peak hour traffic flow data for Year 2040, which is considered to be the worst-case scenario within 15 years upon completion of the current proposed development by 2025, have been adopted for the noise assessment. The methodology for traffic forecast has been endorsed by Transport Department (TD) (See **Appendix 3.1**). The traffic flow data was provided by the Project traffic consultant which has strictly adopted the above-mentioned endorsed methodology for traffic forecast.
- 3.4.3 The UK Department of Transport's procedures "Calculation of Road Traffic Noise" (CRTN) has been used in the prediction of the road traffic noise at the representative NSRs of the proposed development within the Subject Site. The existing topographic



- details, such as the existing village houses near the Subject Site, have been considered in the assessment.
- 3.4.4 The noise prediction has been carried out using the *RoadNoise 2000* software, which is a computerised model developed on the basis of the U.K. Department of Transport's CRTN procedures, and is acceptable to the EPD.

3.5 Prediction and Evaluation of Noise Impacts

- 3.5.1 Details of information on peak hour traffic volume and percentage of heavy vehicle of the road network within the 300m assessment area provided by the Project traffic consultant is presented in **Appendix 3.1**, which represents the worst-case scenario of the projected traffic flows.
- 3.5.2 An assessment on the road traffic noise level at the NSRs based on the above traffic flow data has been conducted. Exiting low noise road surfacing (LNRS) along San Tin Highway has been taken into account. Noise mitigation measures which have already been incorporated in the design of the layout, and considered in the unmitigated scenario include the followings:
 - Setback of residential blocks from the site boundary, behind the non-noisesensitive clubhouse, at the southeast of the Subject Site near the site entrance.
- 3.5.3 Information of existing roadside barriers along Kam Pok Road East has been obtained from Highways Department and included in the assessment as well.
- 3.5.4 As summarised in **Table 3.2**, under the unmitigated scenario, the predicted road traffic noise levels at some NSRs along the eastern side of the Subject Site would exceed the relevant noise criteria of 70 dB(A) by up to 2 dB(A). The detailed unmitigated results are presented in **Appendix 3.2**.

Table 3.2 Summary of Predicted Unmitigated Road Traffic Noise Levels at Representative NSRs

NSR	Predicted Road Traffic Noise Level, L _{10 (1-hour)} , dB(A) ^[1] (Unmitigated)
A01	55 - 67
A02	54 - 57
A03	54 - 57
A04	54 - 57
A05	54 - 57
A06	55 - 58
B01	57 - 62
B02	44 - 62
B03	44 - 62
B04	45 - 63
B05	45 - 64
B06	47 - 65
B07	48 - 66
B08	45 - 66
B09	45 - 66
B10	45 - 66
B11	51 - 64
B12	49 - 64
B13	49 - 64
B14	50 - 64
B15	52 - 67
B16	52 - 70
B17	52 - 70



NSR	Predicted Road Traffic Noise Level, L _{10 (1-hour)} , dB(A) ^[1] (Unmitigated)
B18	52 - 70
B19	52 - 69
B20	52 - 68
B21	52 - 68
B22	51 - 68
B23	51 - 68
B24	52 - 69
C01	57 - 71
C02	55 - 72
C03	48 - 72
C04	48 - 72
C05	48 - <u>71</u>
C06	48 - <u>71</u>
C07	48 - 71
C08	48 - 71
C09	48 - 70
C10	48 - 70
C11	48 - 69
C12	48 - 69
C13	60 - 64
C14	47 - 63
C15	47 - 63
C16	47 - 64
C17	47 - 64
C18	47 - 64
C19	47 - 65
C20	47 - 65
C21	47 - 65
C22	47 - 65
C23	48 - 65
C24	48 - 65
C25	48 - 65
D01	55 - 66
D02	54 - 66
E01	53 - 64
E02	53 - 64
E03	52 - 64
E04	52 - 64
E05	53 - 64
E06	
E07	
E08	
E09	
E10	
E11	
E12	49 - 58 56 - 60
E13	
E14	48 - 58
E15	47 - 57
E16	58 - 66

Notes:

- [1] Bolded and underlined values exceed the noise criteria of 70dB(A).
- 3.5.5 While there are noise exceedances identified at a few NSRs, provision of the following boundary wall/mitigation measures are already incorporated into the design due to other fixed noise sources. As such, these proposed noise mitigation measures are also incorporated and presented in below mitigated scenario for road traffic noise



assessment in order to show compliance with the noise criteria. Incorporation of these proposed noise mitigation measures including the proposed 7.5m to 10.1m high noise barriers in the design of the proposed scheme has been accepted by the Applicant, which is technically feasible as per advice from Project Engineer. Mitigation measures will be incorporated for implementation during the detailed design stage later on:

- A noise barrier of 10.1m high (i.e. 15.2mPD) along a portion of the southwestern boundary of the Subject Site;
- A noise barrier of 9.4m high (i.e. 14.5mPD) along a portion of the southwestern boundary of the Subject Site;
- A noise barrier of 7.9m high (i.e. 13.0mPD) along the southwestern corner of the Subject Site;
- A noise barrier of 7.5m high (i.e. 12.6mPD) along the eastern boundary of the Subject Site;
- A noise barrier of 5.1m high (i.e. 10.2mPD) along a portion of the western boundary of the Subject Site;
- A noise barrier of 4.8m high (i.e. 9.9mPD) along a portion of the southwestern and southern boundary of the Subject Site; and
- Single aspect design has been incorporated, in terms of fixed windows, blank facades, and placing non-noise-sensitive uses along the facades, for the southern façades (directly facing Kam Pok Road East) of residential blocks at the southwest of the Subject Site, i.e. all the Unit Type C residential blocks.
- 3.5.6 The boundary wall/mitigation measures shield the line of sight from the NSRs to the noise sources. The location and extent of the proposed mitigation measures are indicated in **Figure 3.5**, which are adequate to mitigate road traffic noise. The layout plan showing the single aspect design of the Unit Type C residential blocks is present in **Appendix 1.1**.
- 3.5.7 Under the mitigated scenario, those NSRs with identified noise exceedances and those units with single aspect design incorporated, have been assessed to check noise compliance. As seen in the results table, there is no exceedance of the noise criteria at these NSRs. The summary of the road traffic noise impact assessment results is presented in **Table 3.3**, and the details are presented in **Appendix 3.3**.

Table 3.3 Summary of Predicted Mitigated Road Traffic Noise Levels at Representative NSRs

NSR	Predicted Road Traffic Noise Level, L _{10 (1-hour)} , dB(A) (Mitigated)
C01	54 - 60
C02	50 - 58
C03	48 - 58
C04	48 - 58
C05	48 - 58
C06	48 - 58
C07	48 - 58
C08	48 - 58
C09	48 - 70
C10	48 - 70
C11	48 - 69



NSR	Predicted Road Traffic Noise Level, L _{10 (1-hour)} , dB(A) (Mitigated)				
C12	48 - 69				
Remark: Only those NSRs with identified noise exceedances and those units with single aspect					

Remark: Only those NSRs with identified noise exceedances and those units with single aspect design incorporated, have been assessed.

3.6 Conclusion

3.6.1 Noise impacts due to road traffic within 300m radius from the Subject Site have been assessed following the CRTN. With the implementation of the proposed noise mitigation measures in terms of noise barriers and single aspect design, the predicted road traffic noise levels at NSRs within the Subject Site would comply with the relevant noise criteria. With the provision of the recommended mitigation measures, as outlined in Section 3.5.5 above, no adverse or unacceptable traffic noise impact on the proposed development is anticipated.



4. INDUSTRIAL NOISE IMPACT ASSESSMENT

4.1 Introduction

- 4.1.1 In this assessment, potential noise impacts arising from the nearby fixed noise sources within 300m radius on the proposed development has been assessed by general acoustic principle and Technical Memorandum for the Assessment of Noise from Places Other Than Domestic Premises, Public Places or Construction Sites (IND-TM). Practicable environmental mitigation measures would be recommended, where necessary.
- 4.1.2 The proposed sewage pumping station (SPS) at the southeast of the Subject Site will be entirely underground in the basement level and within an enclosed building structure. Therefore, no particular operational noise impact is anticipated from the SPS. For the proposed clubhouse inside the Proposed Development, there will be no fixed plants such as chiller plants or other fixed noise source. Split-type air conditioners will be provided for the two clubhouses. No adverse noise impact from the operation of the clubhouses is therefore anticipated.

4.2 Government Legislation and Standards

Noise Control Ordinance (NCO)

4.2.1 The Noise Control Ordinance (NCO) provides the statutory framework for the control of fixed plant. It defines statutory limits applicable to the fixed plants used during the operational phase of the Project. The Technical Memorandum for the Assessment of Noise from Places other than Domestic Premises, Public Places or Construction Sites (IND-TM) sets the criteria – Acceptable Noise Level (ANL) for governing noise from existing fixed plant / industrial noise sources.

Hong Kong Planning Standards and Guidelines (HKPSG)

- 4.2.2 The NCO requires that noise impacts from existing fixed noise sources shall comply with the Acceptable Noise Levels (ANL) laid down in Table 2 of IND-TM. NSRs are classified according to the Area Sensitivity Rating (AseR). Any NSR shall be assigned an AseR of "C" if it is within 100 m of a zone designated as "Industrial" or "Industrial Estate" on a statutory Outline Zoning Plan, or an AseR of "B" if it is between 100 m and 250 m from such a zone, except for cases which indicate an AseR of "C".
- 4.2.3 As the Subject Site is located in rural area, to be conservative, the AseR of "A" has been adopted and 60 dB(A) will be the noise criteria for day, evening time, and 50 dB(A) for night time. The ANL for AseRs "A" is depicted in **Table 4.1**.

Table 4.1 Relevant Noise Standard for Fixed Noise Sources

Standards	Criteria in Relevant Time Periods	Acceptable Noise Level (ANL)
NCO	Day and Evening (07:00 - 23:00)	60 dB(A)
NCO	Night (23:00 - 07:00)	50 dB(A)

- 4.2.4 The AseRs proposed in this EA are intended for assessment only. Nothing in the EA shall bind the Noise Control Authority in the context of enforcement against any of the fixed noise sources identified and assessed in the future under the NCO.
- 4.2.5 Since the observed fixed noise sources (\$4.3 refers) are existing uses, the ANL criteria is relevant and has been adopted. Field surveys have revealed that no night-time operation at the concerned fixed noise sources, which were closed before 7pm. To be conservative, night-time noise criteria have been referenced in the noise assessment.



4.3 Identification of Potential Noise Impacts

Industrial Noise Sources

4.3.1 Within 300m radius from the boundary of the Subject Site, a few existing open storage activities, including logistic centers, warehouses, open storage sites, have been identified as potential sources of industrial noise. The locations of the potential industrial noise sources are indicated in Figure 4.1. Sheltered structures were observed from the basemap and aerial photos, and during site surveys at the noise sources as indicated in Figure 4.1. These enclosed structure at open storage sites would provide further noise shielding effect. The noise sources during site surveys and details are presented in **Appendix 4.1**. According to the site surveys conducted in July 2019, August 2019, September 2019, March 2020, June 2020, May 2021, July 2021, July 2022, and September 2023, Towngas Open Yard at the south, and Sime Darby Hong Kong Multi Franchise Motor Group at the west have been identified as non-noise sources. For the Towngas Open Yard, it was observed with no particular noisy operation. For Sime Darby Hong Kong Multi Franchise Motor Group, as confirmed with their staff, their operations are inside an enclosed structure without any opening facing the Subject Site, so no particular noise source is identified. As observed during the site visits, the noise sources were found to operate occasionally. There was no night-time operation at the identified fixed noise sources during site surveys (Appendix 4.1 refers). There are other existing village houses as well as residential buildings at Man Yuen Chuen in close vicinity to noise sources S11 and S10 respectively (Figure 4.1 refers). Operation of these noise sources will also need to comply with noise criteria at these existing sensitive uses. Although it is unlikely that all the identified industrial sites will be in operation simultaneously, to be conservative, it has been assumed that all the identified noise sources are in operation at the same time, which also represents a worst case scenario. Noise sources are assumed to operate continuously instead of occasional as observed on-site and all noise sources are regarded as point source. In assessing the noise level, the locations of identified noisy equipment are shown in Figure 4.1. For noise sources S10 and S11, which are in adjacent to the Subject Site, S10a to S10c and S11a to S11b are derived to represent corresponding notional source location with respective to their nearest representative NSRs, which are then adopted for noise assessment as shown in **Figure 4.1**. There are also noted clusters of existing village houses in close proximity to some of the identified fixed noise sources, which are worst affected.

4.4 Determination of Noise Sensitive Receivers and Assessment Points

4.4.1 The planned residential blocks within the Subject Site are noise sensitive receivers (NSRs) of potential industrial noise impact. The proposed residential blocks located closest to the identified industrial noise sources would be worst affected by the noise sources. Therefore, representative assessment points (APs) on the blocks at Subject Site which are located closest to the noise sources are selected for this industrial noise impact assessment as the worst-case scenario. The locations and details of the APs are provided in **Figures 4.2** to **4.5**, and **Table 4.2** below, respectively.

Table 4.2 Assessment Points for Operational Industrial Noise Impact Assessment

NSR	No. of Storeys	АР	Floor	Assessment Level (Ground level +1.2m)
A01	4	A01-01	G	6.3
		A01-11	1	9.8
		A01-21	2	13.3



NSR	No. of	AP	Floor	Assessment Level
NSK	Storeys			(Ground level +1.2m)
		A01-22	2	13.3
		A01-31	3	16.8
		A01-32	3	16.8
•••		A01-33	3	16.8
A02	4	A02-11	1	9.8
		A02-21	2	13.3
		A02-22	2	13.3
		A02-32	3	16.8
A06	4	A02-33	3	16.8
A06	4	A06-21	2	13.3
	-	A06-22	3	13.3
	-	A06-32	3	16.8 16.8
DO6	2	A06-33	1	
B06	2	B06-15 B06-16	1	10.8 10.8
C01	3	C01-11	1	9.8
CUI	3	C01-11	1	9.8
		C01-13	1	9.8
		C01-14 C01-21	2	14.3
C13	3	C13-11	1	9.8
CIJ		C13-12	1	9.8
		C13-13	1	9.8
		C13-14	1	9.8
		C13-21	2	14.3
		C13-22	2	14.3
		C13-23	2	14.3
		C13-24	2	14.3
E13	2	E13-02	G	6.3
	_	E13-12	1	10.8
		E13-13	1	10.8
E19	2	E19-02	G	6.3
		E19-12	1	10.8
		E19-13	1	10.8
E22	3	E22-04	G	6.3
		E22-11	1	10.8
		E22-14	1	10.8
		E22-15	1	10.8
		E22-21	2	15.3
		E22-24	2	15.3
		E22-25	2	15.3
E41	2	E41-02	G	6.3
		E41-13	1	10.8
		E41-14	1	10.8
E41	3	E41-23	2	15.3
		E41-24	2	15.3
E42	3	E42-04	G	6.3
		E42-14	1	10.8
		E42-15	1	10.8
		E42-24	2	15.3
		E42-25	2	15.3
E43	3	E43-14	1	10.8
		E43-15	1	10.8
		E43-24	2	15.3
E44		E43-25	2	15.3
E44	2	E44-03	G	6.3



4.5 Assessment Methodology

- 4.5.1 Information such as locations and types of noise sources, as well as Sound Power Levels (SWLs) of noisy equipment are determined based on site measurement during the operation of concerned open storage sites and general acoustic principal, which are also used for the noise calculation (**Appendix 4.1** refers). Noise measurements were by using Norsonic AS Precision Integration Sound Level Meter Nor139, which complies with International Electrotechnical Commission Publications 651:1979 (Type 1) and 804:1985 (Type 1). The weather condition was good with calm wind condition (<5m/s) during measurement, which satisfies the required criteria. The equipment was properly calibrated immediately prior to and following each measurement by a Norsonic AS calibrator. The noise levels before and after measurement agreed to within 1.0dB. During the noise measurement, the noise level was dominated by the identified noise source.
- 4.5.2 To predict the noise level at the future noise sensitive uses, the following correction factors have been accounted for:
 - Distance correction: based on the shortest horizontal distance between the identified noise sources and the AP, the distance correction is projected based on standard acoustical principle for point source;
 - As observed during the site visits, the noise sources were found to operate
 occasionally. Although it is unlikely that all the identified industrial sources will
 be in operation simultaneously, to be conservative, it has been assumed that all
 the identified noise sources are in operation at the same time, which also
 represents a worst-case scenario. Noise sources are assumed to operate
 continuously instead of in occasion as observed onsite and all noise sources are
 regarded as point source;
 - Façade correction: a +3dB(A) correction is applied to account for noise reflection from façade; and
 - Path difference: path difference is considered in the mitigated scenario for APs exceeding the noise criteria under the unmitigated scenario, and their line of sight to the noise source can be shielded by the proposed noise barrier under the mitigated scenario. It is calculated based on Path Difference Method using the Maekawa equation.
- 4.5.3 Corrected Noise Level (CNL) at the APs of the proposed development can be calculated by applying the above corrections to the measured SWL of the noise sources in accordance with the following formula:

$$CNL = SWL + C_{dist} + C_{fac} + C_{PD}$$
 (for mitigated scenario only)

Where,

CNL is the corrected noise level at the Assessment Point in dB(A)

SWL is the sound power level of the industrial plant in dB(A)

 C_{dist} is the distance correction in dB(A) in accordance with the Technical Memorandum on Noise from Construction Works Other than Percussive Piling.

 C_{fac} is façade correction, +3 dB(A).

CPD is the path difference for mitigated scenario only.



4.6 Prediction and Evaluation of Noise Impacts

Industrial Noise Assessment Results

- 4.6.1 Based on the assumptions mentioned above and information of noise sources in **Section 4.3**, noise level estimation for the selected APs at the Subject Site has been conducted. Noise mitigation measures and higher barriers are also proposed to alleviate potential industrial noise, which have already been incorporated in the design of the layout, and considered in the noise assessment:
 - Single aspect design for the southern façades (directly facing potential industrial noise sources S4 and S5) of residential blocks at the southwest of the Subject Site, such that there would be direct line of sight from sensitive uses of those residential blocks to the potential noise sources;
 - Setback of residential blocks from the site boundary, behind the non-noisesensitive clubhouse, at the southeast of the Subject Site near the site entrance;
 - A noise barrier of 10.1m high (i.e. 15.2mPD) along a portion of the southwestern boundary of the Subject Site;
 - A noise barrier of 9.4m high (i.e. 14.5mPD) along a portion of the southwestern boundary of the Subject Site;
 - A noise barrier of 7.9m high (i.e. 13.0mPD) along the southwestern corner of the Subject Site;
 - A noise barrier of 7.5m high (i.e. 12.6mPD) along the eastern boundary of the Subject Site;
 - A noise barrier of 5.1m high (i.e. 10.2mPD) along a portion of the western boundary of the Subject Site;
 - A noise barrier of 4.8m high (i.e. 9.9mPD) along a portion of the southwestern and southern boundary of the Subject Site;
 - Single aspect design has been incorporated, in terms of fixed windows, blank facades, and placing non-noise-sensitive uses along the facades, for the southern façades (directly facing Kam Pok Road East) of residential blocks at the southwest of the Subject Site, i.e. all the Unit Type C residential blocks;
 - In addition to the above, additional noise mitigation measures such as 1.2m high solid parapet wall at terrace at 2/F and fixed glazing/ blank façade at 2/F at houses labelled D01, E42 to E50 near the eastern boundary, have also been proposed and incorporated (see **Figure 4.6**); and
 - Incorporation of these proposed noise mitigation measures including the proposed 7.5m to 10.1m high noise barriers in the design of the proposed scheme has been accepted by the Applicant, which is technically feasible as per advice from Project Engineer. Mitigation measures will be incorporated for implementation during the detailed design stage later on.
- 4.6.2 The consolidated overall proposed noise mitigation measures for the proposed development including locations and extents of the noise barriers, single aspect design, fixed glazing/ blank facade, and parapet walls are indicated in **Figure 4.6**. With the proposed noise mitigation measures incorporated in the layout, the calculated industrial noise levels at all APs would comply with the noise criteria. With provision



of the recommended mitigation measures above, no adverse or unacceptable industrial noise impact on the proposed development is anticipated.

4.6.3 The predicted industrial noise levels with the above-mentioned noise mitigation measures at the APs are summarised in **Table 4.3**. The details are presented in **Appendix 4.2**. Cross sections showing the lines of sight from some APs to NS with the presence of the proposed noise barrier are presented in **Appendix 4.3**.

Table 4.3 Predicted Noise Levels at APs for Industrial Noise Impact
Assessment

NSR	No. of Storeys	АР	Floor	Assessment Level (Ground level +1.2m)	Criteria, dB(A)	Predicted Noise Level, dB(A)
A01	4	A01-01	G	6.3	50	48
		A01-11	1	10.8	50	47
		A01-21	2	15.3	50	48
		A01-22	2	15.3	50	41
		A01-31	3	19.8	50	47
		A01-32	3	19.8	50	40
		A01-33	3	19.8	50	40
A02	4	A02-11	1	10.8	50	47
		A02-21	2	15.3	50	48
		A02-22	2	15.3	50	42
		A02-32	3	19.8	50	40
		A02-33	3	19.8	50	41
A06	4	A06-21	2	15.3	50	47
7.00		A06-22	2	15.3	50	43
		A06-32	3	19.8	50	44
		A06-33	3	19.8	50	43
B06	2	B06-15	1	10.8	50	48
200	_	B06-16	1	10.8	50	48
C01	3	C01-11	1	9.8	50	48
001		C01-13	1	9.8	50	[2]
		C01-14	1	9.8	50	[2]
		C01-21	2	14.3	50	50
C13	3	C13-11	1	9.8	50	48
010		C13-12	1	9.8	50	39
		C13-13	1	9.8	50	39
		C13-14	1	9.8	50	40
		C13-21	2	14.3	50	48
		C13-22	2	14.3	50	38
		C13-23	2	14.3	50	42
		C13-24	2	14.3	50	43
E13	2	E13-02	G	6.3	50	42
	_	E13-12	1	10.8	50	43
		E13-13	1	10.8	50	49
E19	2	E19-02	G	6.3	50	41
	_	E19-12	1	10.8	50	43
		E19-13	1	10.8	50	49
E22	3	E22-04	G	6.3	50	41
		E22-11	1	10.8	50	43
		E22-14	1	10.8	50	42
		E22-15	1	10.8	50	43
		E22-21	2	15.3	50	49
		E22-24	2	15.3	50	50



NSR	No. of Storeys	АР	Floor	Assessment Level (Ground level +1.2m)	Criteria, dB(A)	Predicted Noise Level, dB(A)
		E22-25	2	15.3	50	50
E41	2	E41-02	G	6.3	50	48
		E41-13	1	10.8	50	48
		E41-14	1	10.8	50	48
E41	3	E41-23	2	15.3	50	48
		E41-24	2	15.3	50	48
E42	3	E42-04	G	6.3	50	47
		E42-14	1	10.8	50	49
		E42-15	1	10.8	50	47
		E42-24	2	15.3	50	49
		E42-25	2	15.3	50	49
E43	2	E43-14	1	10.8	50	48
		E43-15	1	10.8	50	48
		E43-24	2	15.3	50	49
		E43-25	2	15.3	50	49
E44	2	E44-03	G	6.3	50	48

Remarks:

- [1] To be conservative, night-time noise criteria has been referenced.
- [2] Single aspect design has been adopted as a mitigation measure.

4.7 Conclusion

4.7.1 Noise impacts generated from the existing industrial noise sources within 300m radius of the Subject Site have been examined. With the implementation of the proposed noise mitigation measures in terms of noise barriers, single aspect design, solid parapet wall at terrace, and fixed glazing/ blank façade, etc., no adverse industrial noise impact on the proposed development is anticipated.



5. WATER QUALITY IMPACT

5.1 Introduction

5.1.1 This assessment is to identify the potential water quality impact during the construction and operational phases of the proposed development at the Subject Site. The extent of water quality impact assessment was based on an area within 500m radius from the boundary of the Subject Site.

5.2 Assessment Criteria

Water Pollution Control Ordinance

5.2.1 The Water Pollution Control Ordinance (WPCO) provides the major statutory framework to protect and to control the water quality in Hong Kong. According to the Ordinance and its subsidiary legislation, Hong Kong waters are divided into ten Water Control Zones (WCZs). Corresponding statements of Water Quality Objectives (WQOs) are stipulated for different water regimes (marine waters, inland waters, bathing beaches subzones, secondary contact recreation subzones and fish culture subzones) in the WCZ based on their beneficial uses. The Project area is located within Deep Bay WCZ. Key WQOs for river monitoring stations in Deep Bay WCZ is presented in Table 5.1, while the WQOs for Deep Bay WCZ in the Schedule of Cap 358R is also presented in **Appendix 5.1**.

Technical Memorandum

5.2.2 Discharge of effluents are subject to control under the WPCO. The "Technical Memorandum on Standards for Effluents Discharged into Drainage and Sewerage Systems, Inland and Coastal Waters" (TM-DSS) gives guidance on the permissible effluent discharges based on the type of receiving waters (foul sewers, stormwater drains, inland and coastal waters). The limits control the physical, chemical and microbial quality of effluents. Any sewage from the proposed construction and operation activities must comply with the standards for effluents discharged into the foul sewers, inland waters and coastal waters of Deep Bay WCZ, as given in the TM-DSS.

TPB PG No. 12C "Town Planning Board Guidelines for Application for Developments Within Deep Bay Area under Section 16 of Town Planning Ordinance".

5.2.3 As Deep Bay is an ecological sensitive area, a "zero discharge policy" for Deep Bay has been implemented in Deep Bay catchment. Effluents discharged into Deep Bay are required to be properly treated prior to final disposal so as not to cause net increase in pollution load to Deep Bay.

Practice Note

5.2.4 A Professional Persons Environmental Consultative Committee Practice Note (ProPECC PN) was issued by the EPD to provide guidelines for handling and disposal of construction site discharges. The ProPECC PN 2/23 "Construction Site Drainage" provides good practice guidelines for dealing with 10 types of discharge from construction sites. These include surface run-off, groundwater, boring and drilling water, bentonite slurry, water for testing and sterilisation of water retaining structures and water pipes, wastewater from building constructions, acid cleaning, etching and pickling wastewater, and wastewater from site facilities. Practices given in the ProPECC PN 2/23 should be followed as far as possible during construction to minimise the water quality impact due to construction site drainage.



- 5.2.5 The ProPECC PN 1/23 "Drainage Plans subject to Comments by Environmental Protection Department" provides guidelines and practices for handling, treatment and disposal of various effluent discharges to stormwater drains and foul sewers. The design of site drainage and disposal of various site effluents generated within the new development area should follow the relevant guidelines and practices as given in the ProPECC PN 1/23. Best Management Practices (BMPs) for storm water discharge are recommended for the Project to mitigate potential adverse water quality impacts.
 - ETWBTC (Works) No. 5/2005 "Protection of Natural Streams/Rivers from Adverse Impacts Arising from Construction Works".
- 5.2.6 The Technical Circular provides an administrative framework to better protect natural streams/rivers from impacts of construction works. Construction works in adjacent to natural streams/rivers should follow the guidelines and precautionary measures given in the Technical Circular as far as possible.

Table 5.1 Key Water Quality Objectives for River Monitoring Stations in Deep Bay Water Control Zone

Parameter	WQOs
pH range	6.0 - 9.0
Maximum 5-Day Biochemical Oxygen	5
Maximum Chemical Oxygen Demand, mg/L	30
Maximum Annual Median Suspended Solids,	20
Minimum Dissolved Oxygen, mg/L	4

Remark: The above refers to Key WQOs for river monitoring stations in the Northwestern New Territories, River Water Quality in Hong Kong published by EPD (Appendix C refers). Please also refer to **Appendix 5.1** for the list of WQOs for Deep Bay WCZ.

5.3 Water Sensitive Receivers

- 5.3.1 The Subject Site is currently mainly covered by ponds with no engineered drainage system. Currently, surface runoff within the area as well as water ponds are discharged by means of overland flow into drainage ditch to the west of the Site and without any treatment. The nullahs/drainage channels and ponds within the 500m assessment area are identified as the water sensitive receivers (WSRs) for the construction and operation phases of the Project. The Subject Site is partially inside the Wetland Buffer Area (WBA) but falls outside the Wetland Conservation Area (WCA) by about 184m. Ponds within the WBA maybe subject to direct water quality impact from the construction and operation of the Project, while the WCA is subject to indirect water quality impact from the Subject Site as they are separated by other existing uses. In accordance with Nam Sang Wai Outline Zoning Plan (OZP) S/YL-NSW/8 and Kam Tin North OZP S/YL-KTN/11, there are areas zoned as Conservation Area (CA) within the assessment area to the southeast and southwest of the Subject Site. These CA zones are indicated in **Figure 5.1**.
- 5.3.2 During construction of the current proposed WRA which is within Subject Site and during its establishment period, the WRA will form part of a construction site, which is not a WSR. Once the WRA has been fully functional later on, it will become a WSR. During operation, the proposed WRA will be a WSR. In case there will be any discharge from the ponds at WRA, the effluent shall comply with WPCO-TM.



- 5.3.3 The CA zone at the southeast is located at approximately 403m away from the Subject Site, at a higher altitude. It is also separated from the Subject Site by Kam Pok Road East and San Tin Highway. Hence, the CA zone at the southeast is unlikely to be affected by the activities at the Subject Site which is not an identified WSR of proposed development.
- 5.3.4 Some of existing surrounding ponds are abandoned ponds (see **Table 5.2**), thus they may not be a valid WSR of proposed development subject to review during construction phase. Some abandoned ponds within the Subject Site will form part of a construction site and will be filled up, thus they are not WSRs of proposed development. Some of other watercourses to the further north near existing Fairview Park are located at further upstream location and are physically separated from the Subject Site by other existing developments, thus these are not identified as WSRs of proposed development. Please refer to description in **Table 5.2**.
- 5.3.5 For the two CA zones at the southwest, they are located more than 185m away from the Subject Site. They are adjacent to the drainage channel downstream of the Subject Site. They are subject to indirect impact arising from the activities at the Subject Site.
- 5.3.6 Watercourses within 500m assessment area were identified, which are also tabulated in **Table 5.2** and shown in **Figure 5.1**. Identified WSRs of proposed development for both construction and operation phases, are also presented in **Table 5.2**.

Table 5.2 Identified Watercourses and Water Sensitive Receivers

ID	Description	Туре	Status	Estimated Distance to the Subject Site
Identified V	VSRs of Proposed Developme	ent:		
C02	Conservation Area which covers part of Tai Sang Wai and Wing Kei Tsuen	Conservation Area Zone	Existing.	185m
D01	Ngau Tam Mei Drainage Channel	Drainage Channel	Channelised	143m
P03	Ponds in Wing Kei Tsuen	Pond	Abandoned pond (WSR status subject to review)	325m
P04, P05 (part), P07, P08 (part), P10 to P12, P13 (part), P14 (part), P17 (part)	Ponds in Kam Pok Road East	Ponds	abandoned ponds (WSR status subject to review)	in vicinity and up 55m
P19	Pond near Marry Garden House / in Pok Wai Village	Pond	Abandoned pond	24m



ID	Description	Туре	Status	Estimated Distance to the Subject Site			
			(WSR status subject to review)				
P20	Pond near Elite Garden / in Pok Wai Village	Pond	Abandoned pond (WSR status subject to review)	357m			
P21	Pond near Pok Wai Floodwater Pumping Station	Flood storage pond	Existing	209m			
P22, P25	Ponds in Tai Sang Wai	Ponds	Pond / marsh	Over 373m			
P23 - P24, P26 - P27	Ponds in Tai Sang Wai	Ponds	Existing ponds	Over 297m			
P28 - P30	Ponds in Wing Kei Tsuen	Ponds	abandoned ponds (WSR status subject to review)	Over 207m			
P31 - P32, P33 - P35	Ponds in Wing Kei Tsuen	Ponds	Existing ponds	Over 291m			
W01	Nullah along Pok Wai West Road and a small section of Pok Wai Road	Nullah	Channelised	Over 392m			
W02	Drainage ditches connecting Pok Wai Tsuen to Ngau Tam Mei Drainage Channel	Drainage ditches	Existing and unpaved	Over 78m			
W08	Drainage ditches near Man Yuen Chuen	Drainage ditches	Existing and unpaved	4m			
WRA *	Proposed WRA within Subject Site	WRA	Proposed wetland. Only WSR when it is fully functional during its operation.	Within Site			
Watercours	Watercourses Unlikely Affected (NOT Identified WSRs of Proposed Development):						
C01	Conservation Area which covers part of Kai Kung Shan	Conservation Area Zone	Existing, but at a higher altitude.	403m			
P01, P02	Ponds near Ha Chuk Yuen Road	Ponds	Abandoned pond upstream location	Over 346m			



ID	Description	Туре	Status	Estimated Distance to the Subject Site
P05 (part), P06, P08 (part), P09, P13 (part), P14 (part), P17 (part), P15, P16, P18.	Ponds within Subject Site	Ponds	Abandoned ponds form part of construction site of proposed development & to be filled up.	within site boundary
W03	Drainage ditches near Fairview Park	Drainage ditches	Channelised, but at upstream location. Physically separated by other developments.	Over 223m
W04	Nullah near Ha San Wai	Nullah	Channelised, but at upstream location. Physically separated by other developments.	Over 388m
W05	Nullah along Ha San Wai Road	Nullah	Channelised, but at upstream location. Physically separated by other developments.	Over 267m
W06	Roadside drainage ditches along both sides of San Tam Road	Drainage ditches	Channelised, but at upstream location. Physically separated by other developments.	Over 244m
W07	Roadside drainage ditches along both sides of Castle Peak Road – Tam Mi	Drainage ditches	Channelised, but at upstream location. Physically separated by other developments.	Over 158m

Remark: * Proposed WRA within Subject Site (**Figure 1.2** refers). During construction phase and during its establishment period, it will form part of a construction site, thus not a WSR. Once it is fully functional, it becomes a WSR during its operation phase.



5.4 Potential Water Quality Impact

5.4.1 The Subject Site is currently mainly covered by ponds with no engineered drainage system. Currently, surface runoffs within the area as well as water ponds are discharged by means of overland flow into drainage ditch to the west of the Site without any treatment. The potential water quality impacts during the construction phase of the Proposed Development include filling of existing ponds, general construction activities, construction site runoff, and accidental spillage.

Construction Phase

General Construction Activities

- 5.4.2 Various types of construction activities would generate wastewater. They include general cleaning and polishing, wheel washing, dust suppression and utility installation, which would contain high concentrations of suspended solids. Without proper control, these could lead to increase in suspended solids level, as well as increase in turbidity and reduced dissolved oxygen in the nearby watercourses.
- 5.4.3 Wastewater would also be generated from the accumulation of solid waste such as plastic package and construction material, and sewage effluent from the construction workforce during the construction phase. If uncontrolled, they could lead to deterioration in water quality.
- 5.4.4 The Practice Note for Professional Persons (ProPECC Note PN2/23) on Construction Site Drainage provides guidelines on good practice for dealing with discharges from construction sites. It is applicable to this study for control of site runoff and wastewater generated during the construction phase.

Filling of Existing Ponds

- 5.4.5 The existing ponds within Subject Site used to be commercial fishponds. Based on exiting condition, when drain-down of these existing ponds is required due to operational needs, water would be discharged into adjacent existing drainage ditches then to the existing Ngau Tam Mei Drainage Channel and without any treatment.
- 5.4.6 During the construction phase, construction activities will be conducted in phases. The proposed wetland restoration area (WRA) will be created first, before the construction of the residential buildings. The construction activities at the existing abandoned ponds will be scheduled to commence immediately after the dry season as far as possible when the water level is relatively low in the year. Since this project is still at early planning stage, details of construction works are subject to later detailed design stage. Key construction activities to be carried out at WRA area are tabulated below as illustration. Prior to the commencement of the construction, water from the ponds within the WRA extent will be drained to other ponds within the Subject Site for temporary storage. The construction works will be carried out in phases so to avoid discharge where possible. In case there is still water in the WRA extent, the remaining water will, with the consent of the owners of those ponds sought by the Applicant, be transferred to other ponds outside the Subject Site for temporary storage. The chance to drain pond water to the adjacent existing ditches would thus be minimized. With the proposed development, proper drainage system and screening facilities will be provided to treat surface runoff. It is expected that the water is of similar quality as when these ponds were commercial fishponds, so no adverse water quality issue is anticipated. Once the WRA has been created physically, the establishment period for the wetland and relevant planting will take a much longer time to complete in order for it to function. During which, it is still part of a construction site so it is not water



quality sensitive receiver. However, in case the WRA is fully functional later on while there are still construction works at residential development portion, further mitigation measure such as intercepting drains will be provided by the contractor to divert construction runoff away from the established wetland.

Task	Description of Construction Activities
1	Vegetation clearance
2	Draining of pond water to adjacent ponds for temporary storage *
3	Reprofiling at ponds and earth works *
4	Planting and establishment period *
5	Operation of WRA

Remark: The above are key construction activities at WRA areas. Works to be carried out in phases or in pairs. Details are subject to detailed design stage later on.

5.4.7 When the WRA reprofiling and planting are completed, water will be transferred back to the WRA from the temporary storage ponds. Then, the other ponds within the Subject Site will undergo construction/reprofiling. Before the construction / reprofiling, water from the other ponds will be drained to the reprofiled WRA for temporary storage. The reprofiled ponds will be re-filled after the construction has been completed. Any spare water after the re-filling will be absorbed by soakaway mechanism and the chance to drain pond water to drainage ditches would thus be minimized. In case there is still surplus pond water, the pond water will be used on-site for the construction activities such as dust suppression and wheel washing facilities to minimize the water consumption of Project. In case there will be any discharge from the ponds during construction, the effluent shall comply with WPCO-TM.

Construction Site Runoff

- 5.4.8 Site runoff may cause potential water quality impacts. During construction, soil surfaces would be exposed. Site runoff would wash away the soil particles on unpaved lands and areas with the topsoil exposed. This site runoff is characterised by high concentrations of suspended solids. Release of site runoff into the water body directly or via drainage channel could lead to increase in SS levels and turbidity in the nearby water environment. Site runoff may also wash away contaminated soil particles and therefore cause water pollution.
- 5.4.9 Best practice as stipulated in ProPECC Note PN2/23 will be adopted by contractor. As a standard site practice, sufficient site drainage should be provided to collect site runoff for appropriate treatment before discharge. Perimeter drainage should be installed at site perimeter as well as near any watercourses passing through the construction site to avoid polluted construction site runoff from leaving the sites or entering any nearby watercourses or drainage system without appropriate treatment. Silt removal facilities with sufficient capacity, such as sedimentation tanks, should be provided on site to handle all site runoff before discharge.
- 5.4.10 Water pumped out from foundation piling or excavation works would also be discharged into the nearby drainage via silt removal facilities. The Contractor would be required to obtain a license from EPD for discharge to the inland waters. With the



provision of adequate construction site drainage and sediment removal facilities, no unacceptable water quality impacts would be expected.

Accidental Spillage

5.4.11 Site drainage would be well-maintained and good construction practices would be observed to ensure that litter, fuels and solvents are managed, stored and handled properly and do not enter the nearby water streams and coastal water. Therefore, it is expected that no water quality impacts caused by accidental spillage would be generated.

Sewage Effluent from Construction Workforce

- 5.4.12 Sewage effluents will arise from the sanitary facilities provided for the on-site construction workforce. Based on the "Guidelines for Estimating Sewage Flows for Sewage Infrastructure Planning" issued by EPD, the sewage production rate for construction workers is estimated at 0.15 m³ per employee per day. Thus, for every 100 construction workers working simultaneously at the construction site, about 15 m³ of sewage would be generated per day. Sewage would consist of high levels of BOD₅, Ammonia and *E. coli* counts.
- 5.4.13 The sewage would be collected on-site using chemical toilets and be appropriately handled by licensed contractor. No direct discharge of sewage effluent would be allowed. No adverse water quality impact from sewage effluent from construction workforce is expected.

Operation Phase

Surface runoff

- 5.4.14 The Subject Site is currently mainly covered by ponds with no engineered drainage system. Currently, surface runoffs within the area as well as water ponds are discharged by means of overland flow into drainage ditch to the west of the Site without any treatment.
- 5.4.15 During operation, there will be discharge of surface runoff from the proposed development. A proper drainage system would be provided for the proposed development to collect surface runoff for discharge into the drainage via proposed drainage system. The surface runoff will be collected and then discharged via screening facility. There will be no direct discharge without treatment. Mitigation measures have been proposed in **Section 5.6**.

Sewage effluent

- 5.4.16 Domestic sewage from the proposed development would be a major source of water quality impact from the operational phase. Without proper arrangement, sewage may enter the nearby stromwater system or nearby water bodies, resulting in an increase in levels of pollutants such as *E. coli*, suspended solids (SS), and ammonia nitrogen (NH₃-N), etc.
- 5.4.17 The sewage generated from the proposed development will be collected by a properly planned sewage pumping station within Subject Site (with ADWF capacity of about 125 m³/day) to existing Nam Sang Wai Sewage Pumping Station (SPS) via proposed sewer, and will then be conveyed to the existing Yuen Long Sewage Treatment Works (YLSTW) via existing public sewerage network during operation stage as detailed in the separate Sewerage Impact Assessment (SIA) Report. According to the SIA, sewage generation from the Subject Site will take up about 0.30% of the design daily flow of the Nam Sang Wai SPS, and about 0.18% of YLSTW. There should be adequate capacity at the sewerage system to cater for the proposed development. Please also refer to **Figure**



5.2 for the proposed indicative sewerage system. This planned sewerage system will be in place before occupation of proposed development. With this proposed sewerage system in place, there will be no discharge of raw sewage from the proposed development. Thus, no adverse water quality impact is anticipated. Relevant design measures recommended on emergency situation of the proposed SPS have also been proposed in Section 5.6.

Operation and Maintenance of the Proposed WRA

5.4.18 Since there are already existing water ponds within the Subject Site and pond draining is required for such commercial fish ponds, it is expected that the nature of proposed WRA is of similar to existing water ponds during normal operation of WRA. Relevant measures have been proposed in **Section 5.6**.

Leakage of Oil and Grease from Vehicles

5.4.19 For the proposed roads and the underground parking areas inside the Subject Site, proper drainage system will be provided at the proposed development to follow the requirements of ProPECC PN 1/23 and runoff will be discharged via petrol interceptors (Section 5.6.12 refers).

5.5 Mitigation Measures for Construction Phase

Filling of Existing Ponds

5.5.1 As discussed in **Sections 5.4.1** to **5.4.7**, filling of existing ponds and the WRA reprofiling works will be conducted in phases immediately after the dry season as far as possible. Pond water will be drained to other ponds for temporary storage to avoid discharge where possible. With such arrangements, water will be retained in the WRA in the Subject Site. Water loss from the existing abandoned ponds due to the construction activities will be minimized as far as possible, and no discharge of water is anticipated from the construction phase of the proposed development. After the establishment period of WRA, it is fully functional. In case there are still construction works at residential development portion, further mitigation measure such as intercepting drains will be provided by the contractor to divert construction runoff away from the established wetland.

General Construction Activities

5.5.2 The site practices outlined in ProPECC PN 2/23 Construction Site Drainage should be adopted as far as practicable to minimise the potential water quality impacts from various construction activities and construction site runoff. Extra attention should be paid for works areas which are in close proximity to the water sensitive receivers. Reference should be made to relevant best practices and precautionary measures as outlined in the ETWBTC (Works) No. 5/2005 during the course of construction when working in adjacent to watercourse in order to minimize potential impact.

Wheel Washing Facilities

5.5.3 The wheels of all vehicles should be washed before they leave a construction site to ensure no earth, mud, debris and the like is deposited by them on roads. A wheel washing bay should be provided at every site exit if practicable. Wash water should be recycled whenever possible to minimise the generation of wastewater and should have sand and silt removed before discharging into storm drains. The section of construction road between the wheel washing bay and the public road should be paved with backfall to reduce vehicle tracking of soil and to prevent site run-off from entering public road drains.



5.5.4 There will be need for the Contractor to apply to the EPD for a discharge licence for discharge of effluent from the construction site under the WPCO. The discharge quality must meet the requirements specified in the discharge licence. All the runoff and wastewater generated from the works areas should be treated so that it satisfies all the standards listed in the TM-DSS. The beneficial uses of the treated effluent for other on-site activities such as dust suppression, wheel washing and general cleaning etc., can minimise water consumption and reduce the effluent discharge volume. If monitoring of the treated effluent quality from the works areas is required during the construction phase of the Project, the monitoring should be carried out in accordance with the WPCO license.

Wastewater from Solid Waste

- 5.5.5 Debris and refuse generated on-site should be collected, handled and disposed of properly to avoid entering to the nearby watercourses. Stockpiles of cement and other construction materials should be kept covered when not being used.
- 5.5.6 Rubbish and litter from construction sites should also be collected to prevent spreading of rubbish and litter from the site area. It is recommended to clean up the construction waste on a regular basis for good site practice.

Construction Site Runoff

- 5.5.7 In order to meet the requirements of the Technical Memorandum standard under the Water Pollution Control Ordinance, surface runoff from construction sites should be discharged into storm drains via adequately designed sand/silt removal facilities such as sand traps, and sedimentation basins.
- 5.5.8 Exposed slope/soil surfaces should be covered by a tarpaulin or similar material during rainstorms to prevent the washing away of construction materials into any drainage system, watercourses and inshore water. Other measures which are proposed to be implemented before, during, and after rainstorms, as appropriate, are summarized in ProPECC PN 2/23. The surface run-off from construction sites as detailed below shall also be incorporated into the construction site drainage where practicable as an integral part of good practice:
 - Surface run-off from construction sites should be discharged into storm drains
 via adequately designed sand/ silt removal facilities such as sand traps, and
 sediment basins. Channels or earth bunds or sand bag barriers should be
 provided on site to properly direct stormwater to such silt removal facilities.
 Perimeter channels at site boundary should be provided where necessary.
 - Silt removal facilities, channels and manholes should be maintained, and the deposited silt and grit should be removed regularly.
 - Construction work should be programmed to minimize soil excavation works in rainy seasons (April to September). If excavation in soil could not be avoided in these months, temporarily exposed slope surfaces should be covered, and temporary access roads should be protected by crushed stone or gravel, as excavation proceeds.
 - Earthworks final surfaces should be well compacted, and the subsequent permanent work or surface protection should be carried out immediately after the final surfaces are formed.



- Measures should be taken to minimize the ingress of rainwater into trenches. If
 excavation of trenches in wet seasons is necessary, they should be dug and
 backfilled in short sections. Rainwater pumped out from trenches or foundation
 excavations should be discharged into storm drains via silt removal facilities.
- Open stockpiles of construction materials (e.g. aggregates, sand and fill material) on sites should be covered with tarpaulin or similar fabric. Measures should be taken to prevent the washing away of construction materials, soil, silt or debris into any drainage system.
- Manholes (including newly constructed ones) should always be adequately
 covered and temporarily sealed so as to prevent silt, construction materials or
 debris from getting into the drainage system, and to prevent storm run-off from
 getting into foul sewers.
- Precautions should be taken at any time of year when rainstorms are likely;
 actions should be taken when rainstorms are imminent or forecasted, and
 during or after rainstorms.

Accidental Spillage

- 5.5.9 Oils and fuels should only be used and stored in designated areas which have pollution prevention facilities. All fuel tanks and storage areas should be sited on sealed areas to prevent spillage of fuels and solvents to the nearby watercourses. All waste oils and fuels should be collected in designated tanks prior to disposal.
- 5.5.10 Drainage serving an open oil filling point should be connected to storm drains via a petrol interceptor with peak storm bypass.
- 5.5.11 Temporary sewage diversion using an enclosed pipe should be in place for any sewerage upgrading works. In addition, if the sewerage upgrading works are required to be carried out near the existing nullah, control of runoff and drainage from construction works adjacent to inland water should be implemented to prevent high levels of SS from entering the aquatic environment. Measures recommended in ETWB TC (Works) No. 5/2005 "Protection of natural streams/rivers from adverse impacts arising from construction works" should be adopted where applicable.

Sewage Effluent from Construction Workforce

- 5.5.12 Temporary sanitary facilities, such as sufficient chemical toilets, should be employed in the works areas. The toilet facilities should be more than 30 m away from any watercourses. A licensed contractor would be responsible for cleansing and maintenance of the chemical toilets on a regular basis. The number of the temporary sanitary facilities required for the construction sites would be subject to later detailed design, the capacity of the chemical toilets, and contractor's site practices.
- 5.5.13 Notices would be posted at conspicuous locations to remind the workers not to discharge any sewage or wastewater into the nearby environment during the construction phase of the Project. Regular environmental audit on the construction site would be conducted in order to provide an effective control of any malpractices and achieve continual improvement of environmental performance on site.
- 5.5.14 Provided that sewage is not discharged directly into stormwater drain or inland waters and temporary sanitary facilities are used and properly maintained, no adverse water quality impact is anticipated provided good site practice and the recommendation under this section will be implemented properly by the contractor.



5.6 Mitigation Measures for Operation Phase

Surface runoff

- 5.6.1 During the operation phase, proper stormwater drainage system including drainage pipeline will be provided for the Proposed Development to collect stormwater runoff, and discharge through screening facilities following the existing flow regime to the proposed drainage system of the Site, which eventually enters Ngau Tam Mei Drainage Channel (Figure 5.3). There will be no direct discharge without treatment. It is recommended that the drainage system of the development should be designed in such a way that stormwater runoff should be collected and directed towards the site drainage system as far as possible. Standard stormwater drainage system such as road gullies and manhole device will also be provided along the proposed access road and internal roads to remove particles present in stormwater run-off, and discharge into the planned public drainage system. Details of the drainage system and exact alignment will only be available in detailed design stage. As discharge will be conveyed through standard gully grating or trash grille, there will be no uncontrolled discharge of stormwater runoff into the nearby sensitive areas.
- The existing Subject Site is unpaved with no engineered drainage system. Surface runoffs carrying sediment laden within the area are discharged by means of overland flow into nearby drainage ditches without any treatment. With the proposed development, proper drainage system will be in place to collect and treat the surface runoff before any discharge following the existing flow regime. As pollutants contributed by non-point source are often bound or adsorbed onto particles, an effective stormwater management system will be the removal of pollution sources prior to rainstorm and the provision of standard gully grating or trash grille that collect debris or sediment. Regular cleaning and sweeping of road surface/ open areas and prior to occurrence of rainstorm is recommended in order to minimize pollutants in stormwater. Standard gully grating or trash grille that collect debris and sediments should be provided to trap pollutants in stormwater.
- 5.6.3 Stormwater management Best Management Practices (BMPs) as listed out in below paragraphs should be implemented as appropriate to reduce runoff and control the quality of runoff.
- 5.6.4 Exposed surface shall be avoided within the proposed development to minimise soil erosion, thus reduce SS in runoff. The proposed development area should be either paved or covered by plantation.
- 5.6.5 Preliminary screening facilities such as standard gully grating and trash grille, with spacing which is capable of screening large substances such as fallen leaves and rubbish should be provided at the inlet of drainage system. Road gullies with standard design and manhole device and should be incorporated to remove particles present in stormwater run-off. Drainage outlet of any covered car park should be connected to foul sewers via petrol interceptors or similar facilities.
- 5.6.6 Good management measures such as regular road sweeping, and regular inspection, cleansing and maintenance of the screening facilities of the drainage system should be implemented to ensure normal operation of the drainage system and avoid overflow. Additional inspection and cleansing should be carried out before forecasted heavy rainfall.
- 5.6.7 With provision of the planned drainage system and proper implementation of the BMPs, the surface runoff from the proposed development would not give rise to significant water quality impact.



Sewage effluent

- Site so that sewage would be collected and conveyed to existing Nam Sang Wai Sewage Pumping Station via proposed sewers, which will then be conveyed to the existing Yuen long Sewage Treatment Works via existing public sewerage network and existing public Nam Sang Wai Sewage Pumping Station during operation stage. The proposed SPS has a design ADWF of about 125 m³/day. As there will be no direct discharge of sewage to nearby area , no adverse water quality impact is anticipated from sewage generated by the operation of the proposed development. Drainage in covered carparks, covered transport interchange, covered loading and unloading area should be connected to foul sewer via petrol interceptors in accordance with ProPECC PN 1/23. With the provision of the proposed sewerage system, no associated water quality impact is anticipated.
- As discussed above, sewage from the Subject Site will be collected by proposed sewers and SPS for discharge into public sewerage system. Detailed design of the proposed SPS and sewers is only available during later detailed design stage. In case of emergency situation during operation of the proposed SPS, it is proposed that adequate spare parts for the plant will have to be made readily available as well as provision of duty & standby pumps to ensure the operation of the SPS. In addition, measures have also been proposed for emergency such as qualified personnel will be hired to inspect the plant condition and carry out maintenance on a regular basis; equalization tank to provide temporarily storage; and tank away will be provided in case of prolonged outage of SPS for disposal at designated DSD's sewage treatment works. Moreover, twin sewer is proposed in case of maintenance of one of the sewers. With these measures in place, it is considered that the proposed SPS will unlikely cause any adverse water quality impact.

Operation and Maintenance of the Proposed WRA

- 5.6.10 Since there are already existing water ponds within the Subject Site and pond draining is required for such commercial fish ponds, it is expected that the nature of proposed WRA is of similar to existing water ponds. Under normal operation, there will be no discharge from the proposed WRA. Should draining of the WRA is inevitable (e.g. for maintenance purpose or excessive water), the water should be temporarily drained to adjacent ponds so as to avoid discharge. Water in the WRA can also be temporarily drained to adjacent ponds, with the consent of the owners of those ponds sought by the future management party of the Proposed Development, so that discharge of water can be minimized as far as possible. In case there will be any discharge from the ponds, proper pre-treatment should be carried out so that the effluent quality shall comply with WPCO-TM. The discharge should follow the conditions in the effluent discharge licence to be issued and be sited away from natural water stream as much as possible.
- 5.6.11 Currently, there is also discharge of surface runoff at the Subject Site as well as existing ponds, which is directly discharged and untreated. During operation stage, there will be proper drainage system at proposed development to collect and direct surface runoff towards the site drainage system as far as possible. Screening facilities such as standard gully grating and trash grille, with spacing which is capable of screening off large substances such as fallen leaves and rubbish should be provided at the inlet of drainage system/ discharge points. Thus, there will be no direct discharge of surface runoff without treatment, which may affect the WRA. Furthermore, there should be regular cleaning and sweeping of road surface/ open areas as well as prior to occurrence of rainstorm to minimize exposure of pollutants to stormwater.



Leakage of Oil and Grease from Vehicles

5.6.12 Drainages for the proposed roads and the underground parking areas should be connected to foul sewer via petrol interceptors while drainage serving open space should be connected to stormwater drain via screening facilities in accordance with EPD's Practice Note PN 1/23 in order to avoid oil and grease from entering the drainage system.

5.7 Conclusion

- 5.7.1 Surface runoff of stormwater, sewage effluent from the proposed development, and oil leakage from vehicles would be the major sources of water quality impact during the operation of the proposed development. Proper stormwater drainage system with standard screening facilities will be provided to convey the collected drainage to the Ngau Tam Mei Drainage Channel. For the proposed WRA, there will be no discharge under the normal operation. Any maintenance works should be scheduled to be conducted during the dry season or immediately after the dry season as far as possible when the water level is the lowest in the year.
- 5.7.2 For the filling and reprofiling of the existing abandoned ponds, the construction activities should be conducted in phases to avoid water discharge.
- 5.7.3 The sewage generated from the proposed development will be collected by proposed sewers and SPS for discharge into public sewerage system to existing Nam Sang Wai Sewage Pumping Station, and will then conveyed to the existing Yuen long Sewage Treatment Works via existing public sewerage network and existing public Nam Sang Wai Sewage Pumping Station during operation stage. This planned sewerage system will be in place before occupation of proposed development. With this proposed sewerage system in place, there will be no discharge of raw sewage from the proposed development. Thus, no adverse water quality impact is anticipated. Relevant design measures recommended on emergency situation of the proposed SPS, have also been proposed.
- 5.7.4 Provided that mitigation measures such as BMP and provision of appropriately designed drainage and sewerage systems are implemented, adverse water quality impact from the operation of the proposed development is not anticipated.



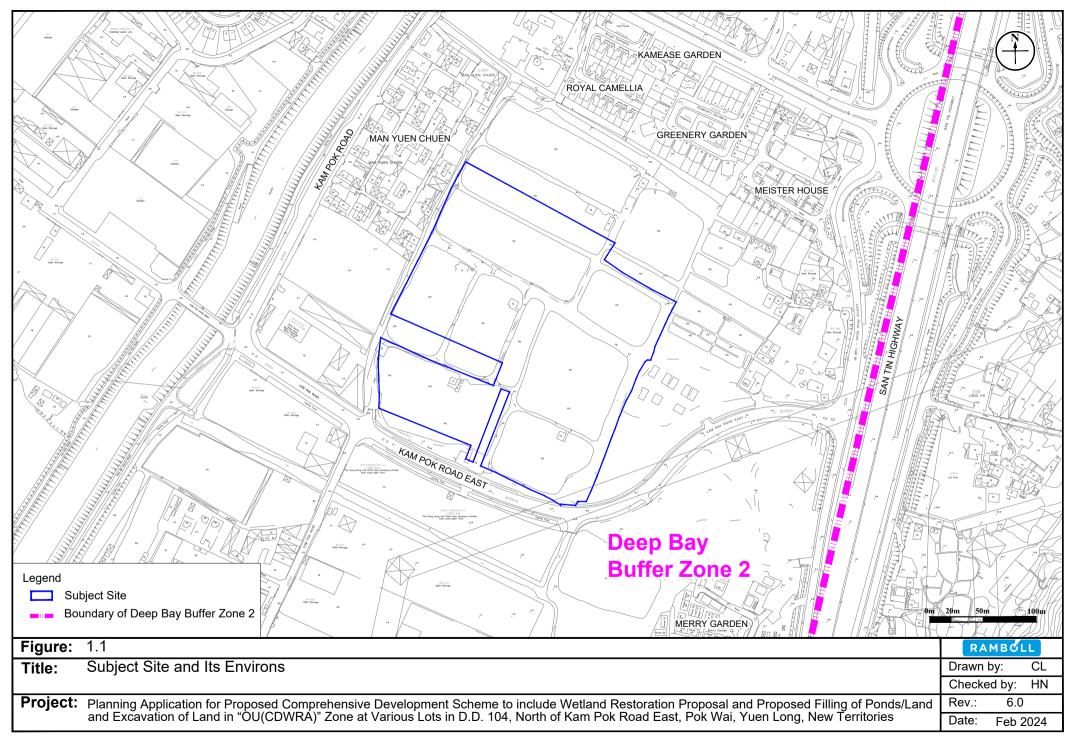
6. OVERALL CONCLUSION

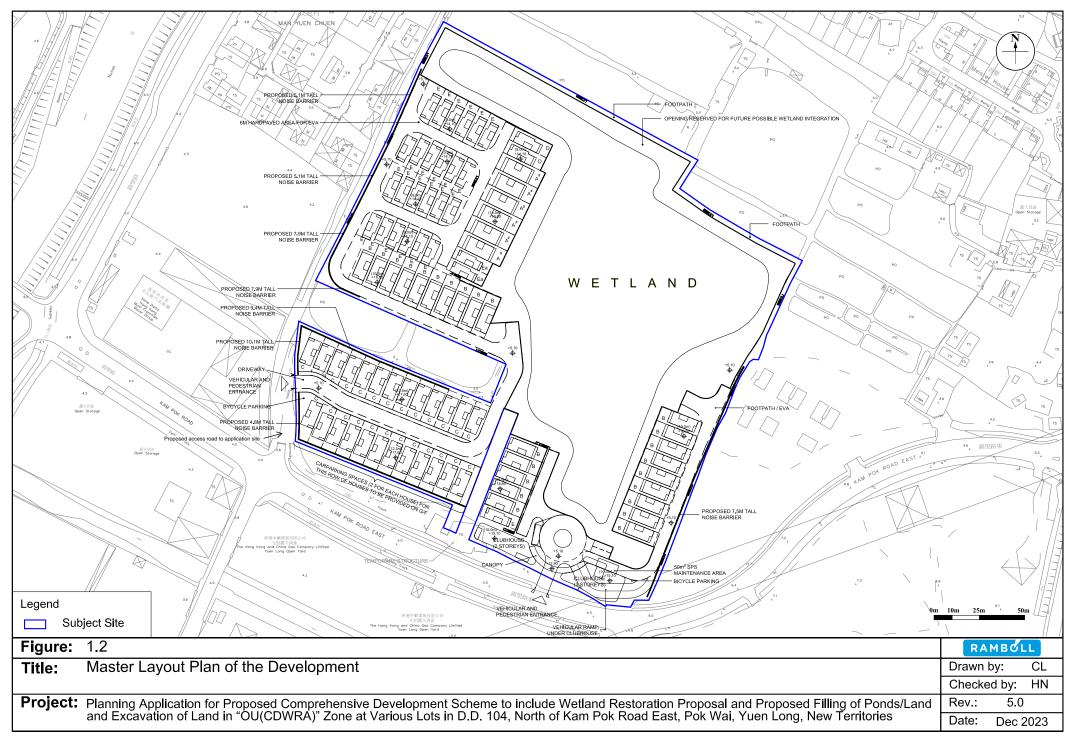
- 6.1.1 The potential air quality, noise and water quality impacts that may arise from the operational phase of the proposed development have been assessed.
- 6.1.2 For air quality impact, construction dust impact, vehicular emission impact, odour impact, and industrial emission impact have been reviewed. With mitigation measures, such as peripheral setback from the site boundary and provision of adequate buffer distances, incorporated into the design of the development, no adverse air quality impact to the proposed development or from the construction of the proposed development is anticipated.
- 6.1.3 For noise impact, road traffic noise and industrial noise impacts have been reviewed. With the adoption of the proposed noise mitigation measures including single aspect design, setback from the site boundary, provision of noise barriers, solid parapet wall, and fixed glazing/ blank façade, etc., the predicted noise levels at the proposed development due to the road traffic and industrial noise can fully comply with the relevant noise criteria, and no unacceptable noise impact is therefore anticipated.
- 6.1.4 For water quality impact, sewerage and drainage impact assessments have been conducted and reported in separate reports. Proper sewerage and drainage systems are proposed in order to ensure no overflow of sewage and stormwater will arise. Any maintenance work for the proposed WRA will be conducted during the dry season to avoid water discharge. BMP will be implemented as well. The filling and reprofiling of the existing abandoned ponds will be conducted in phases to minimize potential water quality impacts. No adverse water quality impact due to the Proposed Development is anticipated.

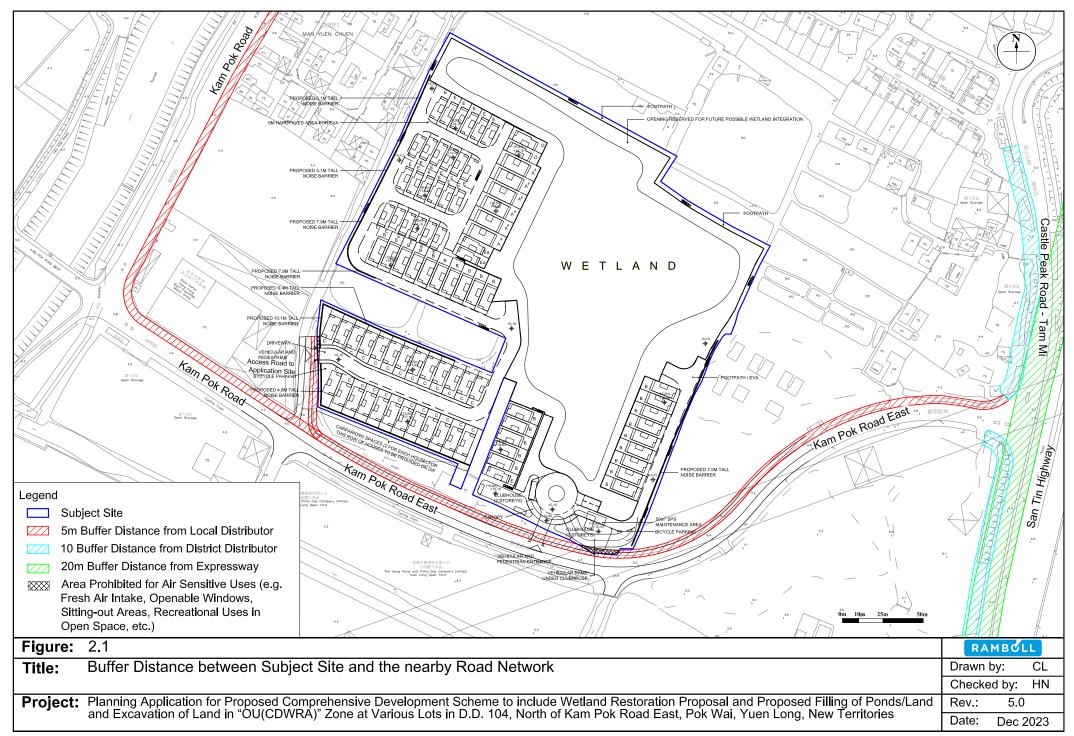


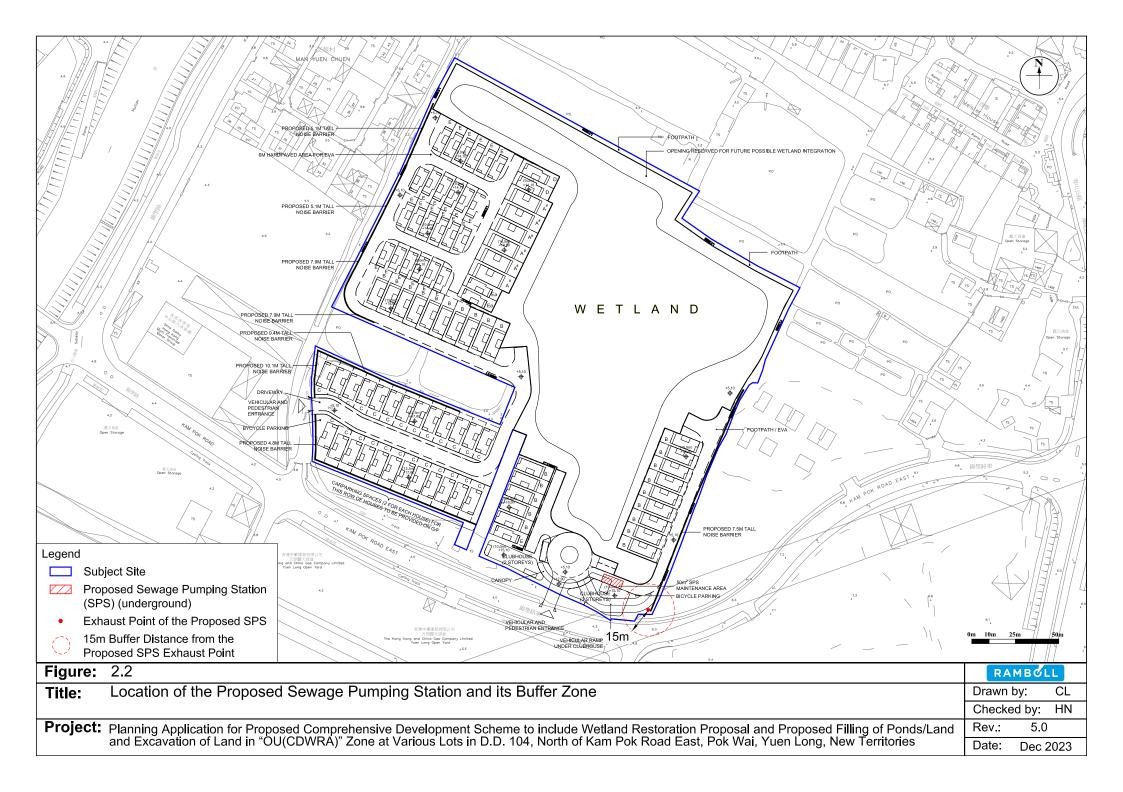
Figures

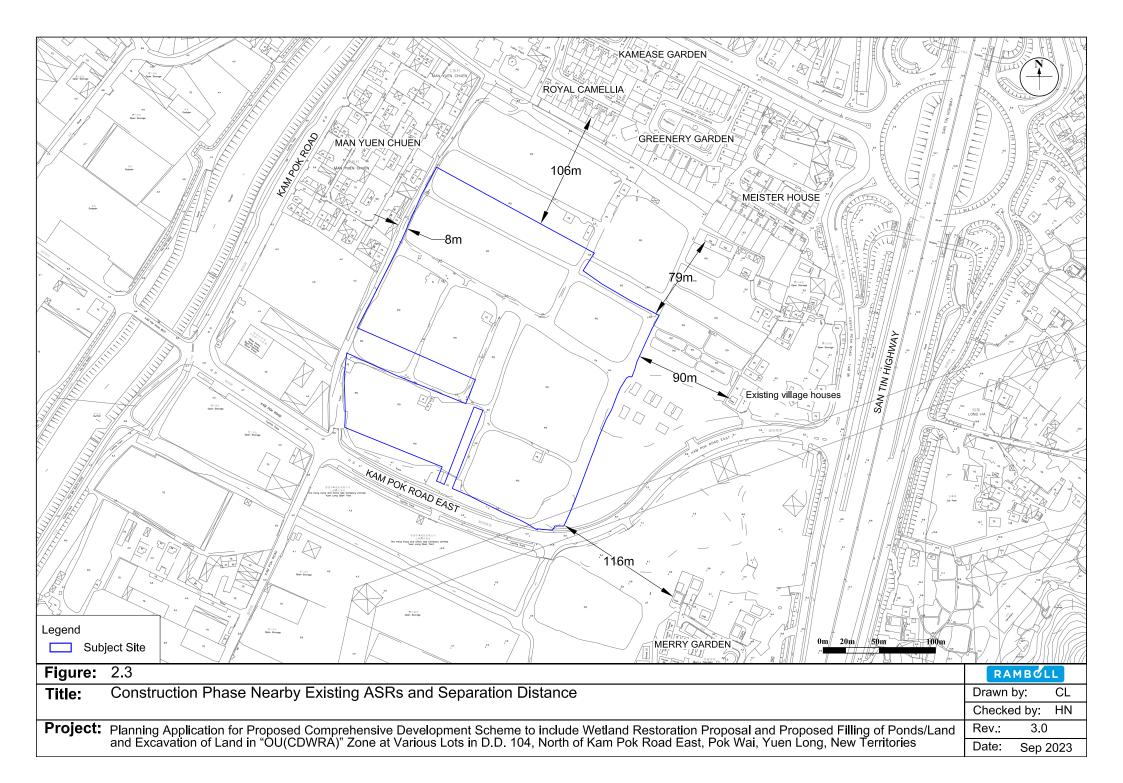


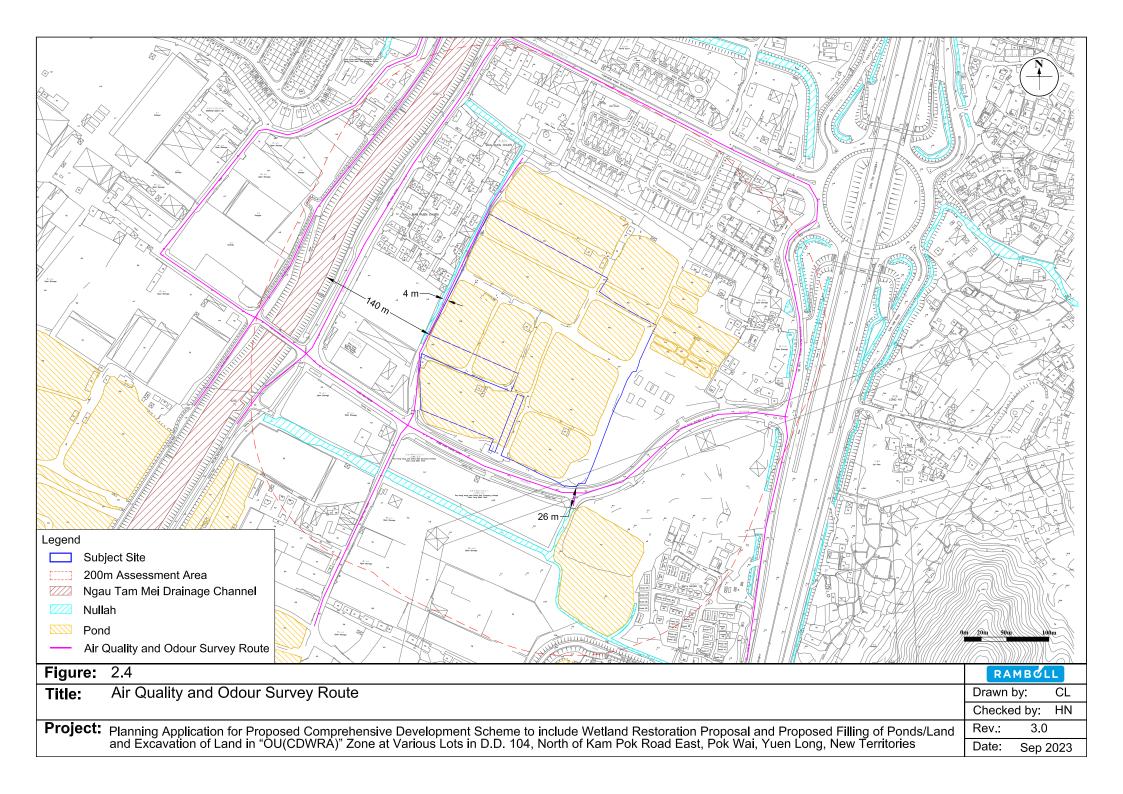


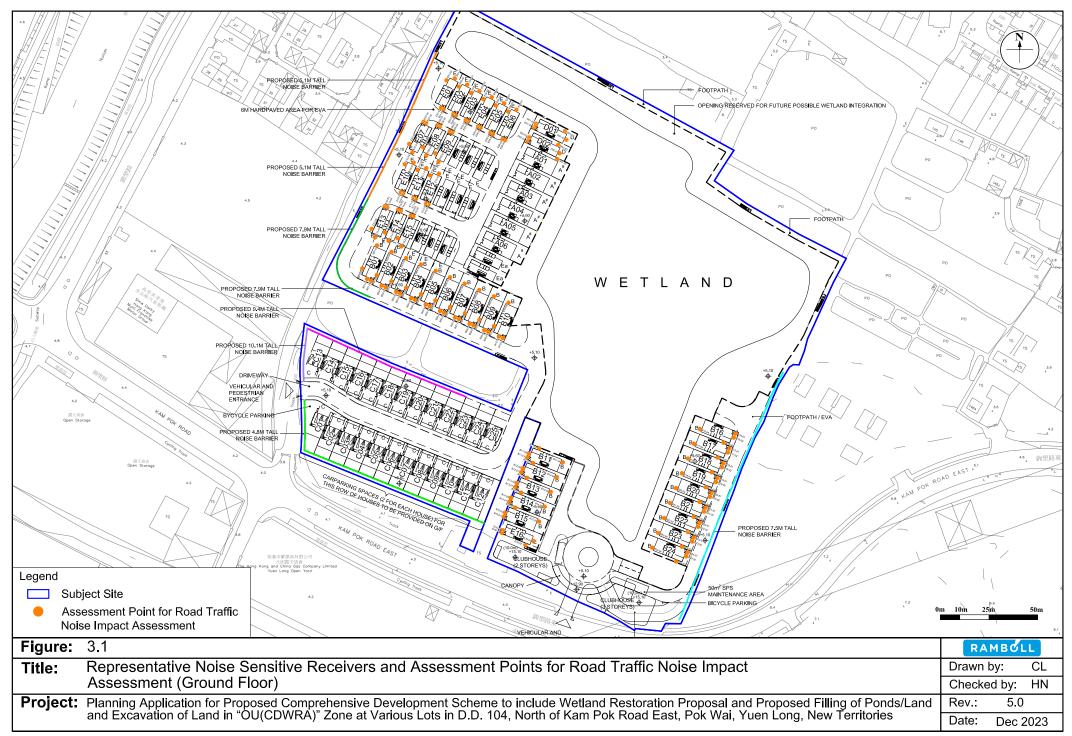


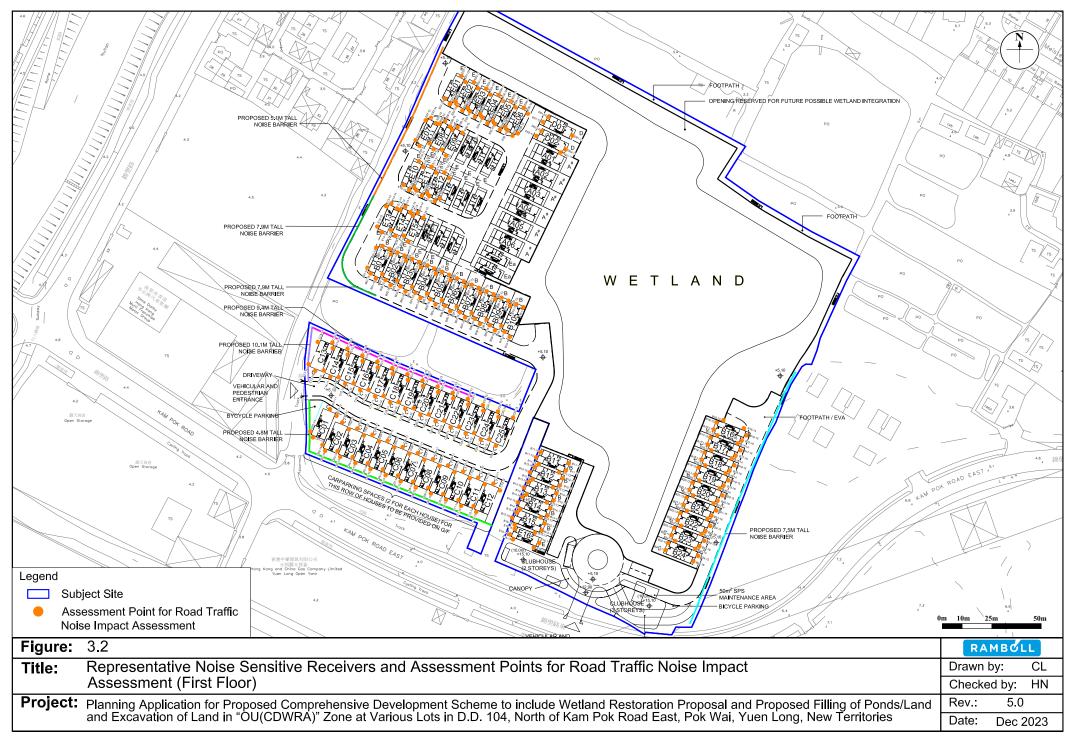


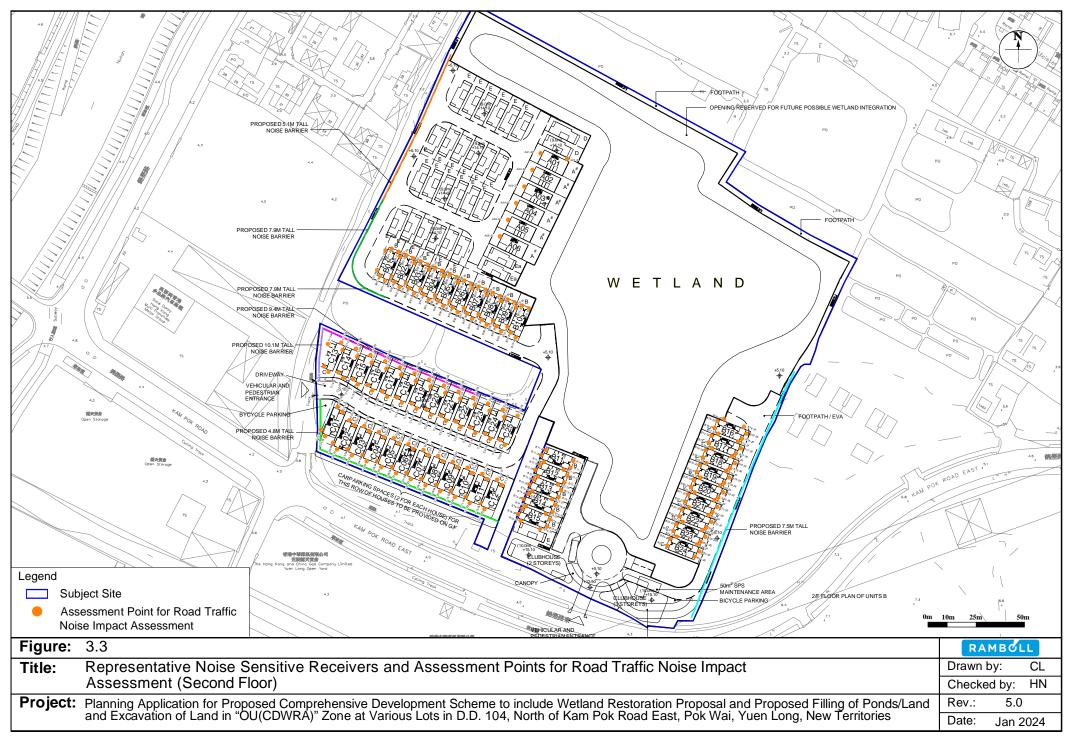


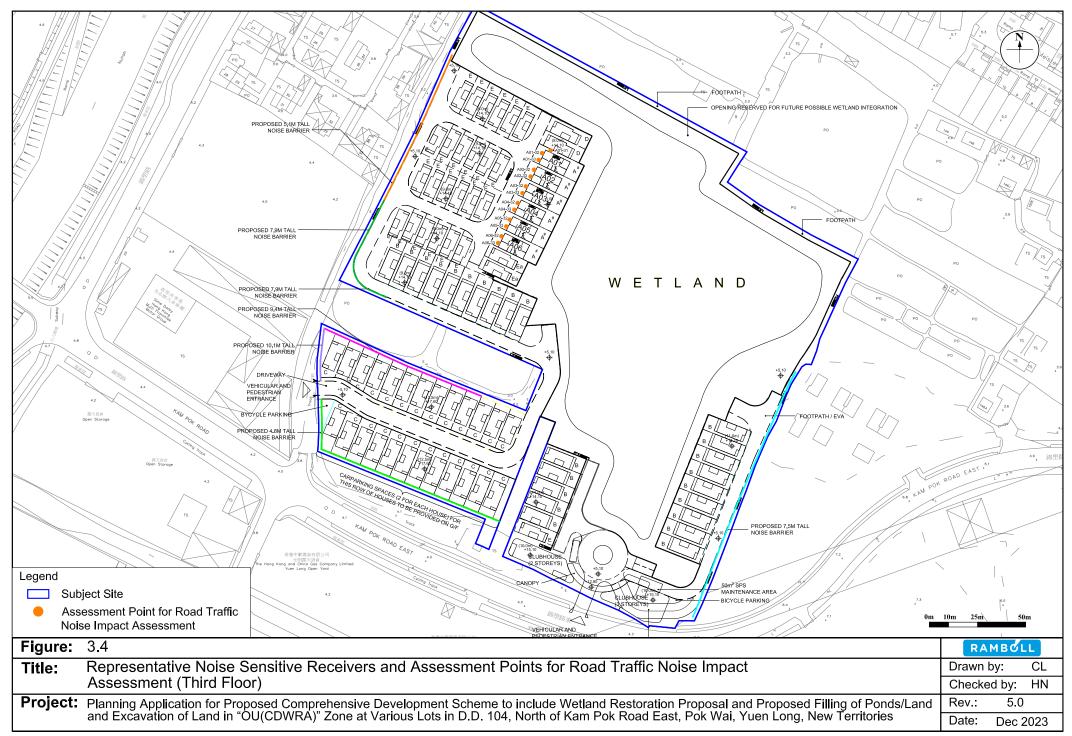


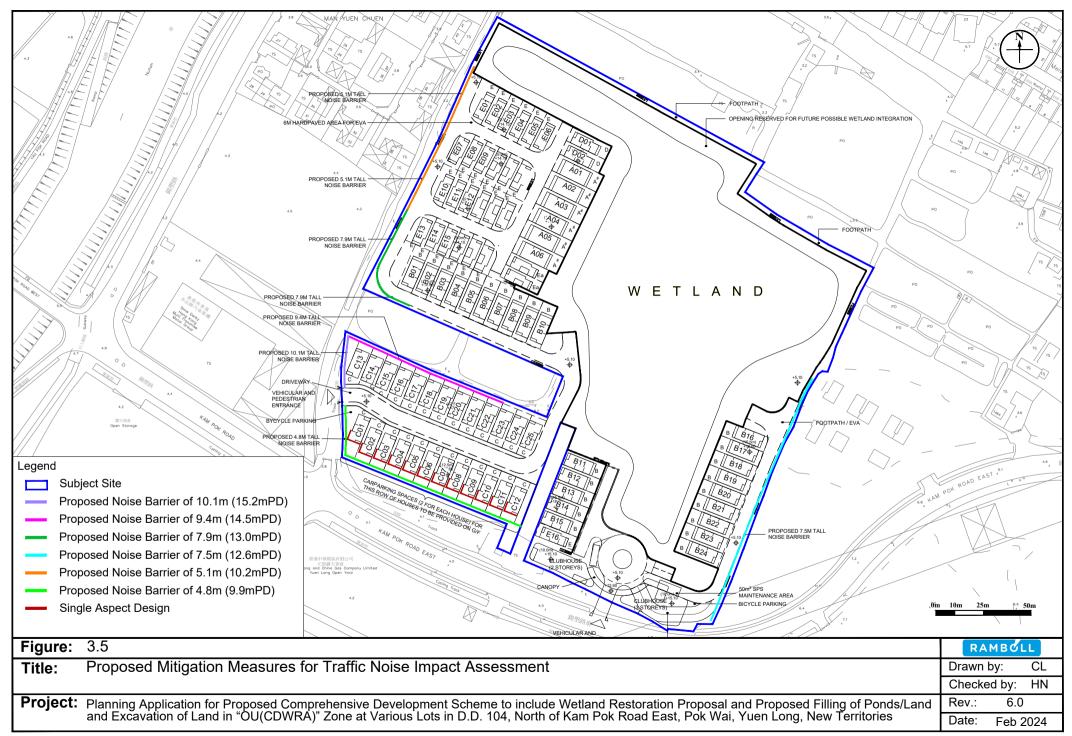


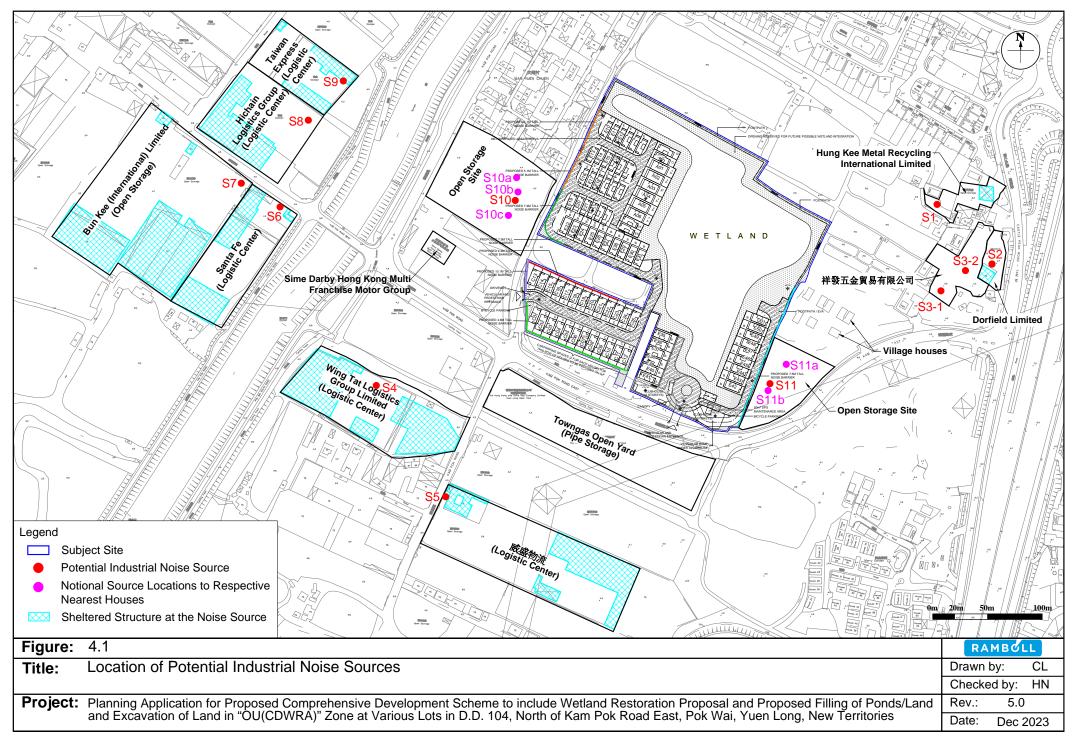


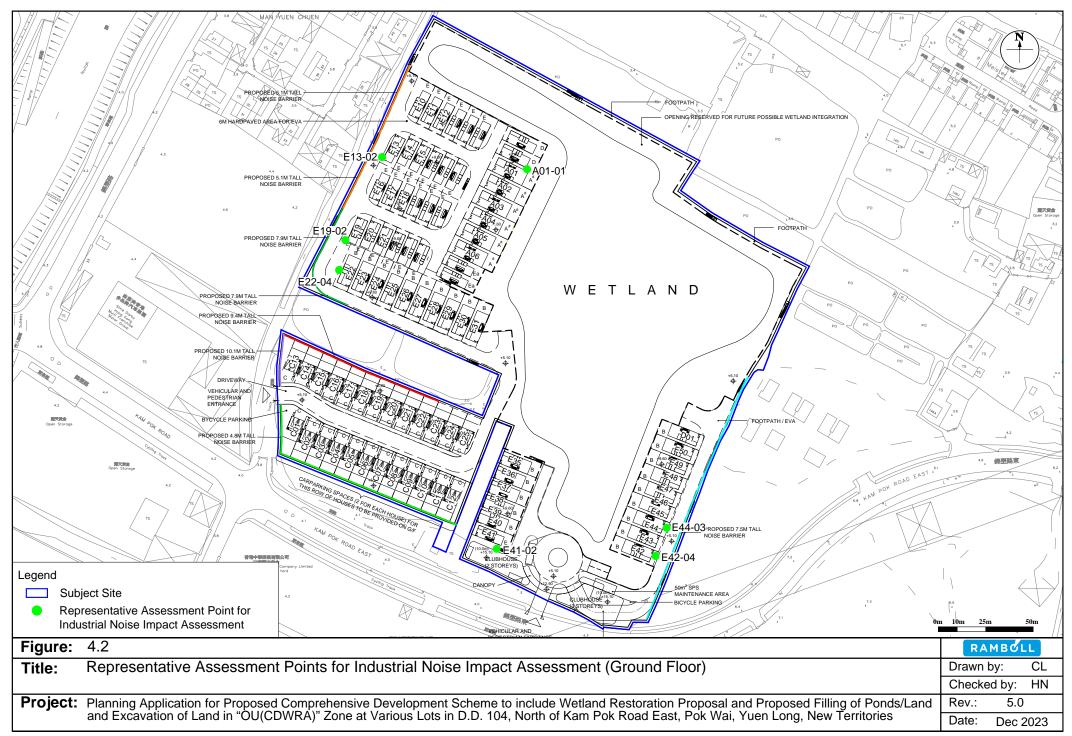


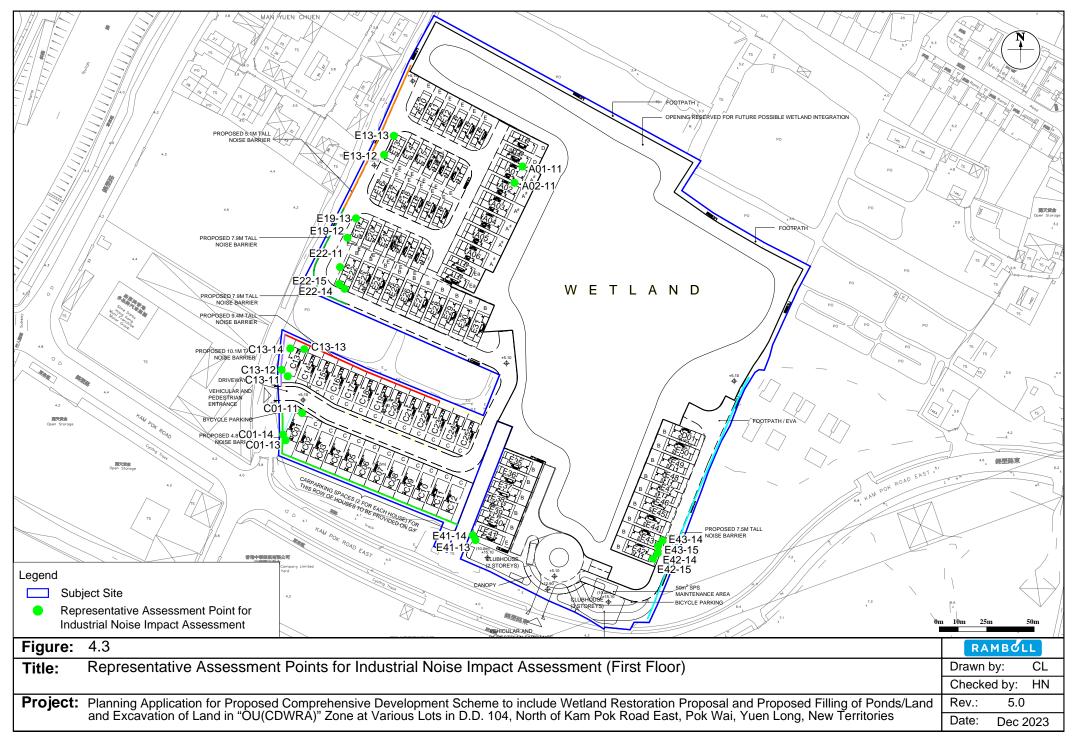


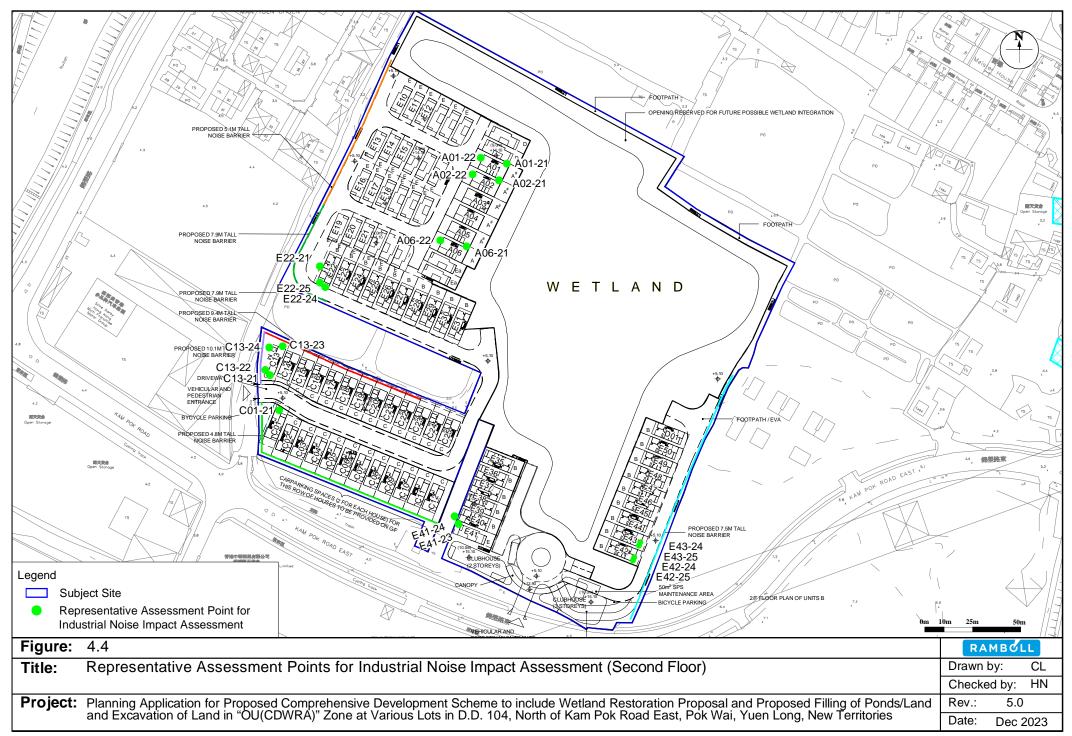


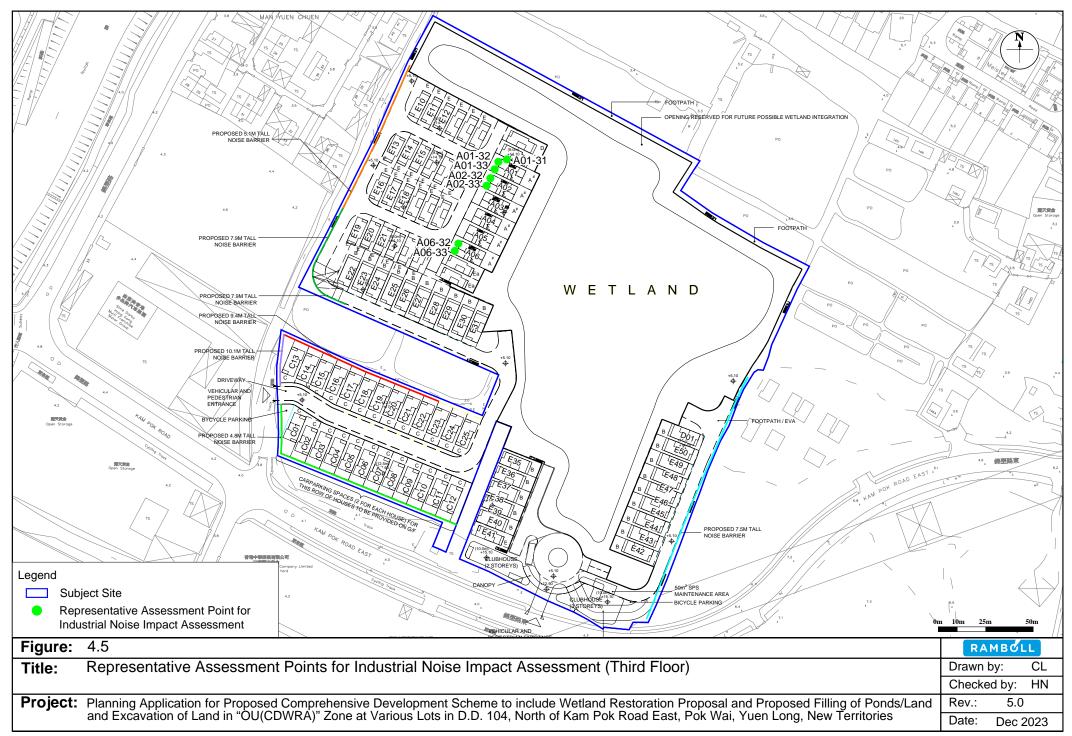


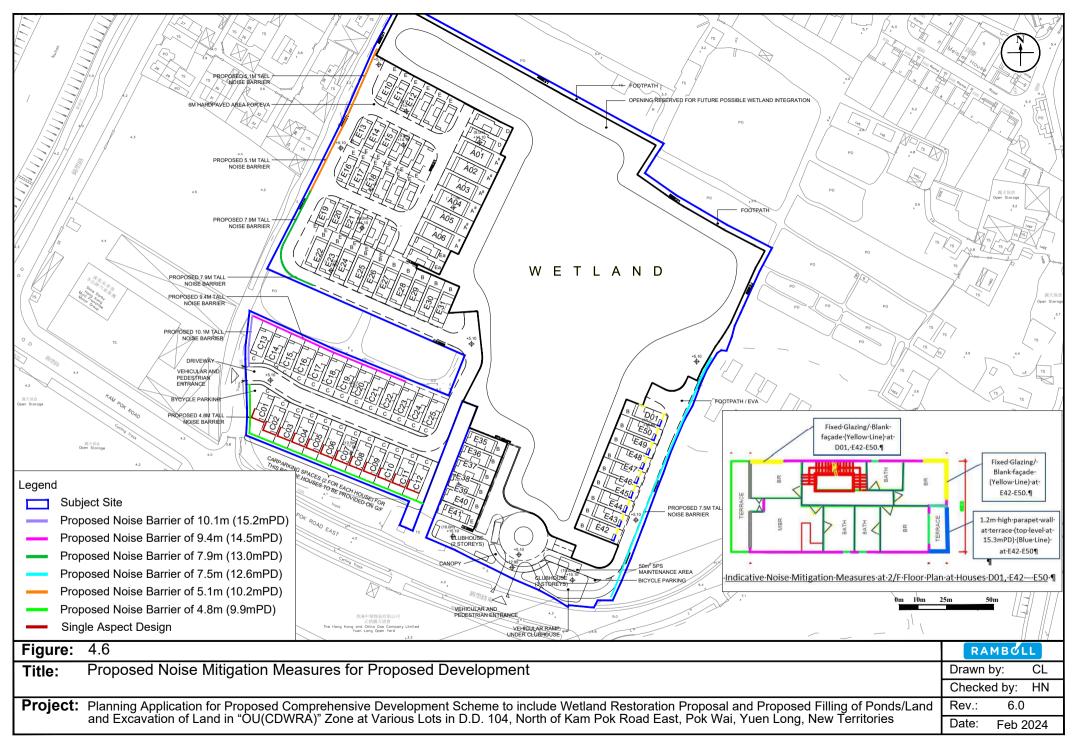


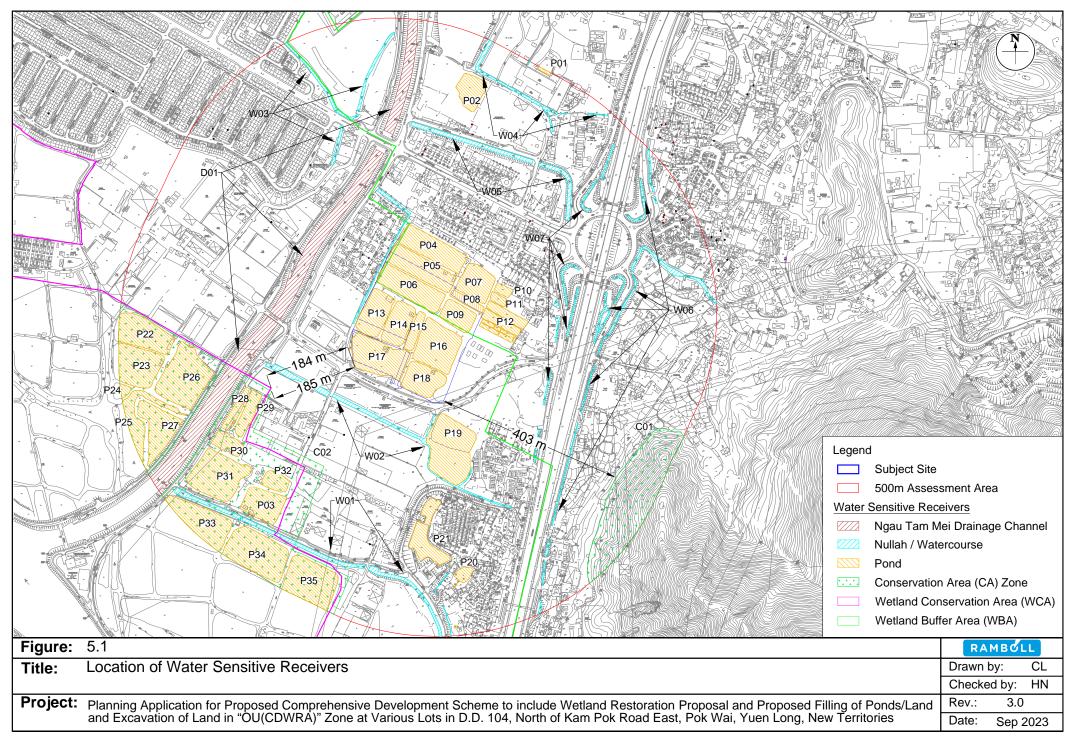


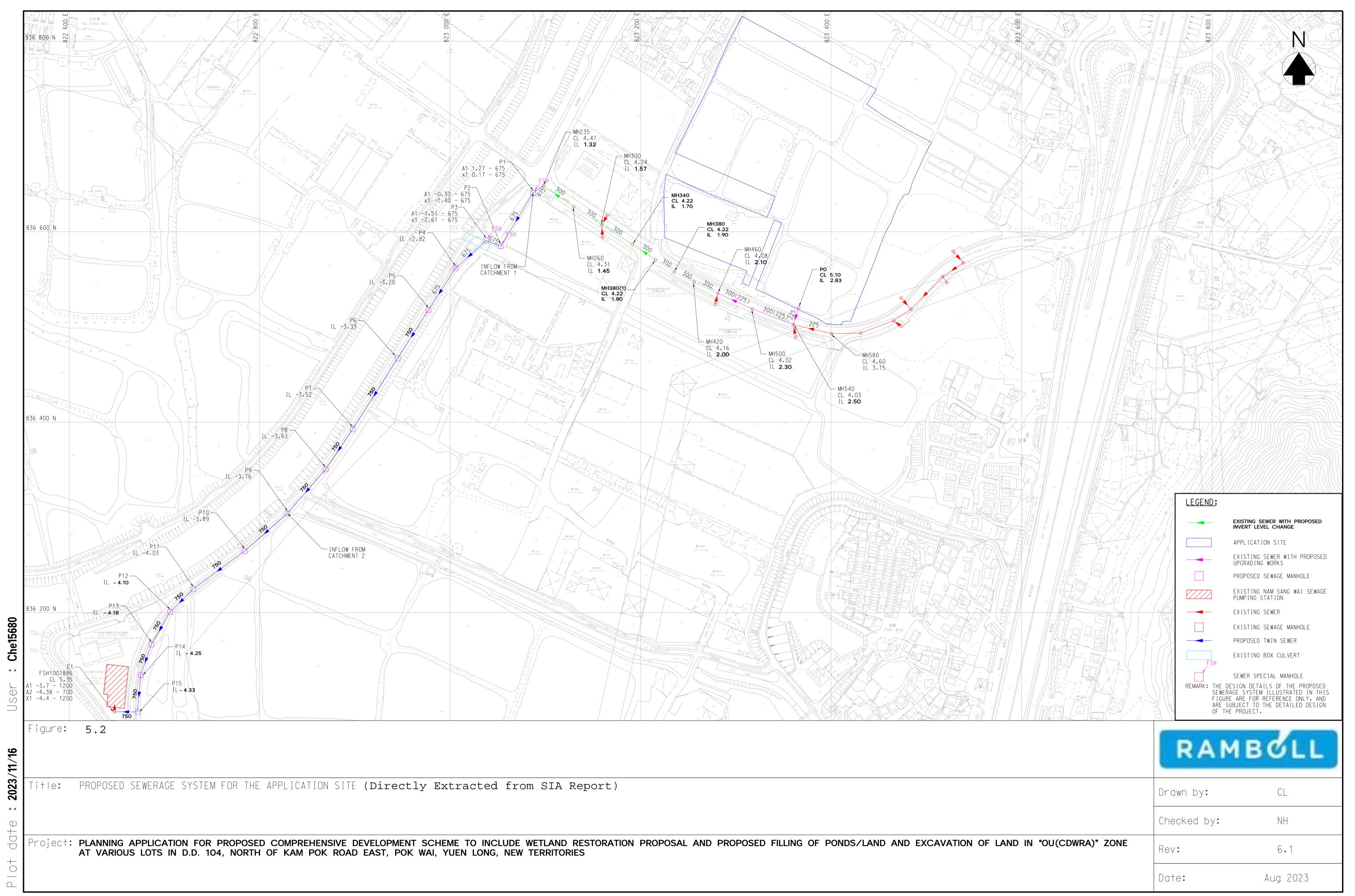


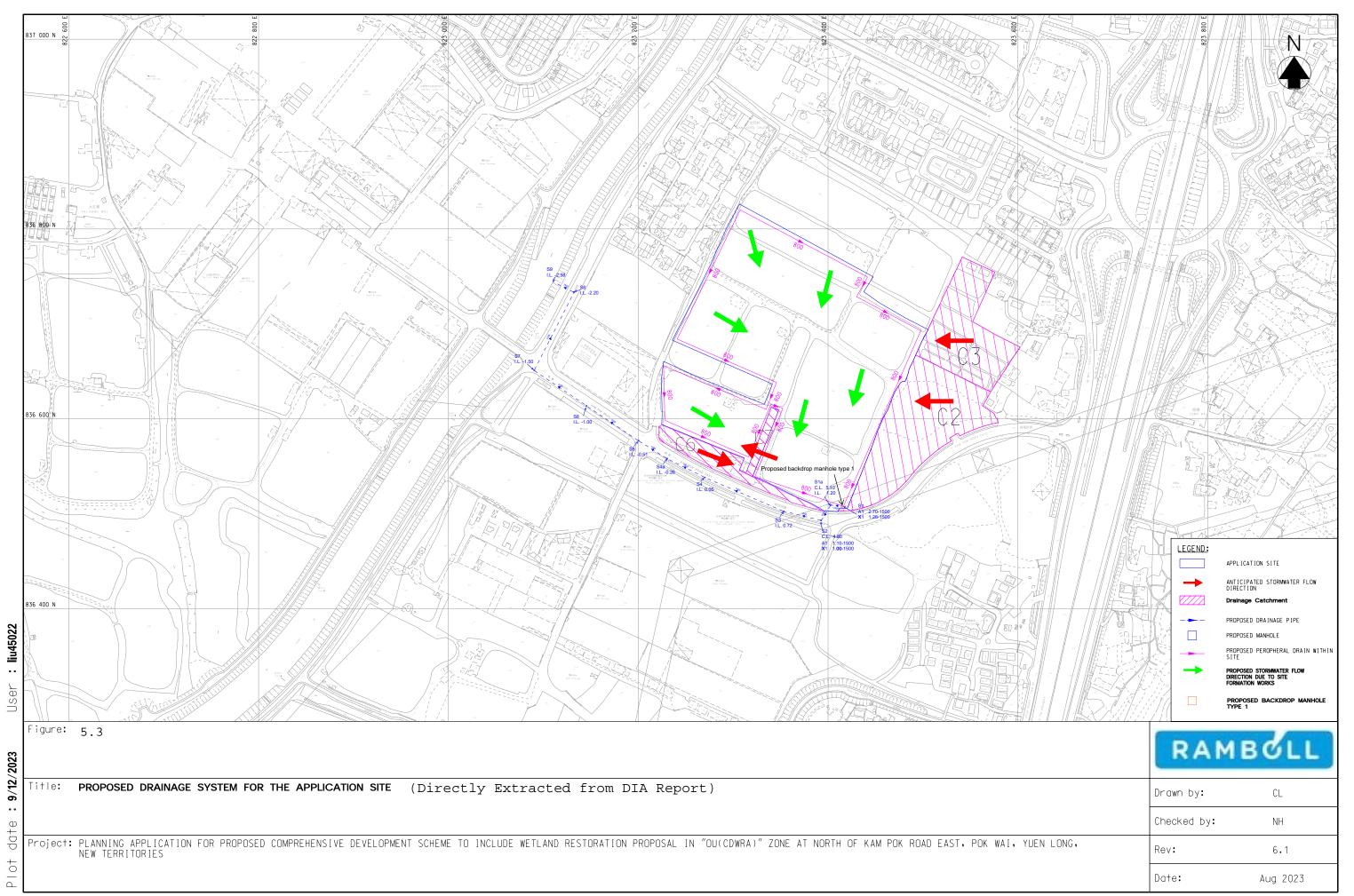












Appendices



Appendix 1.1

Typical Layout of the Residential Houses







Appendix 2.1 Background Air Quality



Proposed Comprehensive Development Scheme to include Wetland Restoration Proposal in "OU(CDWRA)" one at North of Kam Pok Road East, Pok Wai, Yuen Long, New Territories

Statistics of Past Ambient Air Quality (Yuen Long Monitoring Station)

Pollutants	<u></u>		<u> </u>					Con	centration (μg/m³) ⁽¹⁾⁽²⁾	Averaging F	Periods							
Averagin Periods		10 m	in ⁽³⁾⁽⁴⁾		1 Hour Daily 8 Hour moving average			24 Hour			1 Year								
Statistics	AQO	4th	Max	No. of Ex	AQO	19th	Max	No. of Ex	AQO	10th	Max (5)	No. of Ex	AQO	4th	10th / 36th	Max	No. of Ex	AQO	Mean (6)
Sulphur Dioxide, SO ₂			_																
2018	500	52	70	0									50	16		20	0		8
2019		42	53	0										11	1	12	0		5
2020	Not to be	26	27	0									Not to be	10		11	0		5
2021	exceeded	24	26	0		n	.a.			n	.a.		exceeded	14	n.a.	15	0	n.a.	9
2022		21	36	0		"	.a.			"	.a.		more than	7	II.a.	7	0	II.a.	4
5-year average =		33	42	-									3 times per	12		13	-		6
PATH in Year 2025 (28,49)	year	50	54	0									year	12		19	0		3
PATH in Year 2025 (28,50)		52	54	0										13		19	0		3
Respirable Suspended Particulates, RSP														,					
2018													100	-	75	121	4		37
2019														-	83	125	2		37
2020													Not to be	-	77	97	0		30
2021		n.	a.			n	.a.			n	.a.		exceeded	-	73	109	1	50	30
2022													more than	-	56	81	0		25
5-year average =													9 times per year	-	73	107	-		32
PATH in Year 2025 (28,49)													year	-	67	91	0		27
PATH in Year 2025 (28,50)														-	69	96	0		28
Fine Suspended Particulates, FSP														1			_		
2018													50	-	34	80	5		20
2019														-	34	81	5		20
2020													Not to be	-	28	44	0		16
2021		n.	a.			n	.a.			n	.a.		exceeded	-	31	75	3	25	17
2022													more than	-	31	64	5		16
5-year average =													35 times per year	-	32	69	-		18
PATH in Year 2025 (28,49)													per year	-	25	73	10		15
PATH in Year 2025 (28,50)															27	78	10		16
Nitrogen Dioxide, NO ₂																			- 10
2018					200	150	231	3											43
2019						161	193	0											44
2020					Not to be	135	170	0											32
2021		n.	a.		exceeded	148	206	1		n	.a.				n.a.			40	40
2022	1				more than 18 times	122	149	0											37
5-year average =					per year	143	190	-											39
PATH in Year 2025 (28,49)					po. you.	117	178	0											16
PATH in Year 2025 (28,50)						123	184	0											18
Ozone, O ₃									160	160	240	10							42
									100	162	249	10							43
2019 2020									 	200 154	310 234	25 8							53 43
2020									Not to be		286								
2021		n.	a.			n	.a.		exceeded more than	178 194	309	14 22			n.a.			n.a.	49 52
									9 times per	178	278	-	-						
5-year average = PATH in Year 2025 (28,49)									year	216	257	57							48 92
PATH III Teal 2025 (26,49) PATH in Year 2025 (28,50)									'	218	257	60							92
Carbon Monoxide, CO										210	200	00							31
2018							1720	0			1574	0							
2019							2150	0			1903	0							
2020							1530	0			1279	0							
2021							2090	0			1591	0							
2022		n.	a.		30000	n.a.	1700	0	10000	n.a.	1519	0			n.a.			r	ı.a.
5-year average =							1838	-	 		1573	-	1						
PATH in Year 2025 (28,49)							949	0			859	0	1						
PATH in Year 2025 (28,50)							952	0			865	0							
. //////// Total 2020 (20,00)	<u> </u>					<u> </u>	302	Ŭ			300	·							

Summary

Notes:

- (1) Measured at 293 K and 101.325 kPa (one atmosphere)
- (2) Value in red exceeds the AQO
- (3) 10-min average SO2 levels were calculated based on stability classes in the corresponding PATH grid(s)
- (4) " " denotes no data available
- (5) Max. daily 8h moving average for O_3
- (6) Arithmetic mean

P.1 of 1

Appendix 2.2
Confirmation of Road Type by TD



Crystal Lui

From: Chi Sing LAM <chisinglam@td.gov.hk>

Sent: 06 June 2023 16:17

To: LAU Ivan

Cc: cannychan@visionplanning.com.hk; MA Cathy; Henry Ng; 'Katherine Tse';

kimchan@visionplanning.com.hk; Katie Yu; Ming Yip TSE; MOK Moraine; 'Nathan

Chung'; 'Richard Fung'; Wai Shing CHU

Subject: Re: Planning Application A/YL-NSW/314 - Road Category Confirmation

Dear Ivan,

Please find my further clarification on the road category for road section 9A.

Road name	Road type
(9A?) Access Road connecting to the vehicular entry of the Proposed	Not a public road.
Development	No road category.
(2A) (2B) Castle Peak Road – Tam Mei (1)	Primary Distributor (PD)
	Rural Road (RR)
(7B?) Kam Pok Road (1)	Local Distributor (LD)
	Rural Road (RR)
(5A?) Kam Pok Road East (1)	Local Distributor (LD)

Thank you.

Regards, C S LAM E/SD1, TE(NTW) Division Transport Department Tel. 2399 2716

From: Chi Sing LAM/TD/HKSARG
To: LAU Ivan <ilau@systra.com>

Cc: Wai Shing CHU/TD/HKSARG@TD, "cannychan@visionplanning.com.hk" <cannychan@visionplanning.com.hk>, MA Cathy <cma@systra.com>, "hng@ramboll.com" <hng@ramboll.com>, "'Katherine Tse'" <katherinetse@fdbhk.com>, "kimchan@visionplanning.com.hk" <kimchan@visionplanning.com.hk>, "kyu@ramboll.com" <kyu@ramboll.com>, MOK Moraine <mmok@systra.com>, "'Nathan Chung'" <nathanchung@fdbhk.com>, "'Richard Fung'" <richardfung@fdbhk.com>, Ming Yip TSE/TD/HKSARG@TD

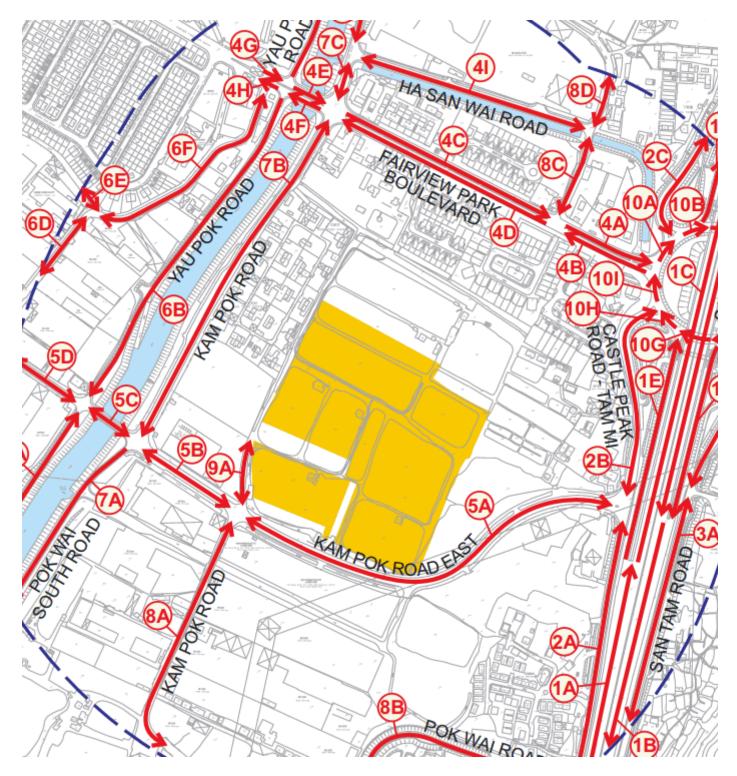
Date: 06-06-23 04:09 PM

Subject: Re: Planning Application A/YL-NSW/314 - Road Category Confirmation

TENTW/ESD1

Dear Mr LAU,

I refer to your preceding email, please find the table below summarizing the road category of the concerned roads:



Please let me know if you need further information.

Thank you.

Regards, C S LAM E/SD1, TE(NTW) Division Transport Department Tel. 2399 2716

From: LAU Ivan <ilau@systra.com>

To: "chisinglam@td.gov.hk" <chisinglam@td.gov.hk>

Cc: "'Nathan Chung'" <nathanchung@fdbhk.com>, "'Richard Fung'" <richardfung@fdbhk.com>, "'Katherine Tse'" <katherinetse@fdbhk.com>, "kimchan@visionplanning.com.hk" <kimchan@visionplanning.com.hk>,

"cannychan@visionplanning.com.hk" <cannychan@visionplanning.com.hk>, "hng@ramboll.com" <hng@ramboll.com>,

"kyu@ramboll.com" <kyu@ramboll.com>, MOK Moraine <mmok@systra.com>, MA Cathy <cma@systra.com>

Date: 22-05-23 04:15 PM

Subject: Planning Application A/YL-NSW/314 - Road Category Confirmation

Dear Mr. Lam,

We, MVA, are commissioned as the traffic consultant for S16 Planning Application for the Proposed Comprehensive Development Scheme to Include Wetland Restoration Proposal in "OU (CDWRA)" Zone at Pok Wai in Yuen Long under Application No. A/YL-NSW/314. Further to the comments received from Environment Protection Department (EPD) on 17 May 2023 regarding the Air Quality Impact Assessment (AQIA) for the aforesaid S16 Planning Application, EPD have the following comments to seek TD's confirmation.

EPD C	Comments
9.	"(a) According to Appendix 3.1 and Figure 2.1, it is noted that an access road (i.e. link ID 9A in NIA) connecting to the proposed development is located to the west of the application site. Please provide the road type (with TD's endorse this access road"
11.	"Appendix 2.2 – It is noted that TD's endorsement on the road type of Castle Peak Road – Tam Mi, Kam Pok Road ar obtained more than a year ago. Please check with TD to confirm if all the road type classification provided in Append

<u>For comment item 9</u>, we would like to seek your advice on the <u>road classification of the access road connecting to the vehicular entry of the proposed development at your earliest convenience. Please find attached file Index Plan.pdf showing the concerned carriageway for your easy reference.</u>

We would like to advise you that the access road connecting to the vehicular entry of the proposed development is considered as a road type of Rural Road (RR) according to below requirement.

According to Chapter 3, Volume 2 of Transport Planning and Design Manual (TPDM) issued by Transport
Department (TD), "Rural Roads - Roads connecting the smaller centres of population or popular recreation
areas with major road networks."

Since the concerned access road will be connecting to the vehicular entry of the proposed development with small centres of population, we would like to advise that the road type of the access road connecting to the vehicular entry of the proposed development is considered as Rural Road (RR) for your comment and confirmation.

<u>For comment item 11</u>, we would like to seek your confirmation that road type classification of Castle Peak Road – Tam Mi, Kam Pok Road and Kam Pok Road East obtained previously are still valid.

Please find the below table showing the summary of the above finding for your easy reference.

Road name	Road type
Access Road connecting to the vehicular entry of the Proposed Development	Rural Road (RR)
Castle Peak Road – Tam Mei ⁽¹⁾	Primary Distributor (PD)
Kam Pok Road (1)	Local Distributor (LD)
Kam Pok Road East ⁽¹⁾	Local Distributor (LD)

Note: (1) Please find attached email from	TD on the road type for	Castle Peak Road,	Kam Pok Road a	ınd
Kam Pok Road East.				

Should you have any enquiries or require further information, please do not hesitate to contact the undersigned or Ms Moraine Mok at 28646303.

Thank you very much for your kind attention.

Best Regards,

Ivan Lau

Principal Traffic Engineer

Tel: +852 2864 6472 (Direct Line) • Gen: +852 2529 7037 • Fax: +852 2527 8490



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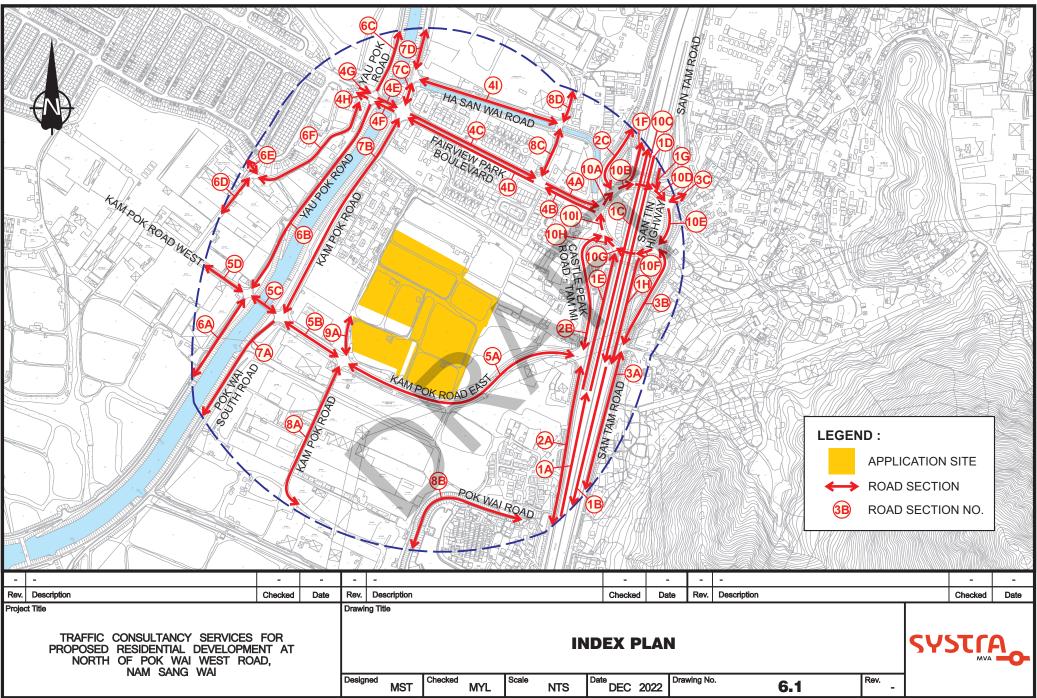
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========= [attachment "Index Plan.pdf" deleted by Chi Sing LAM/TD/HKSARG] [attachment "Email from TD_20211217.pdf" deleted by Chi Sing LAM/TD/HKSARG] [attachment "EPD'comment for Application no. NSW314.pdf" deleted by Chi Sing LAM/TD/HKSARG]

Appendix 3.1

Traffic Forecast for Year 2040 Peak Hour





Year 2040 AM Peak Traffic Forecast

Road Section No. ⁽¹⁾	Poad Namo		2040 Design AM Peak Traffic Flows (veh/hr) (round-up to nearest 10)	HV% ⁽²⁾
1A	San Tin Highway	NB	4230	45%
1B	San Tin Highway	SB	4520	47%
1C	San Tin Highway	NB	3310	48%
1D	San Tin Highway	SB	3440	51%
1E	Slip Road of San Tin Highway	NB	920	35%
1F	Slip Road of San Tin Highway	NB	560	37%
1G	Slip Road of San Tin Highway	SB	700	35%
1H	Slip Road of San Tin Highway	SB	1090	33%
2A	Castle Peak Road - Tam Mi	2-way	520	37%
2B - NB	Castle Peak Road - Tam Mi	NB	430	49%
2B - SB	Castle Peak Road - Tam Mi	SB	300	50%
2C	Castle Peak Road - Tam Mi	2-way	1000	33%
3A	San Tam Road	2-way	960	42%
3B	San Tam Road	2-way	1000	41%
3C	San Tam Road	2-way	920	35%
4A	Fairview Park Boulevard	EB	850	24%
4B	Fairview Park Boulevard	WB	570	31%
4C	Fairview Park Boulevard	EB	810	22%
4D	Fairview Park Boulevard	WB	520	31%
4E	Fairview Park Boulevard	EB	700	14%
4F	Fairview Park Boulevard	WB	530	22%
4G	Fairview Park Boulevard	EB	700	15%
4H	Fairview Park Boulevard	WB	510	22%
41	Ha San Wai Road		50	37%
5A - EB	Kam Pok Road East	2-way EB	170	67%
5A - WB	Kam Pok Road East	WB	170	69%
5B - EB	Kam Pok Road East	EB	120	71%
5B - WB	Kam Pok Road East	WB	120	76%
	Kam Pok Road West			
5C 5D	Kam Pok Road West Kam Pok Road West	2-way	330 320	61% 59%
		2-way		
6A	Yau Pok Road	2-way	30	50%
6B	Yau Pok Road	SB	20 0 ⁽³⁾	25%
6C	Yau Pok Road	NB	<u> </u>	N/A
6D	Unnamed Road	2-way	120	61%
6E	Unnamed Road	2-way	60	56%
6F	Unnamed Road	2-way	170	64%
7A	Pok Wai South Road	SB	60	19%
7B - NB	Kam Pok Road	NB	110	50%
7B - SB	Kam Pok Road	SB	100	37%
7C	Kam Pok Road	2-way	200	24%
7D	Kam Pok Road	2-way	210	20%
8A	Kam Pok Road	2-way	170	70%
8B	Pok Wai Road	2-way	20	22%
8C	Unnamed Road	2-way	100	43%
8D	Unnamed Road	2-way	30	37%
9A	Access Road to Application Site	2-way	20	13%
10A	Fairview Park Boulevard Roundabout	1-way	2220	34%
10B	Fairview Park Boulevard Roundabout	1-way	2260	33%
10C	Fairview Park Boulevard Roundabout	1-way	1700	32%
10D	Fairview Park Boulevard Roundabout	1-way	2400	33%
10E	Fairview Park Boulevard Roundabout	1-way	2480	33%
10F	Fairview Park Boulevard Roundabout	1-way	1980	35%
10G	Fairview Park Boulevard Roundabout	1-way	890	39%
10H	Fairview Park Boulevard Roundabout	1-way	1810	37%
10I	Fairview Park Boulevard Roundabout	1-way	1940	38%

Note:

(1) Refer to Drawing No. 6.1

⁽²⁾ Heavy vehicle (HV) percentage including the category of goods vehicles (GV) (comprise with vans, light goods vehicles (LGV), medium / heavy goods vehicles (MGV/HGV) and container trucks) and the category of public transport (PT) (comprise with public light buses (PLB), non-franchised buses (SPB) (including all small coaches and large coaches) and franchised buses (FB))

⁽³⁾ The road section is emergency vehicle access road with emergency crash gate, thus no general traffic is forecasted



Our Ref: CHK50709210/MYL/L2300926/sys

Ramboll Hong Kong Limited 21/F, BEA Harbour View Centre, 56 Gloucester Road, Wan Chai, Hong Kong

BY EMAIL

hng@ramboll.com

Attn: Mr. Henry Ng

Proposed Residential Development at Various Lots in D.D. 104, Pok Wai, Yuen Long Long Term Traffic Forecast for Noise Impact Assessment 9th June 2023

Dear Sir,

We refer to our submission of traffic forecast dated 22nd May 2023 via email to Transport Department and the endorsement from Transport Department dated 6th June 2023 regarding the captioned project.

We write to confirm that Transport Department's endorsed methodology prepared by us has been strictly adopted in preparing the traffic forecast for the Noise Impact Assessment Report prepared by Ramboll Hong Kong Ltd.

Should you have any queries, please feel free to contact the undersigned at 2864 6303.

Thank you for your kind attention.

Yours faithfully,

Moraine Mok Associate Director

encl.

MA Cathy

From: Chi Sing LAM <chisinglam@td.gov.hk>

Sent: Tuesday, June 6, 2023 4:08 PM

To: LAU Ivan

Cc: cannychan@visionplanning.com.hk; MA Cathy; hng@ramboll.com; 'Katherine Tse';

kimchan@visionplanning.com.hk; kyu@ramboll.com; MOK Moraine; 'Nathan Chung';

'Richard Fung'; Ming Yip TSE

Subject: Re: Planning Application A/YL-NSW/314 - Long term traffic forecast

Dear Mr LAU,

Please note that Noise Impact Assessment is not under our purview. We are not in a position to provide comments on the traffic figures tailor-made for the environmental assessment study.

Notwithstanding the above, we have no objection in principle to the methodology of the traffic forecast.

Thank you.

Regards, C S LAM E/SD1, TE(NTW) Division Transport Department Tel. 2399 2716

From: LAU Ivan <ilau@systra.com>

To: "chisinglam@td.gov.hk" <chisinglam@td.gov.hk>

Cc: "'Nathan Chung'" <nathanchung@fdbhk.com>, "'Richard Fung'" <richardfung@fdbhk.com>, "'Katherine Tse'"

<katherinetse@fdbhk.com>, "kimchan@visionplanning.com.hk" <kimchan@visionplanning.com.hk>,

"cannychan@visionplanning.com.hk" <cannychan@visionplanning.com.hk>, "hng@ramboll.com" <hng@ramboll.com>, "kyu@ramboll.com" <kyu@ramboll.com>, MOK Moraine <mmok@systra.com>, MA Cathy <cma@systra.com>

Date: 22-05-23 04:15 PM

Subject: Planning Application A/YL-NSW/314 - Long term traffic forecast

Dear Mr. Lam,

Further to the Noise Impact Assessment (NIA) and the Traffic Impact Assessment (TIA) report submission attached in S16 Planning Application of TPB Ref. A/YL-NSW/314 on 24 March 2023 (Vision Planning Consultants Limited's Ref: YL-NSW/PA/FDB/22-02), and the comments received from Environment Protection Department (EPD) regarding the NIA for the aforesaid S16 Planning Application, EPD commented that "S.3.4.2 – Please document TD's agreement on the traffic forecast data in the report once available". Please refer to attached file, "EPD's comment for Application no. NSW314.pdf", for the Planning Department's email dated 17 May 2023 regarding the EPD's comment on the aforesaid S16 planning application.

Grateful if you could agree with the methodology of long term traffic forecast and traffic flow as described in Chapter 6 of the latest submission of TIA report, submitted to PlanD on 24 March 2023 (Vision Planning consultants Limited's Ref: YL-NSW/PA/FDB/22-02), for the traffic flow data prediction under the aforesaid S16 planning application. The aforesaid Chapter 6 is also attached, "Chapter 6 of NSW TIA Report.pdf", and please find below download link for the full report of the TIA report under the S16 planning application for your easy reference. download link:

 $\underline{https://sendto.systra.com/pickup?claimID=NHi6TGQiWP4xTits\&claimPasscode=re5AbTeXMR5tfGmS}$

(Please note that the above download link will expire in 7 days)

As illustrated in Chapter 6, please be advised that the anticipated completed year of the Proposed Development is 2025, and therefore design year for 2040 traffic forecasts (15 years after the completion of the Development) have been adopted for NIA.

To derive the long term traffic forecast data for the design year 2040, reference was made to the following information:

- 2019-Based Territorial Population and Employment Data Matrices (TPEDM) planning data published by the Planning Department; and
- Hong Kong Population Projections 2020-2069 published by Census and Statistics Department.

Comparisons are made among the growth rates based on the above reference, we have adopted the growth rate of traffic flows to predict the traffic flow from 2019 to 2040 under conservative approach. Furthermore, the estimated trips generation of the Proposed Development and the planned/committed developments in the nearby area and under the Permitted Development under OZP in the vicinity are also assigned to the existing road network and the forecasted 2040 traffic flows are rounding up to the nearest 10 to allow any unexpected circumstance. Therefore, we would like to advise that the adopted growth rates for 2040 traffic flow data prediction is considered sufficient for NIA.

Grateful if you could agree with the methodology of long term traffic forecast and traffic flow as described in Chapter 6 of the aforesaid TIA report for the traffic flow data prediction under aforesaid S16 planning application.

Should you have any enquiries or require further information, please do not hesitate to contact the undersigned or Ms. Moraine Mok at 28646303.

Best Regards,



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Appendix 3.2

Road Traffic Noise Impact Assessment Results – Unmitigated Scenario



Predicted Results of Road Traffic Noise Impact Assessment for Year 2040 - Unmitigated Scenario (Peak Hour during Morning)

NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Level, L10(1-hour), dB(A)
A01	A01-01	G/F	6.3	66
	A01-11	1/F	9.8	65
	A01-21	2/F	13.3	67
	A01-22	2/F	13.3	55
	A01-31	3/F	16.8	66
	A01-32	3/F	16.8	58
	A01-33	3/F	16.8	58
A02	A02-22	2/F	13.3	54
	A02-32	3/F	16.8	57
	A02-33	3/F	16.8	57

NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Level, L10(1-hour), dB(A)
A03	A03-22	2/F	13.3	54
	A03-32	3/F	16.8	57
	A03-33	3/F	16.8	57
A04	A04-22	2/F	13.3	54
	A04-32	3/F	16.8	57
	A04-33	3/F	16.8	57

NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Level, L10(1-hour), dB(A)
A05	A05-22	2/F	13.3	54
	A05-32	3/F	16.8	57
	A05-33	3/F	16.8	57
A06	A06-22	2/F	13.3	55
	A06-32	3/F	16.8	58
1	A06-33	3/F	16.8	57

NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Level, L10(1-hour), dB(A)
B01	B01-01	G/F	6.3	57
	B01-02	G/F	6.3	58
	B01-03	G/F	6.3	59
	B01-04	G/F	6.3	60
	B01-11	1/F	10.8	59
	B01-12	1/F	10.8	61
	B01-13	1/F	10.8	59
	B01-14	1/F	10.8	59
	B01-15	1/F	10.8	59
	B01-16	1/F	10.8	59
	B01-21	2/F	13.3	62
	B01-22	2/F	13.3	62
	B01-23	2/F	13.3	60
	B01-24	2/F	13.3	60
	B01-25	2/F	13.3	60
	B01-26	2/F	13.3	60
B02	B02-01	G/F	6.3	56
	B02-02	G/F	6.3	56
	B02-03	G/F	6.3	44
	B02-04	G/F	6.3	58
	B02-11	1/F	10.8	59
	B02-12	1/F	10.8	59
	B02-13	1/F	10.8	49
	B02-14	1/F	10.8	47
	B02-15	1/F	10.8	56
	B02-16	1/F	10.8	58
	B02-21	2/F	13.3	62
	B02-22	2/F	13.3	62
	B02-23	2/F	13.3	53
	B02-24	2/F	13.3	52
	B02-25	2/F	13.3	58
	B02-26	2/F	13.3	59
B03	B03-01	G/F	6.3	56
	B03-02	G/F	6.3	56
	B03-03	G/F	6.3	44
	B03-04	G/F	6.3	58
	B03-11	1/F	10.8	59
	B03-12	1/F	10.8	59
	B03-13	1/F	10.8	49
	B03-14	1/F	10.8	47
	B03-15	1/F	10.8	56
	B03-16	1/F	10.8	57
	B03-21	2/F	13.3	62
	B03-22	2/F	13.3	62
	B03-23	2/F	13.3	53
	B03-24	2/F	13.3	52
	B03-25	2/F	13.3	58
	B03-26	2/F	13.3	59

				I B Pate III IN
NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Level, L10(1-hour), dB(A)
B04	B04-01	G/F	6.3	55
	B04-02	G/F	6.3	55
	B04-03	G/F	6.3	45
	B04-04	G/F	6.3	58
	B04-11	1/F	10.8	59
	B04-12	1/F	10.8	59
	B04-13	1/F	10.8	49
	B04-14	1/F	10.8	48
	B04-15	1/F	10.8	55
	B04-16	1/F	10.8	57
	B04-21	2/F	13.3	63
	B04-22	2/F	13.3	62
	B04-23	2/F	13.3	54
	B04-24	2/F	13.3	52
	B04-25	2/F	13.3	57
	B04-26	2/F	13.3	59
B05	B05-01	G/F	6.3	55
	B05-02	G/F	6.3	55
	B05-03	G/F	6.3	45
	B05-04	G/F	6.3	58
	B05-11	1/F	10.8	61
	B05-12	1/F	10.8	60
	B05-13	1/F	10.8	49
	B05-14	1/F	10.8	48
	B05-15	1/F	10.8	55
	B05-16	1/F	10.8	57
	B05-21	2/F	13.3	64
	B05-22	2/F	13.3	63
	B05-23	2/F	13.3	53
	B05-24	2/F	13.3	52
	B05-25	2/F	13.3	57
	B05-26	2/F	13.3	59
B06	B06-01	G/F	6.3	55
200	B06-02	G/F	6.3	55
	B06-03	G/F	6.3	47
	B06-04	G/F	6.3	60
	B06-11	1/F	10.8	63
	B06-12	1/F	10.8	62
	B06-13	1/F	10.8	50
	B06-14	1/F	10.8	49
	B06-15	1/F	10.8	55
	B06-16	1/F	10.8	56
	B06-21	2/F	13.3	65
	B06-22	2/F	13.3	65
	B06-23	2/F	13.3	53
	B06-24	2/F	13.3	53
	B06-25	2/F	13.3	57
	B06-26	2/F	13.3	58
	D00-20	4/ F	13.3] 30

NSR	AP ID	Floor	Level,	Predicted Unmitigated Noise
NON	AFID	1 1001	mPD	Level, L10(1-hour), dB(A)
B07	B07-01	G/F	6.3	55
	B07-02	G/F	6.3	55
	B07-03	G/F	6.3	48
	B07-04	G/F	6.3	63
	B07-11	1/F	10.8	65
	B07-12	1/F	10.8	64
	B07-13	1/F	10.8	51
	B07-14	1/F	10.8	50
	B07-15	1/F	10.8	55
	B07-16	1/F	10.8	56
	B07-21	2/F	13.3	66
	B07-22	2/F	13.3	65
	B07-23	2/F	13.3	56
	B07-24	2/F	13.3	53
	B07-25	2/F	13.3	57
	B07-26	2/F	13.3	58
B08	B08-01	G/F	6.3	55
	B08-02	G/F	6.3	55
	B08-03	G/F	6.3	45
	B08-04	G/F	6.3	65
	B08-11	1/F	10.8	65
	B08-12	1/F	10.8	65
	B08-13	1/F	10.8	55
	B08-14	1/F	10.8	48
	B08-15	1/F	10.8	55
	B08-16	1/F	10.8	57
	B08-21	2/F	13.3	66
	B08-22	2/F	13.3	66
	B08-23	2/F	13.3	57
	B08-24	2/F	13.3	52
	B08-25	2/F 2/F	13.3	57
		2/F 2/F		59
DOO	B08-26		13.3	56
B09	B09-01 B09-02	G/F	6.3	56
		G/F	6.3	
	B09-03	G/F	6.3	45
	B09-04	G/F	6.3	65
	B09-11	1/F	10.8	65
	B09-12	1/F	10.8	65
	B09-13	1/F	10.8	54
	B09-14	1/F	10.8	48
	B09-15	1/F	10.8	54
	B09-16	1/F	10.8	57
	B09-21	2/F	13.3	66
	B09-22	2/F	13.3	66
	B09-23	2/F	13.3	56
	B09-24	2/F	13.3	53
	B09-25	2/F	13.3	57
	B09-26	2/F	13.3	59

NSR	AP ID	Floor	Level,	Predicted Unmitigated Noise
		FIOOI	mPD	Level, L10(1-hour), dB(A)
B10	B10-01	G/F	6.3	65
	B10-02	G/F	6.3	59
	B10-03	G/F	6.3	45
	B10-04	G/F	6.3	65
	B10-11	1/F	10.8	66
	B10-12	1/F	10.8	65
	B10-13	1/F	10.8	55
	B10-14	1/F	10.8	48
	B10-15	1/F	10.8	54
	B10-16	1/F	10.8	64
	B10-21	2/F	13.3	66
	B10-22	2/F	13.3	66
	B10-23	2/F	13.3	57
	B10-24	2/F	13.3	53
	B10-25	2/F	13.3	57
	B10-26	2/F	13.3	64
B11	B11-01	G/F	6.3	51
	B11-02	G/F	6.3	51
	B11-03	G/F	6.3	63
	B11-04	G/F	6.3	62
	B11-11	1/F	10.8	63
	B11-12	1/F	10.8	62
	B11-13	1/F	10.8	55
	B11-14	1/F	10.8	51
	B11-15	1/F	10.8	53
	B11-16	1/F	10.8	52
	B11-21	2/F	13.3	64
	B11-22	2/F	13.3	64
	B11-23	2/F	13.3	58
	B11-24	2/F	13.3	56
	B11-25	2/F	13.3	56
	B11-26	2/F	13.3	55
B12	B12-01	G/F	6.3	52
	B12-02	G/F	6.3	52
	B12-03	G/F	6.3	49
	B12-04	G/F	6.3	61
	B12-11	1/F	10.8	62
	B12-12	1/F	10.8	62
	B12-13	1/F	10.8	56
	B12-14	1/F	10.8	52
	B12-15	1/F	10.8	54
	B12-16	1/F	10.8	53
	B12-21	2/F	13.3	64
	B12-21	2/F	13.3	64
	B12-22	2/F	13.3	59
	B12-23	2/F	13.3	56
	B12-24	2/F	13.3	57
	B12-25	2/F	13.3	56
	D12-20	Z/ F	13.3] 30

NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Level, L10(1-hour), dB(A)
B13	B13-01	G/F	6.3	53
	B13-02	G/F	6.3	53
	B13-03	G/F	6.3	49
	B13-04	G/F	6.3	60
	B13-11	1/F	10.8	61
	B13-12	1/F	10.8	61
	B13-13	1/F	10.8	57
	B13-14	1/F	10.8	52
	B13-15	1/F	10.8	56
	B13-16	1/F	10.8	54
	B13-21	2/F	13.3	64
	B13-22	2/F	13.3	64
	B13-23	2/F	13.3	60
	B13-24	2/F	13.3	56
	B13-24	2/F	13.3	59
	B13-26	2/F	13.3	57
B14	B13-20	G/F		59
D14			6.3 6.3	58
	B14-02	G/F		50
	B14-03	G/F	6.3	59
	B14-04	G/F	6.3	
	B14-11	1/F	10.8	61
	B14-12	1/F	10.8	61
	B14-13	1/F	10.8	58
	B14-14	1/F	10.8	62
	B14-15	1/F	10.8	60
	B14-16	1/F	10.8	58
	B14-21	2/F	13.3	63
	B14-22	2/F	13.3	63
	B14-23	2/F	13.3	61
	B14-24	2/F	13.3	64
	B14-25	2/F	13.3	62
D.4.5	B14-26	2/F	13.3	60
B15	B15-01	G/F	6.3	64
	B15-02	G/F	6.3	63
	B15-03	G/F	6.3	52
	B15-04	G/F	6.3	58
	B15-11	1/F	10.8	60
	B15-12	1/F	10.8	60
	B15-13	1/F	10.8	59
	B15-14	1/F	10.8	66
	B15-15	1/F	10.8	65
	B15-16	1/F	10.8	63
	B15-21	2/F	13.3	63
	B15-22	2/F	13.3	63
	B15-23	2/F	13.3	64
	B15-24	2/F	13.3	67
	B15-25	2/F	13.3	66
	B15-26	2/F	13.3	64

NSR	AP ID	Floor	Level,	Predicted Unmitigated Noise
1401	AI ID	1 1001	mPD	Level, L10(1-hour), dB(A)
B16	B16-01	G/F	6.3	68
	B16-02	G/F	6.3	68
	B16-03	G/F	6.3	55
	B16-04	G/F	6.3	52
	B16-11	1/F	10.8	53
	B16-12	1/F	10.8	56
	B16-13	1/F	10.8	68
	B16-14	1/F	10.8	69
	B16-15	1/F	10.8	69
	B16-16	1/F	10.8	69
	B16-21	2/F	13.3	56
	B16-22	2/F	13.3	59
	B16-23	2/F	13.3	69
	B16-24	2/F	13.3	70
	B16-25	2/F	13.3	70
	B16-26	2/F	13.3	70
B17	B17-01	G/F	6.3	68
	B17-02	G/F	6.3	68
	B17-03	G/F	6.3	55
	B17-04	G/F	6.3	52
	B17-11	1/F	10.8	53
	B17-12	1/F	10.8	53
	B17-13	1/F	10.8	53
	B17-14	1/F	10.8	68
	B17-15	1/F	10.8	68
	B17-16	1/F	10.8	68
	B17-10	2/F	13.3	56
	B17-21	2/F	13.3	56
	B17-22	2/F	13.3	57
	B17-23	2/F	13.3	70
	B17-24	2/F 2/F	13.3	70
		2/F 2/F		70
D40	B17-26		13.3	
B18	B18-01	G/F	6.3	67
	B18-02	G/F	6.3	67
	B18-03	G/F	6.3	56
	B18-04	G/F	6.3	52
	B18-11	1/F	10.8	53
	B18-12	1/F	10.8	53
	B18-13	1/F	10.8	55
	B18-14	1/F	10.8	67
	B18-15	1/F	10.8	68
	B18-16	1/F	10.8	67
	B18-21	2/F	13.3	56
	B18-22	2/F	13.3	56
	B18-23	2/F	13.3	59
	B18-24	2/F	13.3	69
	B18-25	2/F	13.3	70
	B18-26	2/F	13.3	69

			Level,	Predicted Unmitigated Noise
NSR	AP ID	Floor	mPD	Level, L10(1-hour), dB(A)
B19	B19-01	G/F	6.3	65
	B19-02	G/F	6.3	65
	B19-03	G/F	6.3	59
	B19-04	G/F	6.3	52
	B19-11	1/F	10.8	53
	B19-12	1/F	10.8	53
	B19-13	1/F	10.8	55
	B19-14	1/F	10.8	66
	B19-15	1/F	10.8	66
	B19-16	1/F	10.8	66
	B19-21	2/F	13.3	56
	B19-22	2/F	13.3	56
	B19-23	2/F	13.3	59
	B19-24	2/F	13.3	68
	B19-25	2/F	13.3	69
	B19-26	2/F	13.3	68
B20	B20-01	G/F	6.3	64
	B20-02	G/F	6.3	64
	B20-03	G/F	6.3	59
	B20-04	G/F	6.3	52
	B20-11	1/F	10.8	53
	B20-12	1/F	10.8	53
	B20-13	1/F	10.8	58
	B20-14	1/F	10.8	64
	B20-15	1/F	10.8	66
	B20-16	1/F	10.8	65
	B20-21	2/F	13.3	56
	B20-22	2/F	13.3	56
	B20-23	2/F	13.3	61
	B20-24	2/F	13.3	67
	B20-25	2/F	13.3	68
	B20-26	2/F	13.3	68
B21	B21-01	G/F	6.3	63
	B21-02	G/F	6.3	63
	B21-03	G/F	6.3	52
	B21-04	G/F	6.3	52
	B21-11	1/F	10.8	53
	B21-12	1/F	10.8	53
	B21-13	1/F	10.8	56
	B21-14	1/F	10.8	64
	B21-15	1/F	10.8	65
	B21-16	1/F	10.8	64
	B21-21	2/F	13.3	56
	B21-22	2/F	13.3	56
	B21-23	2/F	13.3	59
	B21-24	2/F	13.3	67
	B21-25	2/F	13.3	68
	B21-26	2/F	13.3	67
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			Lovel	Predicted Unmitigated Noise
NSR	AP ID	Floor	Level, mPD	Level, L10(1-hour), dB(A)
B22	B22-01	G/F	6.3	63
	B22-02	G/F	6.3	63
	B22-03	G/F	6.3	53
	B22-04	G/F	6.3	51
	B22-11	1/F	10.8	53
	B22-12	1/F	10.8	53
	B22-13	1/F	10.8	53
	B22-14	1/F	10.8	63
	B22-15	1/F	10.8	65
	B22-16	1/F	10.8	64
	B22-21	2/F	13.3	56
	B22-22	2/F	13.3	56
	B22-23	2/F	13.3	58
	B22-24	2/F	13.3	67
	B22-25	2/F	13.3	68
	B22-26	2/F	13.3	68
B23	B23-01	G/F	6.3	61
D20	B23-02	G/F	6.3	62
	B23-03	G/F	6.3	55
	B23-04	G/F	6.3	51
	B23-11	1/F	10.8	53
	B23-12	1/F	10.8	53
	B23-13	1/F	10.8	53
	B23-14	1/F	10.8	64
	B23-15	1/F	10.8	64
	B23-16	1/F	10.8	63
	B23-21	2/F	13.3	56
	B23-22	2/F	13.3	56
	B23-23	2/F	13.3	58
	B23-24	2/F	13.3	67
	B23-25	2/F	13.3	68
	B23-26	2/F	13.3	68
B24	B24-01	G/F	6.3	62
<i>D</i>	B24-02	G/F	6.3	63
	B24-03	G/F	6.3	62
	B24-04	G/F	6.3	55
	B24-11	1/F	10.8	56
	B24-12	1/F	10.8	52
	B24-13	1/F	10.8	55
	B24-14	1/F	10.8	63
	B24-15	1/F	10.8	65
	B24-16	1/F	10.8	65
	B24-21	2/F	13.3	58
	B24-22	2/F	13.3	56
	B24-23	2/F	13.3	60
	B24-24	2/F	13.3	68
	B24-25	2/F	13.3	69
	B24-26	2/F	13.3	69

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NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Unmitigated
C01	C01-11	1/F	9.8	58
	C01-12	1/F	9.8	57
	C01-13	1/F	9.8	70
	C01-14	1/F	9.8	69
	C01-21	2/F	14.3	61
	C01-22	2/F	14.3	59
	C01-23	2/F	14.3	71
	C01-24	2/F	14.3	70
C02	C02-11	1/F	9.8	55
	C02-12	1/F	9.8	55
	C02-13	1/F	9.8	72
	C02-14	1/F	9.8	70
	C02-21	2/F	14.3	58
	C02-22	2/F	14.3	57
	C02-23	2/F	14.3	72
	C02-24	2/F	14.3	71
C03	C03-11	1/F	9.8	56
	C03-12	1/F	9.8	54
	C03-13	1/F	9.8	72
	C03-14	1/F	9.8	48
	C03-21	2/F	14.3	58
	C03-22	2/F	14.3	58
	C03-23	2/F	14.3	72
	C03-24	2/F	14.3	53
C04	C04-11	1/F	9.8	55
	C04-12	1/F	9.8	54
	C04-13	1/F	9.8	71
	C04-14	1/F	9.8	48
	C04-21	2/F	14.3	58
	C04-22	2/F	14.3	57
	C04-23	2/F	14.3	72
	C04-24	2/F	14.3	53

			Level,	Predicted Unmitigated Noise
NSR	AP ID	Floor	mPD	Level, L10(1-hour), dB(A)
C05	C05-11	1/F	9.8	55
	C05-12	1/F	9.8	54
	C05-13	1/F	9.8	71
	C05-14	1/F	9.8	48
	C05-21	2/F	14.3	58
	C05-22	2/F	14.3	57
	C05-23	2/F	14.3	71
	C05-24	2/F	14.3	53
C06	C06-11	1/F	9.8	55
	C06-12	1/F	9.8	54
	C06-13	1/F	9.8	71
	C06-14	1/F	9.8	48
	C06-21	2/F	14.3	58
	C06-22	2/F	14.3	57
	C06-23	2/F	14.3	71
	C06-24	2/F	14.3	53
C07	C07-11	1/F	9.8	55
	C07-12	1/F	9.8	54
	C07-13	1/F	9.8	71
	C07-14	1/F	9.8	48
	C07-21	2/F	14.3	58
	C07-22	2/F	14.3	58
	C07-23	2/F	14.3	71
	C07-24	2/F	14.3	53
C08	C08-11	1/F	9.8	58
	C08-12	1/F	9.8	54
	C08-13	1/F	9.8	70
	C08-14	1/F	9.8	48
	C08-21	2/F	14.3	59
	C08-22	2/F	14.3	61
	C08-23	2/F	14.3	71
	C08-24	2/F	14.3	53

NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Level, L10(1-hour), dB(A)
C09	C09-11	1/F	9.8	61
	C09-12	1/F	9.8	54
	C09-13	1/F	9.8	70
	C09-14	1/F	9.8	48
	C09-21	2/F	14.3	62
	C09-22	2/F	14.3	62
	C09-23	2/F	14.3	70
	C09-24	2/F	14.3	53
C10	C10-11	1/F	9.8	60
	C10-12	1/F	9.8	53
	C10-13	1/F	9.8	69
	C10-14	1/F	9.8	48
	C10-21	2/F	14.3	62
	C10-22	2/F	14.3	61
	C10-23	2/F	14.3	70
	C10-24	2/F	14.3	53
C11	C11-11	1/F	9.8	57
	C11-12	1/F	9.8	53
	C11-13	1/F	9.8	69
	C11-14	1/F	9.8	48
	C11-21	2/F	14.3	61
	C11-22	2/F	14.3	59
	C11-23	2/F	14.3	69
	C11-24	2/F	14.3	53
C12	C12-11	1/F	9.8	55
	C12-12	1/F	9.8	55
	C12-13	1/F	9.8	68
	C12-14	1/F	9.8	48
	C12-21	2/F	14.3	59
	C12-22	2/F	14.3	57
	C12-23	2/F	14.3	69
	C12-24	2/F	14.3	53

NSR	AP ID	Floor	Level,	Predicted Unmitigated Noise
	AI ID	1 1001	mPD	Level, L10(1-hour), dB(A)
C13	C13-11	1/F	9.8	63
	C13-12	1/F	9.8	64
	C13-13	1/F	9.8	62
	C13-14	1/F	9.8	60
	C13-21	2/F	14.3	64
	C13-22	2/F	14.3	64
	C13-23	2/F	14.3	62
	C13-24	2/F	14.3	62
C14	C14-11	1/F	9.8	61
	C14-12	1/F	9.8	61
	C14-13	1/F	9.8	62
	C14-14	1/F	9.8	47
	C14-21	2/F	14.3	62
	C14-22	2/F	14.3	62
	C14-23	2/F	14.3	63
	C14-24	2/F	14.3	52
C15	C15-11	1/F	9.8	58
	C15-12	1/F	9.8	59
	C15-13	1/F	9.8	63
	C15-14	1/F	9.8	47
	C15-21	2/F	14.3	61
	C15-22	2/F	14.3	60
	C15-23	2/F	14.3	63
	C15-24	2/F	14.3	52
C16	C16-11	1/F	9.8	57
	C16-12	1/F	9.8	53
	C16-13	1/F	9.8	63
	C16-14	1/F	9.8	47
	C16-21	2/F	14.3	59
	C16-22	2/F	14.3	58
	C16-23	2/F	14.3	64
	C16-24	2/F	14.3	52

			Level,	Predicted Unmitigated Noise
NSR	AP ID	Floor	mPD	Level, L10(1-hour), dB(A)
C17	C17-11	1/F	9.8	55
017	C17-12	1/F	9.8	51
	C17-13	1/F	9.8	64
	C17-14	1/F	9.8	47
	C17-21	2/F	14.3	58
	C17-22	2/F	14.3	57
	C17-23	2/F	14.3	64
	C17-24	2/F	14.3	52
C18	C18-11	1/F	9.8	54
	C18-12	1/F	9.8	51
	C18-13	1/F	9.8	64
	C18-14	1/F	9.8	47
	C18-21	2/F	14.3	58
	C18-22	2/F	14.3	56
	C18-23	2/F	14.3	64
	C18-24	2/F	14.3	52
C19	C19-11	1/F	9.8	54
	C19-12	1/F	9.8	51
	C19-13	1/F	9.8	64
	C19-14	1/F	9.8	47
	C19-21	2/F	14.3	57
	C19-22	2/F	14.3	55
	C19-23	2/F	14.3	65
	C19-24	2/F	14.3	52
C20	C20-11	1/F	9.8	54
	C20-12	1/F	9.8	51
	C20-13	1/F	9.8	64
	C20-14	1/F	9.8	47
	C20-21	2/F	14.3	57
	C20-22	2/F	14.3	54
	C20-23	2/F	14.3	65
	C20-24	2/F	14.3	52

NSR	AP ID	Floor	Level,	Predicted Unmitigated Noise
	AI ID		mPD	Level, L10(1-hour), dB(A)
C21	C21-11	1/F	9.8	53
	C21-12	1/F	9.8	51
	C21-13	1/F	9.8	64
	C21-14	1/F	9.8	47
	C21-21	2/F	14.3	57
	C21-22	2/F	14.3	54
	C21-23	2/F	14.3	65
	C21-24	2/F	14.3	52
C22	C22-11	1/F	9.8	53
	C22-12	1/F	9.8	51
	C22-13	1/F	9.8	64
	C22-14	1/F	9.8	47
	C22-21	2/F	14.3	57
	C22-22	2/F	14.3	54
	C22-23	2/F	14.3	65
	C22-24	2/F	14.3	52
C23	C23-11	1/F	9.8	53
	C23-12	1/F	9.8	51
	C23-13	1/F	9.8	64
	C23-14	1/F	9.8	48
	C23-21	2/F	14.3	57
	C23-22	2/F	14.3	55
	C23-23	2/F	14.3	65
	C23-24	2/F	14.3	52
C24	C24-11	1/F	9.8	53
	C24-12	1/F	9.8	51
	C24-13	1/F	9.8	64
	C24-14	1/F	9.8	48
	C24-21	2/F	14.3	57
	C24-22	2/F	14.3	54
	C24-23	2/F	14.3	65
	C24-24	2/F	14.3	52

NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Level, L10(1-hour), dB(A)
C25	C25-11	1/F	9.8	53
	C25-12	1/F	9.8	50
	C25-13	1/F	9.8	65
	C25-14	1/F	9.8	48
	C25-21	2/F	14.3	57
	C25-22	2/F	14.3	54
	C25-23	2/F	14.3	65
	C25-24	2/F	14.3	52

			Lovel	Dradiated Unmitigated Naisa
NSR	AP ID	Floor	Level,	Predicted Unmitigated Noise
11011	7	1 1001	mPD	Level, L10(1-hour), dB(A)
D01	D01-01	G/F	6.3	66
	D01-02	G/F	6.3	66
	D01-03	G/F	6.3	55
	D01-04	G/F	6.3	55
	D01-11	1/F	10.8	66
	D01-12	1/F	10.8	57
	D01-13	1/F	10.8	57
D02	D02-01	G/F	6.3	66
	D02-02	G/F	6.3	65
	D02-03	G/F	6.3	54
	D02-04	G/F	6.3	54
	D02-11	1/F	10.8	66
	D02-12	1/F	10.8	56
	D02-13	1/F	10.8	56

			Level,	Predicted Unmitigated Noise
NSR	AP ID	Floor	mPD	Level, L10(1-hour), dB(A)
E01	E01-01	G/F	6.3	63
	E01-02	G/F	6.3	58
	E01-03	G/F	6.3	54
	E01-04	G/F	6.3	54
	E01-11	1/F	10.8	64
	E01-12	1/F	10.8	58
	E01-13	1/F	10.8	53
	E01-14	1/F	10.8	57
	E01-15	1/F	10.8	57
E02	E02-01	G/F	6.3	63
	E02-02	G/F	6.3	55
	E02-03	G/F	6.3	53
	E02-04	G/F	6.3	53
	E02-11	1/F	10.8	64
	E02-12	1/F	10.8	58
	E02-13	1/F	10.8	53
	E02-14	1/F	10.8	56
	E02-15	1/F	10.8	55
E03	E03-01	G/F	6.3	63
	E03-02	G/F	6.3	54
	E03-03	G/F	6.3	52
	E03-04	G/F	6.3	52
	E03-11	1/F	10.8	64
	E03-12	1/F	10.8	58
	E03-13	1/F	10.8	53
	E03-14	1/F	10.8	55
	E03-15	1/F	10.8	55
E04	E04-01	G/F	6.3	64
	E04-02	G/F	6.3	55
	E04-03	G/F	6.3	52
	E04-04	G/F	6.3	52
	E04-11	1/F	10.8	64
	E04-12	1/F	10.8	59
	E04-13	1/F	10.8	54
	E04-14	1/F	10.8	55
	E04-15	1/F	10.8	54
E05	E05-01	G/F	6.3	64
1	E05-02	G/F	6.3	55
1	E05-03	G/F	6.3	53
1	E05-04	G/F	6.3	53
1	E05-11	1/F	10.8	63
1	E05-12	1/F	10.8	58
1	E05-13	1/F	10.8	54
1	E05-14	1/F	10.8	56
	E05-15	1/F	10.8	54

	E05-14	1/F	10.8	50
	E05-15	1/F	10.8	54
NSR	AP ID	Floor	Level,	Predicted Unmitigated Noise
NOK	AP ID	FIOOI	mPD	Level, L10(1-hour), dB(A)
E16	E16-01	G/F	6.3	58
	E16-02	G/F	6.3	60
	E16-03	G/F	6.3	65
	E16-04	G/F	6.3	65
	E16-11	1/F	10.8	60
	E16-12	1/F	10.8	61
	E16-13	1/F	10.8	66
	E16-14	1/F	10.8	66
	E16-15	1/F	10.8	65
				<u> </u>

NSR	AP ID	Floor	Level,	Predicted Unmitigated Noise
NOK	AP ID	FIOOI	mPD	Level, L10(1-hour), dB(A)
E06	E06-01	G/F	6.3	63
	E06-02	G/F	6.3	55
	E06-03	G/F	6.3	52
	E06-04	G/F	6.3	53
	E06-11	1/F	10.8	63
	E06-12	1/F	10.8	60
	E06-13	1/F	10.8	58
	E06-14	1/F	10.8	56
	E06-15	1/F	10.8	54
E07	E07-01	G/F	6.3	58
	E07-02	G/F	6.3	56
	E07-03	G/F	6.3	57
	E07-04	G/F	6.3	56
	E07-11	1/F	10.8	59
	E07-12	1/F	10.8	58
	E07-13	1/F	10.8	57
	E07-14	1/F	10.8	59
	E07-15	1/F	10.8	56
E08	E08-01	G/F	6.3	57
	E08-02	G/F	6.3	48
	E08-03	G/F	6.3	55
	E08-04	G/F	6.3	55
	E08-11	1/F	10.8	57
	E08-12	1/F	10.8	52
	E08-13	1/F	10.8	55
	E08-14	1/F	10.8	58
	E08-15	1/F	10.8	56
E09	E09-01	G/F	6.3	55
	E09-02	G/F	6.3	49
	E09-03	G/F	6.3	54
	E09-04	G/F	6.3	54
	E09-11	1/F	10.8	56
	E09-12	1/F	10.8	56
	E09-13	1/F	10.8	53
	E09-14	1/F	10.8	57
	E09-15	1/F	10.8	56
E10	E10-01	G/F	6.3	55
	E10-02	G/F	6.3	59
	E10-03	G/F	6.3	59
	E10-04	G/F	6.3	59
	E10-11	1/F	10.8	57
	E10-12	1/F	10.8	54
	E10-13	1/F	10.8	51
	E10-14	1/F	10.8	60
	E10-15	1/F	10.8	59

NSR	AP ID	Floor	Level, mPD	Predicted Unmitigated Noise Level, L10(1-hour), dB(A)
E11	E11-01	G/F	6.3	55
	E11-02	G/F	6.3	49
	E11-03	G/F	6.3	58
	E11-04	G/F	6.3	58
	E11-11	1/F	10.8	57
	E11-12	1/F	10.8	53
	E11-13	1/F	10.8	51
	E11-14	1/F	10.8	59
	E11-15	1/F	10.8	58
E12	E12-01	G/F	6.3	54
	E12-02	G/F	6.3	49
	E12-03	G/F	6.3	57
	E12-04	G/F	6.3	57
	E12-11	1/F	10.8	56
	E12-12	1/F	10.8	53
	E12-13	1/F	10.8	51
	E12-14	1/F	10.8	58
	E12-15	1/F	10.8	58
E13	E13-01	G/F	6.3	59
L 13	E13-02	G/F	6.3	59
	E13-03	G/F	6.3	59
	E13-04	G/F	6.3	58
	E13-11	1/F	10.8	60
	E13-12	1/F	10.8	60
	E13-13	1/F	10.8	60
	E13-14	1/F	10.8	60
	E13-15	1/F	10.8	56
E14	E14-01	G/F	6.3	57
	E14-02	G/F	6.3	48
	E14-03	G/F	6.3	56
	E14-04	G/F	6.3	56
	E14-11	1/F	10.8	58
	E14-12	1/F	10.8	53
	E14-13	1/F	10.8	55
	E14-14	1/F	10.8	58
	E14-15	1/F	10.8	55
E15	E15-01	G/F	6.3	57
	E15-02	G/F	6.3	47
	E15-03	G/F	6.3	55
	E15-04	G/F	6.3	55
	E15-04	1/F	10.8	57
	E15-12	1/F	10.8	53
	E15-12	1/F	10.8	52
	E15-13	1/F	10.8	57
	E15-14	1/F	10.8	55
	E 10-10	I/F	10.0	JU

Note: Values in red exceed the noise criteria.

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Appendix 3.3

Road Traffic Noise Impact Assessment Results – Mitigated Scenario



Predicted Results of Road Traffic Noise Impact Assessment for Year 2040 - Mitigated Scenario (Peak Hour during Morning)

NSR	AP ID	Floor	Level, mPD	Predicted Mitigated Noise Level, L10(1-hour), dB(A)
C01	C01-11	1/F	9.8	56
CUI	C01-11	1/F	9.8	54
	C01-12	1/F	9.8	Fixed window
	C01-13	1/F	9.8	Fixed window Fixed window
	C01-14	2/F	14.3	60
	C01-21	2/F	14.3	58
	C01-22	2/F	14.3	Fixed window
	C01-23	2/F	14.3	Fixed window
<u> </u>				
C02	C02-11	1/F	9.8	54
	C02-12	1/F	9.8	50
	C02-13	1/F	9.8	Fixed window
	C02-14	1/F	9.8	Fixed window
	C02-21	2/F	14.3	58
	C02-22	2/F	14.3	57
	C02-23	2/F	14.3	Fixed window
	C02-24	2/F	14.3	Fixed window
C03	C03-11	1/F	9.8	55
	C03-12	1/F	9.8	50
	C03-13	1/F	9.8	Fixed window
	C03-14	1/F	9.8	Fixed window
	C03-21	2/F	14.3	58
	C03-22	2/F	14.3	57
	C03-23	2/F	14.3	Fixed window
	C03-24	2/F	14.3	Fixed window
C04	C04-11	1/F	9.8	55
	C04-12	1/F	9.8	50
	C04-13	1/F	9.8	Fixed window
	C04-14	1/F	9.8	Fixed window
	C04-21	2/F	14.3	58
	C04-22	2/F	14.3	57
	C04-23	2/F	14.3	Fixed window
	C04-24	2/F	14.3	Fixed window

NSR	AP ID	Floor	Level,	Predicted Mitigated Noise
NOK	AP ID	FIOOI	mPD	Level, L10(1-hour), dB(A)
C05	C05-11	1/F	9.8	55
	C05-12	1/F	9.8	50
	C05-13	1/F	9.8	Fixed window
	C05-14	1/F	9.8	Fixed window
	C05-21	2/F	14.3	58
	C05-22	2/F	14.3	57
	C05-23	2/F	14.3	Fixed window
	C05-24	2/F	14.3	Fixed window
C06	C06-11	1/F	9.8	54
	C06-12	1/F	9.8	50
	C06-13	1/F	9.8	Fixed window
	C06-14	1/F	9.8	Fixed window
	C06-21	2/F	14.3	58
	C06-22	2/F	14.3	57
	C06-23	2/F	14.3	Fixed window
	C06-24	2/F	14.3	Fixed window
C07	C07-11	1/F	9.8	54
	C07-12	1/F	9.8	50
	C07-13	1/F	9.8	Fixed window
	C07-14	1/F	9.8	Fixed window
	C07-21	2/F	14.3	58
	C07-22	2/F	14.3	57
	C07-23	2/F	14.3	Fixed window
	C07-24	2/F	14.3	Fixed window
C08	C08-11	1/F	9.8	55
	C08-12	1/F	9.8	50
	C08-13	1/F	9.8	Fixed window
	C08-14	1/F	9.8	Fixed window
	C08-21	2/F	14.3	58
	C08-22	2/F	14.3	58
	C08-23	2/F	14.3	Fixed window
	C08-24	2/F	14.3	Fixed window

NSR	AP ID	Floor	Level, mPD	Predicted Mitigated Noise Level, L10(1-hour), dB(A)
C09	C09-11	1/F	9.8	58
	C09-12	1/F	9.8	50
	C09-13	1/F	9.8	Fixed window
	C09-14	1/F	9.8	Fixed window
	C09-21	2/F	14.3	60
	C09-22	2/F	14.3	61
	C09-23	2/F	14.3	Fixed window
	C09-24	2/F	14.3	Fixed window
C10	C10-11	1/F	9.8	60
	C10-12	1/F	9.8	52
	C10-13	1/F	9.8	Fixed window
	C10-14	1/F	9.8	Fixed window
	C10-21	2/F	14.3	62
	C10-22	2/F	14.3	61
	C10-23	2/F	14.3	Fixed window
	C10-24	2/F	14.3	Fixed window
C11	C11-11	1/F	9.8	57
	C11-12	1/F	9.8	53
	C11-13	1/F	9.8	Fixed window
	C11-14	1/F	9.8	Fixed window
	C11-21	2/F	14.3	61
	C11-22	2/F	14.3	59
	C11-23	2/F	14.3	Fixed window
	C11-24	2/F	14.3	Fixed window
C12	C12-11	1/F	9.8	54
	C12-12	1/F	9.8	55
	C12-13	1/F	9.8	Fixed window
	C12-14	1/F	9.8	Fixed window
	C12-21	2/F	14.3	58
	C12-22	2/F	14.3	57
	C12-23	2/F	14.3	Fixed window
	C12-24	2/F	14.3	Fixed window

Remark 1: With regards to the above, relevant noise mitigation measures such as noise barriers were also proposed due to fixed noise sources, thus the above figures have taken into account such proposed noise mitigation measures. Only the NSRs whose noise levels have exceeded the noise criteria have been presented in the table to show

compliance. For other NSRs, their noise level under unmitigated scenario can already comply with relevant noise criteria.

Remark 2: For C01 - C12, the proposed internal layout design with fixed glazing has been incorporated.

Appendix 4.1

Inventory of Potential Industrial Noise Sources



Sources of Industrial Noise

ID.	Description	A 41 14 [1]	Coord	linates	SWL,	mPD+	Measured SPL,	Distance from	Distance
ID	Description	Activity [1]	х	у	dB(A) [2]	1m	dB(A) [2][3]	Source, m [2]	Correction, dB(A)
S1	Hung Kee Metal Recycling International Limited	Fork Lift	823601	836709	91.4	4.2	66.5	7.0	24.9
S2	Dorfield Limited	Fork Lift	823652	836655	94.9	4.7	66.9	10.0	28.0
S3-1	祥發五金貿易有限公司	Scraping Metal	823605	836630	96.8	4.9	71.4	7.4	25.4
S3-2	祥發五金貿易有限公司	Lorry Movement with Crane	823627	836649	99.0	4.9	73.0	7.9	26.0
S4	Wing Tat Logistics Group Limited	Fork Lift	823089	836544	94.4	4.6	69.5	7.0	24.9
S5	威盛物流	Loading Unloading of Goods	823153	836442	98.5	4.9	72.4	8.0	26.1
S6	Santa Fe	Fork Lift	823001	836707	98.0	5.6	71.9	8.0	26.1
S7	Bun Kee (International) Limitied	Loading Unloading of Goods Carried Out By Lorry with Crane	822966	836729	95.7	5.1	66.9	11.0	28.8
S8	Hichain Logistics Group	Fork Lift	823027	836786	91.4	5.7	66.5	7.0	24.9
S9	Taiwan Express	Fork Lift	823059	836822	92.5	5.7	68.9	6.0	23.6
S10	Open storage site (east) [4]	Lorry Movement with Crane	823216	836713	99.0	5.2	73.0	7.9	26.0
S10a	Open storage site (east) [4]	Lorry Movement with Crane	823217	836734	99.0	5.2	73.0	7.9	26.0
S10b	Open storage site (east) [4]	Lorry Movement with Crane	823219	836721	99.0	5.2	73.0	7.9	26.0
S10c	Open storage site (east) [4]	Lorry Movement with Crane	823210	836699	99.0	5.2	73.0	7.9	26.0
S11	Open storage site (west) [4]	Lorry Movement with Crane	823449	836546	99.0	7.4	73.0	7.9	26.0
S11a	Open storage site (west) [4]	Lorry Movement with Crane	823464	836563	99.0	7.4	73.0	7.9	26.0
S11b	Open storage site (west) [4]	Lorry Movement with Crane	823447	836539	99.0	7.4	73.0	7.9	26.0

Notes:

Plant inventory at each noise source was based on site surveys in July 2019, August 2019, September 2019, March 2020, June 2020, May 2021, July 2021, July 2022, and September 2023. As observed during the site surveys, noisy plants were only found to operate occasionally. No night-time operation was observed during site surveys and the noise sources were found to be closed at night-time.

- [1] Site visits were carried out and that the above noise sources had no night-time operation. Type of noise sources are based on site observation during site visit.
- [2] Sound power levels (SWL) of the noise noise sources are determined based on the sound pressure levels (SPL) measurement conducted on-site and general acoustic principal.
- [3] SPLs were measured at free-field.
- S10, S10a, S10b, and S10c represent the notional noise source location at noise source S10 & with respective to different NSR locations. Accordingly, S11, S11a, and S11b represent the notional noise source location at noise source S11 & with respective to different NSR locations.

Appendix 4.2
Industrial Noise Impact Assessment Results



				T	Noise S	ource (NS)		Distance	Correction	ons, dB(A	Unmitigated		Consider for	Barrier	Horizontal	Horizontal	NS level (1m	Slant	Slant	Distance from	Path	Path	Mitigated			
ID	Floor			x	у	Height		x		WL, B(A)	from NS to	Distance		Noise Level,	Intensity	Path Difference?	Height, mPD	Distance from AP to Barrier,	Distance from NS to Barrier,	above	Distance from AP to Barrier,	Distance from Barrier to NS,	AP to NS, m [C]	Difference , m	Difference Correction,	Noise Level, dB(A) [7]
A01-01	G	A01-01-G	A01-01-S1	823356	836744			823601	836709		247.6	-55.9	3.0	39	7124	N	-	-	-	ground -	-	-	-		-	39
		A01-01-G	A01-01-S3-1				S3-1	823605	836630	96.8	273.4	-56.7	3.0	43	20173	N	-	-	-	-	-	-	-	-	-	43
		A01-01-G	A01-01-S3-2				S3-2	823627	836649 9	99.0	287.3	-57.2	3.0	45	30096	N	-	-	-	-	-	-	-	-	-	45
		A01-01-G										Total SPL	, dB(A) [4]	48		'			'	'				Total S	PL, dB(A) [4]:	48
E13-02	G	E13-02-G	E13-02-S4	823280	836751	6.3	S4	823089	836544	94.4	281.2	-57.0	3.0	40	11041	Y	10.2	22.8	258.4	4.6	23.1	258.5	281.2	0.4	14.3	26
'		E13-02-G	E13-02-S6				S6	823001		98.0	282.0	-57.0	3.0	44	24862	Y	10.2	7.8	274.2	5.6	8.7	274.3	282.0	1.0	17.9	26
		E13-02-G	E13-02-S8				S8	823027	836786	91.4	255.3	-56.1	3.0	38	6699	Y	10.2	6.7	248.6	5.7	7.8	248.7	255.3	1.1	18.4	20
		E13-02-G	E13-02-S9				S9	823059	836822 9	92.5	232.2	-55.3	3.0	40	10392	Y	10.2	6.5	225.7	5.7	7.6	225.7	232.2	1.1	18.5	22
		E13-02-G	E13-02-S10a				S10a	823217	836734	99.0	64.9	-44.2	3.0	58	590293	Y	10.2	8.5	56.4	5.2	9.4	56.6	64.9	1.1	18.3	39
		E13-02-G										Total SPL	_, dB(A) ^[4]	58										Total S	PL, dB(A) ^[4] :	40
E19-02	G	E19-02-G	E19-02-S4	823261	836707	6.3		823089	836544		236.5	-55.5	3.0	42	15614	Y	13.0	23.7	212.8	4.6	24.6	213.0	236.5	1.1	18.4	24
		E19-02-G	E19-02-S6				S6	823001	836707	98.0	259.4	-56.3	3.0	45	29400	Y	13.0	9.9	249.5	5.6	12.0	249.6	259.4	2.2	20.0	25
		E19-02-G	E19-02-S7				S7	822966			295.5	-57.4	3.0	41	13445	Y	13.0	9.5	286.0	5.1	11.6	286.1	295.5	2.2	20.0	21
		E19-02-G	E19-02-S8				S8		836786		246.7	-55.8	3.0	39	7178	Y	13.0	8.9	237.8	5.7	11.1	237.9	246.7	2.4	20.0	19
		E19-02-G	E19-02-S9				S9	823059		92.5	232.2	-55.3	3.0	40	10388	Y	13.0	8.8	223.4	5.7	11.1	223.5	232.2	2.4	20.0	20
		E19-02-G E19-02-G	E19-02-S10b				S10b	823219	836721	39.0	44.3	-40.9		61 61	1265881	Y	13.0	8.9	35.4	5.2	11.1	36.3	44.3	3.1	20.0	41 41
		E19-02-G										Total SPL	_, dB(A) **	01										I otal S	SPL, dB(A) ^[4] :	41
E22-04	G	E22-04-G		823257	836691	6.3			836544		223.4	-55.0	3.0	42	17505	Y	13.0	14.4	209.0	4.6	15.9	209.1	223.4	1.7	20.0	22
		E22-04-G	E22-04-S6				S6 S7	823001			256.5	-56.2	3.0	45	30060	Y	13.0	12.5	244.0	5.6	14.2	244.1	256.5	1.8	20.0	25
		E22-04-G E22-04-G	E22-04-S7 E22-04-S8				S8	822966 823027			293.8 249.1	-57.4 -55.9	3.0	41 38	13606 7039	Y	13.0	12.5 12.5	281.3 236.6	5.1 5.7	14.2 14.2	281.4 236.7	293.8 249.1	1.8	20.0	21 18
		E22-04-G	E22-04-S9				S9	823059		92.5	237.6	-55.5	3.0	40	9919	Y	13.0	12.5	225.1	5.7	14.2	225.3	237.6	1.8	20.0	20
		E22-04-G	E22-04-S10c						836699		48.1	-41.6	3.0	60	1073719	Ÿ	13.0	12.5	35.6	5.2	14.2	36.4	48.1	2.5	20.0	40
		E22-04-G					1		1			Total SPL					10.0								PL, dB(A) [4]:	
E41-02	G	E41-02-G	E41-02-S4	823340	836544	6.3	S4	823089	836544	94.4	251.2	-56.0	3.0	41	13842	N	Ι.								T -	41
		E41-02-G	E41-02-S5				S5		836442		213.6	-54.6	3.0	47	48990	N	-	-	-	-	-	-	-	-		47
		E41-02-G										Total SPL	., dB(A) ^[4]	48		•		•	•					Total S	PL, dB(A) [4]:	48
E42-04	G	E42-04-G	E42-04-S1	823424	836540	6.3	S1	823601	836709	91.4	245.0	-55.8	3.0	39	7275	Y	12.6	18.4	226.6	4.2	19.4	226.8	245.0	1.2	18.8	20
'		E42-04-G	E42-04-S2				S2	823652			254.7	-56.1	3.0	42	15062	Y	12.6	11.6	243.1	4.7	13.2	243.2	254.7	1.7	20.0	22
		E42-04-G	E42-04-S3-1				S3-1	823605	836630 9	96.8	202.1	-54.1	3.0	46	36943	Y	12.6	11.6	190.5	4.9	13.2	190.6	202.1	1.8	20.0	26
		E42-04-G	E42-04-S3-2				S3-2	823627	836649	99.0	230.5	-55.3	3.0	47	46779	Y	12.6	11.9	218.6	4.9	13.5	218.7	230.5	1.7	20.0	27
		E42-04-G	E42-04-S11b				S11b	823447	836539	99.0	23.0	-35.2	3.0	67	4705736	Y	12.6	8.2	14.8	7.4	10.3	15.7	23.0	3.0	20.0	47
		E42-04-G										Total SPL	_, dB(A) ^[4]	67										Total S	PL, dB(A) ^[4] :	47
E44-03	G	E44-03-G	E44-03-S1	823430	836555	6.3	S1	823601	836709	91.4	230.6	-55.3	3.0	39	8210	Y	12.6	17.2	213.4	4.2	18.3	213.6	230.6	1.3	19.1	20
		E44-03-G	E44-03-S2				S2	823652	836655	94.9	243.1	-55.7	3.0	42	16542	Y	12.6	11.0	232.1	4.7	12.7	232.2	243.1	1.8	20.0	22
		E44-03-G	E44-03-S3-1				S3-1	823605	836630	96.8	190.5	-53.6	3.0	46	41556	Y	12.6	10.9	179.6	4.9	12.6	179.8	190.5	1.9	20.0	26
		E44-03-G	E44-03-S3-2				S3-2	823627		99.0	218.6	-54.8	3.0	47	52011	Y	12.6	11.3	207.3	4.9	12.9	207.4	218.6	1.8	20.0	27
		E44-03-G	E44-03-S11				S11	823449	836546	99.0	21.1	-34.5	3.0	67	5577630	Y	12.6	7.7	13.4	7.4	9.9	14.4	21.1	3.2	20.0	47
		E44-03-G										Total SPL	_, dB(A) ^[4]	68										Total S	PL, dB(A) ^[4] :	48
A01-11	1	A01-11-1	A01-11-S1	823353	836746	9.8	S1	823601	836709	91.4	250.7	-56.0	3.0	38	6950	N	-	-	-	-	-	-	-	-	-	38
		A01-11-1	A01-11-S3-1					823605	836630		276.7	-56.8	3.0	43	19703	N	-	-	-	-	-	-	-	-	-	43
		A01-11-1	A01-11-S3-2				S3-2	823627	836649	99.0	290.5	-57.3	3.0	45	29433	N	-	-	-	-	-	-	-	-	-	45
		A01-11-1										Total SPL	_, dB(A) ^[4]	47										Total S	PL, dB(A) [4]:	47
A02-11	1	A02-11-1	A02-11-S1	823349	836737	9.8	S1	823601	836709	91.4	253.8	-56.1	3.0	38	6781	N	-			-		-	-	-	-	38
		A02-11-1	A02-11-S3-1						836630		277.1	-56.9	3.0	43	19643	N	-	-	-	-	-	-	-	-	-	43
		A02-11-1	A02-11-S3-2				S3-2	823627	836649	99.0	291.8	-57.3		45	29177	N	-	-	-	-	-	-	-	-	-	45
		A02-11-1										Total SPL	_, dB(A) ^[4]	: 47										Total S	PL, dB(A) [4]:	47

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Q/ProjectsiFDBNPWWREA00/05 Assessmentsi02 Noisel01 Fixed Plant/R8923_v5.0/R8923_v5.0_App 4.1 to 4.3 - 20231228.xisx

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Confidential

	Assessment Point (AP) Noise Source									Distance	Correction	ns. dB(A)	Unmitigated		Consider for	Barrier	Horizontal	Horizontal	NS level (1m	Slant	Slant	Distance from	Path	Path	Mitigated
ID	Floor			x	у	Height	t in	×	. SWL,	from NS to		Façade	Noise Level,	Intensity	Path	Height,	Distance from	Distance from	above	Distance from	Distance from	AP to NS, m	Difference		Noise Level,
ID	FIOOI			×	У	, mPD	םיו ו	, x	y dB(A)	AP, m ^[1]	Distance	raçaue	dB(A) [2][3][4]		Difference?	mPD	AP to Barrier,	NS to Barrier,	ground	AP to Barrier	, Barrier to NS,	[C]	, m	Correction,	dB(A) [7]
C01-11	1	C01-11-1	C01-11-S6	922227	926616	9.8	100	922001	836707 98.0	253.1	-56.1	3.0	45	30871	N	Ι.			T -	1		-	T -	- 1	45
		C01-11-1	C01-11-S7	023237	030010	5.0			836729 95.7	294.0	-57.4	3.0	41	13588	N	1	- :	- :	 	+ :	-	-	-	-	41
		C01-11-1	C01-11-S8				S8		836786 91.4	270.7	-56.6	3.0	38	5960	N	-	-	-	-	-	-	-	-	-	38
		C01-11-1	C01-11-S9				S9	823059	836822 92.5	272.7	-56.7	3.0	39	7530	N	-	-	-	-	-	-	-	-	-	39
		C01-11-1	C01-11-S10c				S10c	823210	836699 99.0	87.9	-46.9	3.0	55	321250	Y	15.2	32.9	55.0	5.2	33.3	55.9	87.9	1.3	19.3	36
		C01-11-1									Total SPL,	dB(A) [4]:	56										Total S	PL, dB(A) ^[4] :	48
004.40		7004 40 4	004 40 04	000000	000004	0.0	104	1000000	000544 04.4	450.0	540	2.0	40	38404	T 101	Ι.									
C01-13	1	C01-13-1 C01-13-1	C01-13-S4 C01-13-S5	823229	836601	9.8	S5	823153	836544 94.4 836442 98.5	150.8 176.3	-51.6 -52.9	3.0	46 49	71910	[9]	1	-	-	-	 			-		-
		C01-13-1	C01-13-S6				S6		836707 98.0	250.7	-56.0	3.0	45	31459	[9]		-	-		 	-	-			-
		C01-13-1	C01-13-S7				S7		836729 95.7	291.9	-57.3	3.0	41	13778	[9]	-	-	-	-	-	-	-	-	-	-
		C01-13-1	C01-13-S8				S8		836786 91.4	273.5	-56.7	3.0	38	5839	[9]	-	-	-	-	-	-	-	-	-	-
		C01-13-1	C01-13-S9					823059		278.4	-56.9	3.0	39	7229	[9]	-	-	-	-	-	-	-	-	-	-
		C01-13-1	C01-13-S10c				S10c	823210	836699 99.0	99.6	-48.0	3.0	54	250296	[9]	-	-	-	-	-	-	-	-	-	-
		C01-13-1									Total SPL,	dB(A) [4]:	56										Total S	PL, dB(A) ^[4] :	[9]
C01-14	1	C01-14-1	C01-14-S4	823227	836604	9.8	S4	823089	836544 94.4	150.7	-51.6	3.0	46	38440	[9]	-	-	-			-		-	- 1	-
		C01-14-1	C01-14-S5						836442 98.5	178.4	-53.0	3.0	48	70207	[9]	-	-	-	-	-	-	-	-	-	-
		C01-14-1	C01-14-S6						836707 98.0	248.3	-55.9	3.0	45	32086	[9]	-	-	-	-		-	-	-	-	-
		C01-14-1	C01-14-S7				S7		836729 95.7	289.4	-57.2	3.0	41	14017	[9]	-	-	-	-	-	-	-	-	-	-
		C01-14-1	C01-14-S8						836786 91.4	270.5	-56.6	3.0	38	5969	[9]	-	-	-	-	-	-	-	-		-
		C01-14-1 C01-14-1	C01-14-S9 C01-14-S10c						836822 92.5 836699 99.0	275.2 96.5	-56.8 -47.7	3.0	39 54	7397 267021	[9] [9]	-	-	-	-	-	-	-	-	-	-
		C01-14-1	1001-14-0100				10100	020210	030033 33.0	30.0	Total SPL,			201021	[0]		_	_			_	-	Total S	PL, dB(A) ^[4] :	[9]
		_																							
C13-11	1	C13-11-1	C13-11-S4	823230	836635	9.8			836544 94.4	167.5	-52.5	3.0	45	31112	Y	15.2	4.2	163.3	4.6	6.8	163.7	167.5	3.0	20.0	25
		C13-11-1	C13-11-S5						836442 98.5	207.6	-54.3	3.0	47	51835	N Y	-	-	-	-	-	-	-	-	-	47
		C13-11-1 C13-11-1	C13-11-S6 C13-11-S7						836707 98.0 836729 95.7	239.6 280.0	-55.6 -56.9	3.0	45 42	34457 14981	Y	15.2 15.2	3.7	235.9 276.2	5.6 5.1	6.5	236.1 276.4	239.6 280.0	3.0	20.0	25 22
		C13-11-1	C13-11-S7						836786 91.4	252.8	-56.1	3.0	38	6832	Y	15.2	4.4	248.4	5.7	7.0	248.6	252.8	2.7	20.0	18
		C13-11-1	C13-11-S9					823059		253.2	-56.1	3.0	39	8735	Y	15.2	5.3	247.9	5.7	7.6	248.1	253.2	2.4	20.0	19
		C13-11-1	C13-11-S10c						836699 99.0	67.2	-44.5	3.0	57	550813	Y	15.2	10.2	57.0	5.2	11.5	57.8	67.2	2.2	20.0	37
		C13-11-1									Total SPL,	dB(A) [4]:	58										Total S	PL, dB(A) ^[4] :	48
C13-12	1	C13-12-1	C13-12-S4	823226	836638	9.8	IS/I	823080	836544 94.4	166.7	-52.4	3.0	45	31445		15.2	0.6	166.1	4.6	5.4	166.4	166.7	5.2	20.0	25
010-12		C13-12-1	C13-12-S5	020220	000000	3.0	S5		836442 98.5	209.5	-54.4	3.0	47	50888	Y	15.2	1.9	207.6	4.9	5.7	207.9	209.5	4.1	20.0	27
		C13-12-1	C13-12-S6				S6		836707 98.0	235.4	-55.4	3.0	46	35681	Y	15.2	0.5	234.9	5.6	5.4	235.1	235.4	5.1	20.0	26
		C13-12-1	C13-12-S7				S7		836729 95.7	275.7	-56.8	3.0	42	15444	Y	15.2	0.5	275.2	5.1	5.4	275.4	275.7	5.1	20.0	22
		C13-12-1	C13-12-S8						836786 91.4	248.2	-55.9	3.0	39	7090	Y	15.2	0.5	247.7	5.7	5.4	247.9	248.2	5.1	20.0	19
		C13-12-1	C13-12-S9						836822 92.5	248.5	-55.9	3.0	40	9068	Y	15.2	0.6	247.9	5.7	5.4	248.1	248.5	5.0	20.0	20
		C13-12-1 C13-12-1	C13-12-S10c				S10c	823210	836699 99.0	63.0	-44.0	3.0	58 59	625478	Y	15.2	1.2	61.8	5.2	5.5	62.6	63.0	5.1	20.0	38 39
		010-12-1									Total SPL,	uB(A) ***:	99										rotal S	PL, dB(A) ^[4] :	33
C13-13	1	C13-13-1	C13-13-S6	823238	836649	9.8			836707 98.0	244.2	-55.8	3.0	45	33179	Y	15.2	11.2	233.0	5.6	12.4	233.1	244.2	1.4	19.5	26
		C13-13-1	C13-13-S7				S7	822966		283.9	-57.1	3.0	42	14570	Y	15.2	11.3	272.6	5.1	12.5	272.8	283.9	1.4	19.5	22
		C13-13-1	C13-13-S8						836786 91.4	251.8	-56.0	3.0	38	6885	Y	15.2	12.4	239.4	5.7	13.5	239.6	251.8	1.3	19.2	19
		C13-13-1 C13-13-1	C13-13-S9 C13-13-S10c						836822 92.5 836699 99.0	249.1 57.5	-55.9 -43.2	3.0	40 59	9027 751114	Y	15.2 15.2	13.9 4.6	235.2 52.9	5.7 5.2	14.9 7.1	235.4 53.9	249.1 57.5	1.2 3.4	18.8 20.0	21 39
\Box		C13-13-1	1010-10-0100				10100	023210	0.00000 88.0	51.0	Total SPL,			131114		13.2	1 4.0	32.9	3.2	1.1	33.8	51.5		PL, dB(A) [4]:	39
		_										GB(A)												L, UD(A) **:	
C13-14	1	C13-14-1	C13-14-S4	823231	836650	9.8	S4	823089	836544 94.4	177.0	-53.0	3.0	44	27882	Y	15.2	5.1	171.9	4.6	7.4	172.2	177.0	2.7	20.0	24
		C13-14-1	C13-14-S5						836442 98.5	221.7	-54.9	3.0	47	45449	Y	15.2	13.8	207.9	4.9	14.8	208.2	221.7	1.3	19.0	28
		C13-14-1 C13-14-1	C13-14-S6				S6	823001		236.9	-55.5	3.0	45	35249	Y	15.2	3.7	233.2	5.6	6.5	233.4	236.9	3.0	20.0	25
		C13-14-1 C13-14-1	C13-14-S7				S7 S8	822966 823027	836729 95.7 836786 91.4	276.7 245.5	-56.8 -55.8	3.0	42 39	15339 7248	Y	15.2 15.2	3.8 4.2	272.9 241.3	5.1 5.7	6.6	273.1 241.5	276.7 245.5	3.0 2.8	20.0	22 19
		C13-14-1	C13-14-S9					823059		243.6	-55.7	3.0	40	9443	Y	15.2	4.7	238.9	5.7	7.2	239.0	243.6	2.6	20.0	20
		C13-14-1	C13-14-S10c						836699 99.0	53.9	-42.6	3.0	59	856002	Y	15.2	10.9	43.0	5.2	12.2	44.1	53.9	2.4	20.0	39
		C13-14-1						•			Total SPL,	dB(A) ^[4] :	60										Total S	PL, dB(A) [4]:	40
E13-12	- 1	E13-12-1	E13-12-S4	823200	836753	10.8	IQ/	823000	836544 94.4	282.6	-57.0	3.0	40	10939	l N	Ι.			Ι -	T -					40
L10-12	'	E13-12-1	E13-12-S6	323200	000/32	10.0			836707 98.0	282.8	-57.0	3.0	44	24723	N N	+ -	-	-	-	-	-		-	-	44
		E13-12-1	E13-12-S8				S8		836786 91.4	255.8	-56.2	3.0	38	6676	N		-	-	-	 	-	-			38
		E13-12-1	E13-12-S9					823059	836822 92.5	232.4	-55.3	3.0	40	10373	N	-	-	-	-	-	-	-	-		40
		E13-12-1	E13-12-S10a				310	823217	836734 99.0	65.8	-44.4	3.0	58	573983	Y	10.2	9.4	56.4	5.2	9.4	56.6	65.8	0.2	12.4	45
		E13-12-1									Total SPL,	dB(A) [4]:	58										Total S	PL, dB(A) [4]:	49

					Noise S	ource (NS	5)		Correction		Unmitigated		Consider for	Barrier	Horizontal	Horizontal	NS level (1m	Slant	Slant	Distance from	Path	Path	Mitigated			
In.	Floor			l	١.,	Height	1			SWL,	from NS to	Dietenes	Facade	Noise Level,	Intensity	Path	Height,	Distance from	Distance from	above	Distance from	Distance from	AP to NS, m	Difference	Difference	Noise Level,
10	FIOOI			_ ×	У	, mPD		X	У	dB(A)	AP, m ^[1]	Distance	raçaue	dB(A) [2][3][4]		Difference?	mPD	AP to Barrier,	NS to Barrier,	ground	AP to Barrier,	Barrier to NS,	[C]	, m	Correction,	dB(A) [7]
E13-13	1	E13-13-1	E13-13-S4	823286	836762	10.8	S4	823089	836544	94.4	293.4	-57.3	3.0	40	10147	N	-	-	-	-	-	-	-	-	-	40
		E13-13-1	E13-13-S6	1			S6	823001	836707	98.0	289.6	-57.2	3.0	44	23585	N	-	-	-	-	-	-	-	-	-	44
		E13-13-1	E13-13-S8	1			S8	823027	836786	91.4	259.7	-56.3	3.0	38	6476	N	-	-	-	-	-	-	-	-	-	38
		E13-13-1	E13-13-S9	1			S9	823059	836822	92.5	234.5	-55.4	3.0	40	10190	N	-	-	-	-	-	-	-	-	-	40
		E13-13-1	E13-13-S10a				S10a	823217	836734	99.0	73.9	-45.4	3.0	57	455205	Y	10.2	10.5	63.4	5.2	10.5	63.6	73.9	0.2	12.0	45
		E13-13-1								•		Total SPL	, dB(A) [4]	57										Total S	PL, dB(A) [4]:	49

		Assessment P	Point (AP)					Noise Sc	ource (NS)	Distance	Correctio	ns. dB(A)	Unmitigated		Consider for	Barrier	Horizontal	Horizontal	NS level (1m	Slant	Slant	Distance from	Path	Path	Mitigated
ID	Floor			×	у	Height		х	y SWL,	from NS to	Distance	Façade	Noise Level,	Intensity	Path	Height,	Distance from	Distance from	above		Distance from	AP to NS, m	Difference	Difference	
						, mPD)		- (aB(A)	AP, m [1]			dB(A) [2][3][4]		Difference?	mPD	AP to Barrier,	NS to Barrier,	ground	AP to Barrier,		[C]	, m	Correction,	dB(A) [7]
E19-12	1	E19-12-1	E19-12-S4	823261	836708	10.8		823089		237.8	-55.5	3.0	42	15451	Y	13.0	24.4	213.4	4.6	24.5	213.5	237.8	0.3	12.8	29
		E19-12-1 E19-12-1	E19-12-S6 E19-12-S7	1					836707 98.0 836729 95.7	259.9 296.0	-56.3 -57.4	3.0	45 41	29275 13403	Y	13.0	13.9	246.0 282.3	5.6 5.1	14.1	246.1 282.4	259.9 296.0	0.3	13.1	32 28
		E19-12-1	E19-12-S7	1			S8		836786 91.4	246.8	-57.4	3.0	39	7170	Y	13.0	13.6	233.2	5.7	13.8	233.3	246.8	0.3	13.1	25
		E19-12-1	E19-12-S9	1					836822 92.5	232.1	-55.3	3.0	40	10399	Y	13.0	14.2	217.9	5.7	14.4	218.0	232.1	0.3	13.1	27
		E19-12-1	E19-12-S10b	J					836721 99.0	44.5	-41.0	3.0	61	1256741	, ,	13.0	13.6	30.9	5.2	13.8	31.8	44.5	1.1	18.6	42
		E19-12-1	L19-12-310D				3100	023213	030721 99.0	44.5	Total SPL,			1230741	-	13.0	13.0	30.5	3.2	13.0	31.0	44.5		PL, dB(A) ^[4] :	
		L10-12-1									iotai SPL,	aB(A) · ·:	01										i otai S	PL, 0B(A) * *:	
E19-13	1	E19-13-1	E19-13-S4	823266	836718	10.8	S4	823089	836544 94.4	248.2	-55.9	3.0	42	14182	Y	13.0	25.7	222.5	4.6	25.8	222.6	248.2	0.3	12.6	29
		E19-13-1	E19-13-S6	1			S6	823001	836707 98.0	264.7	-56.5	3.0	45	28233	N	-	9.3	-	-	-	-	-	-	-	45
		E19-13-1	E19-13-S7	1			S7	822966	836729 95.7	300.0	-57.5	3.0	41	13050	N	-	8.9	-	-	-	-	-	-	-	41
		E19-13-1	E19-13-S8	1			S8	823027	836786 91.4	248.1	-55.9	3.0	39	7097	N	-	8.2	-	-	-	-	-	-	-	39
		E19-13-1	E19-13-S9	1			S9	823059	836822 92.5	231.2	-55.3	3.0	40	10476	N	-	8.1	-	-	-	-	-	-	-	40
		E19-13-1	E19-13-S10b	1			S10b	823219	836721 99.0	47.2	-41.5	3.0	60	1115475	Y	13.0	8.2	39.0	5.2	8.5	39.8	47.2	1.1	18.3	42
		E19-13-1									Total SPL,	dB(A) [4]:	61										Total S	PL, dB(A) [4]:	49
		_																							
E22-11	1	E22-11-1	E22-11-S6	823257	836693	10.8	_		836707 98.0	256.4	-56.2	3.0	45	30081	Y	13.0	14.3	242.1	5.6	14.5	242.2	256.4	0.3	13.0	32
		E22-11-1	E22-11-S7						836729 95.7	293.6	-57.4	3.0	41	13623	Y	13.0	14.3	279.3	5.1	14.5	279.4	293.6	0.3	13.0	28
		E22-11-1	E22-11-S8	1					836786 91.4	248.5	-55.9	3.0	38	7071	Y	13.0	12.5	236.0	5.7	12.7	236.1	248.5	0.3	13.3	25
		E22-11-1	E22-11-S9				S9		836822 92.5	236.8	-55.5	3.0	40	9988	Y	13.0	12.5	224.3	5.7	12.7	224.4	236.8	0.3	13.4	27
		E22-11-1	E22-11-S10				S10	823216	836713 99.0	46.0	-41.3	3.0	61	1188440	Y	13.0	12.5	33.5	5.2	12.7	34.4	46.0	1.1	18.4	42
		E22-11-1									Total SPL,	dB(A) [4]:	61										Total S	PL, dB(A) ^[4] :	43
E22-14	1	E22-14-1	E22-14-S4	823260	836681	10.8	S4	823080	836544 94.4	218.8	-54.8	3.0	43	18250	Y	13.0	7.0	211.8	4.6	7.3	211.9	218.8	0.5	15.3	27
L22=14		E22-14-1	E22-14-S6	023200	030001	10.0	S6		836707 98.0	259.6	-56.3	3.0	45	29347	Y	13.0	13.5	246.1	5.6	13.7	246.2	259.6	0.3	13.1	32
		E22-14-1	E22-14-S7	1					836729 95.7	297.5	-57.5	3.0	41	13269	Y Y	13.0	13.5	284.0	5.1	13.7	284.1	297.5	0.3	13.1	28
		E22-14-1	E22-14-S8	1			S8		836786 91.4	255.1	-56.1	3.0	38	6709	Y	13.0	17.6	237.5	5.7	17.7	237.6	255.1	0.2	12.6	26
		E22-14-1	E22-14-S9	†			_		836822 92.5	245.1	-55.8	3.0	40	9323	Y	13.0	17.6	227.5	5.7	17.7	227.6	245.1	0.3	12.6	27
		E22-14-1	E22-14-S10	†					836713 99.0	53.9	-42.6	3.0	59	865127	Y	13.0	17.6	36.3	5.2	17.7	37.1	53.9	1.0	17.9	41
		E22-14-1									Total SPL,				-		-		-	1				PL, dB(A) [4]:	
																								-,,	
E22-15	1	E22-15-1	E22-15-S4	823257	836684	10.8			836544 94.4	218.2	-54.8	3.0	43	18337	Y	13.0	7.9	210.3	4.6	8.2	210.5	218.2	0.5	15.0	28
		E22-15-1	E22-15-S6	1					836707 98.0	256.6	-56.2	3.0	45	30045	Y	13.0	13.3	243.3	5.6	13.5	243.4	256.6	0.3	13.2	32
		E22-15-1	E22-15-S7				S7		836729 95.7	294.3	-57.4	3.0	41	13557	Y	13.0	13.3	281.0	5.1	13.5	281.1	294.3	0.3	13.2	28
		E22-15-1	E22-15-S8	1			S8		836786 91.4	251.5	-56.0	3.0	38	6904	Y	13.0	13.3	238.2	5.7	13.5	238.3	251.5	0.3	13.2	25
		E22-15-1	E22-15-S9						836822 92.5	241.3	-55.7	3.0	40	9618	Y	13.0	13.3	228.0	5.7	13.5	228.1	241.3	0.3	13.2	27
		E22-15-1	E22-15-S10				S10	823216	836713 99.0	50.1	-42.0	3.0	60	990218	Y	13.0	13.3	36.8	5.2	13.5	37.6	50.1	1.0	18.0	42
		E22-15-1									Total SPL,	dB(A) [4]:	60										Total S	PL, dB(A) ^[4] :	43
E41-13	1	E41-13-1	E41-13-S4	922220	926540	10.0	64	922090	836544 94.4	239.5	-55.6	3.0	42	15223	N	Τ.		T -						-	42
L41-13		E41-13-1	E41-13-S5	023323	030343	10.0			836442 98.5	205.7	-54.3	3.0	47	52809	N		 		 		-	-	<u> </u>	-	47
		E41-13-1	141-10-00			I	100	020100	000442 00.0	200.1	Total SPL,			02000		1 -	_	_		_		_		PL. dB(A) ^[4] :	
		= '									i otai SPL,	ub(A) **:											TOTAL S	L, UD(A) **:	
E41-14	1	E41-14-1	E41-14-S4	823327	836551	10.8	S4	823089	836544 94.4	238.1	-55.5	3.0	42	15403	N	-	-	-	-	-	-	-	-	-	42
		E41-14-1	E41-14-S5	1			S5	823153	836442 98.5	205.8	-54.3	3.0	47	52763	N	-	-	-	-	-	-	-	-	-	47
		E41-14-1	'						'		Total SPL,	dB(A) [4]:	48										Total S	PL, dB(A) ^[4] :	48
E42-14	1	E42-14-1	E42-14-S1	823425	836542	10.8			836709 91.4	243.6	-55.7	3.0	39	7359	Y	12.6	18.2	225.4	4.2	18.3	225.6	243.6	0.39	14.3	24
		E42-14-1	E42-14-S2	1					836655 94.9	253.6	-56.1	3.0	42	15199	Y	12.6	11.6	242.0	4.7	11.7	242.1	253.6	0.17	11.2	31
		E42-14-1	E42-14-S3-1	1					836630 96.8	200.9	-54.1	3.0	46	37363	Y	12.6	11.5	189.4	4.9	11.6	189.6	200.9	0.73	16.7	29
		E42-14-1	E42-14-S3-2	1					836649 99.0	229.3	-55.2	3.0	47	47256	Y	12.6	11.9	217.4	4.9	12.0	217.5	229.3	0.74	16.8	30
		E42-14-1	E42-14-S11b				211	823447	836539 99.0	22.5	-35.1	3.0	67	4896798	Y	12.6	9.4	13.1	7.4	9.6	14.1	22.5	1.07	18.3	49
		E42-14-1									Total SPL,	dB(A) [4]:	67										Total S	PL, dB(A) [4]:	49

P. 4 of 8
Q/ProjectsiFDBNPWWREA00/05 Assessmentsi02 Noisel01 Fixed Plant/R8923_v5.0/R8923_v5.0_App 4.1 to 4.3 - 20231228.xisx

Confidential

		Assessment I	Point (AP)				Noise Sc	ource (NS)	Distance	Correction	ons. dB(A)	Unmitigated		Consider for	Barrier	Horizontal	Horizontal	NS level (1m	Slant	Slant	Distance from	Path	Path	Mitigated
ID	Floor		x	y	Height	t _{ID}	x	, sw	, from NS to	Distance		Noise Level,	Intensity	Path	Height,	Distance from	Distance from	above	Distance from	Distance from	AP to NS, m	Difference		Noise Level,
E42-15	1	E42-15-1	E42-15-S1 82342	2 836539	, mPD 10.8		823601	836709 91.		-55.9	3.0	dB(A) [2][3][4] 39	7142	Difference?	mPD 12.6	AP to Barrier, 21.2	NS to Barrier, 226.1	ground 4.2	AP to Barrier, 21.3	Barrier to NS, 226.2	[C] 247.3	, m 0.19	Correction, 11.7	dB(A) ^[7] 27
		E42-15-1	E42-15-S2		1		823652			-56.2	3.0	42	14799	Y	12.6	13.4	243.6	4.7	13.5	244.1	257.0	0.65	16.2	25
		E42-15-1	E42-15-S3-1					836630 96.		-54.2	3.0	46	36130	Y	12.6	13.4	190.9	4.9	13.5	191.2	204.3	0.41	14.4	31
		E42-15-1	E42-15-S3-2					836649 99.		-55.3	3.0	47	45871	Y	12.6	13.8	218.9	4.9	13.9	219.1	232.7	0.28	13.0	34
		E42-15-1 E42-15-1	E42-15-S11b			L.	823447	836539 99.	0 24.8	-35.9	3.0	66 66	4042547	Y	12.6	10.0	14.8	7.4	10.1	16.2	24.8	1.53	19.8	46 47
		E42-15-1								Total SPL	., dB(A) ^[4] :	66										Total S	PL, dB(A) ^[4] :	47
E43-14	1	E43-14-1	E43-14-S1 82342	7 836548	10.8			836709 91.		-55.5	3.0	39	7762	Y	12.6	17.7	219.5	4.2	17.8	219.7	237.2	0.80	17.1	22
		E43-14-1	E43-14-S2				823652	836655 94.		-55.9	3.0	42	15845	Y	12.6	11.3	237.0	4.7	11.4	237.2	248.3	0.30	13.3	29
		E43-14-1	E43-14-S3-1				823605	836630 96.		-53.8	3.0	46	39371	Y	12.6	11.2	184.5	4.9	11.3	184.7	195.7	0.32	13.5	32
		E43-14-1 E43-14-1	E43-14-S3-2 E43-14-S11					836649 99. 836546 99.		-55.0 -34.7	3.0	47 67	49536 5292111	Y	12.6 12.6	11.6 8.1	212.4 13.6	4.9 7.4	11.7 8.3	212.5 15.1	224.0 21.7	0.28 1.73	13.0 20.0	34 47
		E43-14-1	L43-14-311			311	023445	030340 33.	0 21.7		, dB(A) [4]:	67	3232111	'	12.0	0.1	15.0	211.1	204.49	14.3			PL, dB(A) ^[4] :	48
E43-15	1	E43-15-1		836546	10.8			836709 91.		-55.6	3.0	39	7528	Y	12.6	20.6	220.3	4.2	20.7	220.4	240.9	0.14	10.5	28
		E43-15-1 E43-15-1	E43-15-S2 E43-15-S3-1				823652 823605			-56.0 -54.0	3.0	42 46	15423 38053	Y	12.6 12.6	13.1 13.0	238.6 186.1	4.7 4.9	13.2 13.1	238.8 186.3	251.7 199.1	0.28	13.0 13.7	29 32
		E43-15-1	E43-15-S3-1					836649 99.		-54.0	3.0	47	48062	Y	12.6	13.5	213.9	4.9	13.6	214.0	227.4	0.34	12.6	34
		E43-15-1	E43-15-S11					836546 99.		-35.6	3.0	66	4353133	Y	12.6	9.9	14.0	7.4	10.1	15.1	23.9	1.17	18.7	48
		E43-15-1									, dB(A) [4]:								·			Total S	PL, dB(A) [4]:	
		10101		=	1 40 -	lo. I		000700					7007											
A01-21	2	A01-21-2 A01-21-2	A01-21-S1 82335 A01-21-S3-1	836745	13.3		823601 823605	836709 91. 836630 96.		-55.9 -56.8	3.0	38 43	7037 19939	N N	-	155.7	-		-	-	-	-	-	38 43
		A01-21-2 A01-21-2	A01-21-S3-1				823627			-57.2	3.0	45	29766	N N	-	155.7	- :	- :	- : -		- : -	-	- :	45
		A01-21-2	A01-21-S11a					836563 99.		-54.5	3.0	47	55446	Y	12.6	185.7	26.0	7.4	185.7	26.5	211.7	0.5	15.4	32
		A01-21-2								Total SPL	, dB(A) [4]:	50					1				1	Total S	PL, dB(A) [4]:	
		1				1 1			-1															
A01-22	2	A01-22-2 A01-22-2	A01-22-S9 82334 A01-22-S10a	1 836748	13.3			836822 92. 836734 99.		-57.3 -49.9	3.0	38 52	6582 159663	N Y	10.2	74.4	50.4	5.2	74.4	50.6	124.7	0.3	13.4	38 39
		A01-22-2	A01-22-310a			Siua	023217	030734 99.	0 124.7		., dB(A) ^[4] :		159005		10.2	74.4	50.4	5.2	74.4	50.6	124.7		PL, dB(A) ^[4] :	
										TOTAL SEL	., ub(A) .											TOTAL S	FL, UD(A) .	
A02-21	2	A02-21-2	A02-21-S1 82335	1 836736	13.3			836709 91.		-56.0	3.0	38	6865	N	-	-	-	-	-	-	-	-	-	38
		A02-21-2	A02-21-S3-1				823605			-56.8	3.0	43	19880	N	-	156.0	-	-	-	-	-	-	-	43 45
		A02-21-2 A02-21-2	A02-21-S3-2 A02-21-S11a					836649 99. 836563 99.		-57.3 -54.3	3.0	45 48	29507 58206	N Y	12.6	157.1 181.3	25.3	7.4	181.3	25.8	206.6	0.5	15.5	32
		A02-21-2	A02-21-311a			опа	023404	030303 99.	0 200.0		, dB(A) [4]:		36206	1	12.0	101.3	25.3	7.4	101.3	23.0	200.0		PL, dB(A) [4]:	
											., ab(/, .												, u_(/,) .	
A02-22	2	A02-22-2	A02-22-S9 82333	836739	13.3			836822 92.		-57.2	3.0	38	6661	N	-	-	-	-	-	-	-	-	-	38
		A02-22-2 A02-22-2	A02-22-S10a			S10a	823217	836734 99.	0 119.9	-49.6	3.0 , dB(A) ^[4] :	52 53	172970	Y	10.2	71.5	48.3	5.2	71.6	48.6	119.9	0.3	13.6	39 42
		A02-22-2								Total SPL	., dB(A) · ·:	- 55										i otai S	PL, dB(A) ^[4] :	42
A06-21	2	A06-21-2	A06-21-S1 82333	4 836702	13.3			836709 91.		-56.6	3.0	38	6091	N	-	-	-	-	-	-	-	-	-	38
		A06-21-2	A06-21-S3-1				823605			-57.0	3.0	43	19184	N	-	-	-	-	-	-	-	-	-	43
		A06-21-2 A06-21-2	A06-21-S3-2 A06-21-S11a					836649 99. 836563 99.		-57.5	3.0	44	27921 68959	N Y	12.6	166.9	22.9	7.4	166.9	23.5	189.8	-	- 45.0	44 33
		A06-21-2	A00-21-311a			опа	023404	030303 99.	0 109.0	-53.6	3.0 , dB(A) ^[4] :	48 51	00939	-	12.0	100.9	22.9	7.4	100.9	23.5	109.0	0.6	15.8 PL, dB(A) ^[4] :	47
										TOTAL OF E	, ub(A) .											Total o	, ub(A) .	
A06-22	2	A06-22-2		836705	13.3			836822 92.		-57.1	3.0	38	6839	N	-	-	-	-	-	-	-	-	-	38
		A06-22-2 A06-22-2	A06-22-S10b			S10b	823219	836721 99.	0 102.8	-48.2	3.0 , dB(A) ^[4] :	54 54	235153	Y	13.0	66.3	36.5	5.2	66.3	37.3	102.8	0.8	17.2 PL, dB(A) ^[4] :	36 43
		AUU-22-2								iotai SPL	., ab(A) 19:	J**										ı otal S	rL, aB(A) 171:	40
C01-21	2	C01-21-2	C01-21-S6 82323	836616	14.3			836707 98.		-56.0	3.0	45	31234	N	-	-	-	-	-	-	-	-	-	45
		C01-21-2	C01-21-S7					836729 95.		-57.3	3.0	41	13726	N	-	-	-	-	-	-	-	-	-	41
		C01-21-2	C01-21-S8				823027			-56.6	3.0	38	6022	N	-	-	-	-	-	-	-	-	-	38
		C01-21-2 C01-21-2	C01-21-S9 C01-21-S11b				823059 823447			-56.7 -55.0	3.0	39 47	7603 49200	N N	+ -	-	-	-	-	-	-	-	-	39 47
		C01-21-2	JUI - 2 I - 3 I IU			Louin	J2J441	555555 39.	224.1		, dB(A) ^[4] :	50	70200	IN	<u> </u>		-					Total S	PL, dB(A) ^[4] :	
		_																				.oui o	,	
C13-21	2	C13-21-2	C13-21-S4 82323	1 836634	14.3			836544 94.		-52.5	3.0	45	30800	Y	15.2	5.7	162.7	4.6	5.8	163.0	168.4	0.4	14.5	30
		C13-21-2 C13-21-2	C13-21-S5 C13-21-S6				823153 823001	836442 98. 836707 98.		-54.3 -55.6	3.0	47 45	51839 34037	N Y	15.2	5.2	235.9	5.6	5.3	236.0	241.1	0.3	12.9	47 32
		C13-21-2 C13-21-2	C13-21-S6				823001	836707 98. 836729 95.		-55.6	3.0	45	14825	Y	15.2	5.2	235.9	5.6	5.3	236.0	241.1	0.3	12.9	29
		C13-21-2	C13-21-S8				823027	836786 91.		-56.1	3.0	38	6755	Y	15.2	6.1	248.2	5.7	6.2	248.3	254.3	0.3	12.6	26
		C13-21-2	C13-21-S9				823059			-56.1	3.0	39	8643	Y	15.2	7.2	247.4	5.7	7.3	247.6	254.6	0.2	12.4	27
		C13-21-2	C13-21-S11b			S11b	823447	836539 99.		-55.5	3.0	46	44613	Υ	12.6	222.0	14.0	7.4	222.0	14.9	236.0	0.9	17.8	29
		C13-21-2								Total SPL	., dB(A) ^[4] :	53										Total S	PL, dB(A) [4]:	48
C13-22	2	C13-22-2	C13-22-S4 82322	836637	143	S4	823080	836544 04	4 168.1	-52.5	3.0	45	30920	Y	15.2	3.2	164.9	4.6	3.3	165.2	168.1	0.5	14.9	30
10.0.22	<u>~</u>	13.0222	1 0.0 22.04 02022	1 000007	1 44.5	(·	-20003		. 100.1	J 52.5	3.0		1 00020	· · ·	10.2	J.2	1 .04.0		3.0	.50.2	1.30.1		1 .7.5	30

		Assessment F	Point (AP)				Noise 9	Source (NS)	Т	Distance	Correction	ns dR/A\	Unmitigated		Consider for	Barrier	Horizontal	Horizontal	NS level (1m	Slant	Slant	Distance from	Path	Path	Mitigated
ID	Floor	Assessment P	J (Al)	x		eight	ID x	T , S	SWL,	from NS to	Distance	Façade	Noise Level,	Intensity	Path	Height,	Distance from	Distance from	above	Distance from	Distance from	AP to NS, m		Difference	Noise Level,
ID	FIOOI	040.00.0	040.00.05	*	y , m	ทยบ		, d	IB(A)	AP, m [1]			dB(A) [2][3][4]	50000	Difference?	mPD	AP to Barrier,	NS to Barrier,	ground	AP to Barrier,		[C]	, m	Correction,	dB(A) ^[7]
		C13-22-2 C13-22-2	C13-22-S5 C13-22-S6					3 836442 1 836707	98.5	209.4	-54.4 -55.5	3.0	47 45	50938 34907	Y	15.2 15.2	6.9 2.8	202.5 235.2	4.9 5.6	7.0	202.8 235.4	209.4 238.0	0.3	13.5	34 32
		C13-22-2	C13-22-S7					6 836729		278.4	-56.9	3.0	42	15156	Y	15.2	2.8	275.6	5.1	2.9	275.7	278.4	0.3	13.6	28
		C13-22-2	C13-22-S8					7 836786		250.7	-56.0	3.0	38	6947	Y	15.2	3.3	247.4	5.7	3.4	247.6	250.7	0.3	13.3	25
		C13-22-2	C13-22-S9			- 1	82305	9 836822	92.5	250.9	-56.0	3.0	39	8897	Y	15.2	3.9	247.0	5.7	4.0	247.2	250.9	0.3	13.1	26
		C13-22-2		•	•		•				Total SPL,	dB(A) ^[4] :	52			•				•			Total SF	PL, dB(A) [4]:	38
C13-23	2	C13-23-2	C13-23-S6 82	23238 836	6650 14	4.3	S6 82300	1 836707	98.0	243.4	-55.7	3.0	45	33394	Y	15.2	10.4	233.0	5.6	10.4	233.2	243.4	0.2	12.4	33
		C13-23-2	C13-23-S7			- 1	S7 82296	6 836729	95.7	283.1	-57.0	3.0	42	14652	Y	15.2	10.5	272.6	5.1	10.5	272.8	283.1	0.2	12.2	29
		C13-23-2	C13-23-S8					7 836786		251.1	-56.0	3.0	38	6928	Y	15.2	11.5	239.6	5.7	11.5	239.8	251.1	0.2	12.2	26
		C13-23-2	C13-23-S9					9 836822		248.4	-55.9	3.0	40	9081	Y	15.2	8.1	240.3	5.7	8.1	240.4	248.4	0.2	12.4	27
		C13-23-2 C13-23-2	C13-23-S10c				S10c 82321	0 836699	99.0	56.9	-43.1 Total SPL,	3.0	59 59	767742	Y	15.2	4.6	52.3	5.2	4.7	53.2	56.9	1.0	18.2 PL, dB(A) ^[4] :	41 42
		_																							
C13-24	2	C13-24-2	C13-24-S4 82	23231 836	6649 14			9 836544		176.3	-52.9	3.0	44	28088	Y	15.2	4.8	171.5 208.0	4.6	4.9	171.9 208.2	176.3	0.4	14.5	30
		C13-24-2 C13-24-2	C13-24-S5 C13-24-S6					3 836442 1 836707		221.0 236.8	-54.9 -55.5	3.0	47 45	45763 35281	Y	15.2 15.2	13.0 3.5	233.3	4.9 5.6	13.0	208.2	221.0 236.8	0.3	13.1 13.4	34 32
		C13-24-2	C13-24-S7					6 836729		276.6	-56.8	3.0	42	15347	Y	15.2	3.6	273.0	5.1	3.7	273.2	276.6	0.3	13.4	29
		C13-24-2	C13-24-S8					7 836786		245.6	-55.8	3.0	39	7239	Y	15.2	3.9	241.7	5.7	4.0	241.9	245.6	0.3	13.1	25
		C13-24-2	C13-24-S9					9 836822		243.9	-55.7	3.0	40	9420	Y	15.2	4.5	239.4	5.7	4.6	239.5	243.9	0.3	13.0	27
		C13-24-2	C13-24-S10c				S10c 82321	0 836699	99.0	54.4	-42.7	3.0	59	839212	Y	15.2	7.1	47.3	5.2	7.2	48.4	54.4	1.1	18.4	41
		C13-24-2									Total SPL,	, dB(A) ^[4] :	60										Total SF	PL, dB(A) [4]:	43
A01-31	3	A01-31-3	A01-31-S1 82	23346 836	6749 16			1 836709		258.9	-56.3	3.0	38	6517	N	-	-	-	-	-	-	-	-	-	38
		A01-31-3	A01-31-S3-1					5 836630		285.3	-57.1	3.0	43	18535	N	-	-	-	-	-	-	-	-	-	43
		A01-31-3 A01-31-3	A01-31-S3-2				S3-2 82362	7 836649	99.0	299.1	-57.5 Total SPL,	3.0 dB(A) ^[4] :	44 47	27778	N	-	-	-	-	-	-	-	- Total SF	- PL, dB(A) ^[4] :	44 47
104.00	3	A01-32-3	A01-32-S9 82	00044	10740	00 1	20 00005	9 836822	00.5	291.7	-57.3	3.0	38	6581		1 -		1			1				38
A01-32	3	A01-32-3 A01-32-3	A01-32-S9 82 A01-32-S10a	23341 836	16/48			7 836734		124.8	-57.3 -49.9	3.0	52	159501	N Y	10.2	83.4	41.4	5.2	83.7	41.7	124.8	0.6	15.7	36
		A01-32-3	7101 02 0104				02021	, 000, 01,	00.0	121.0	Total SPL,			100001		10.2	00.1		0.2	00.7		121.0		PL, dB(A) [4]:	40
A01-33	3	A01-33-3	A01-33-S9 82	23339 836	6744 16			9 836822		290.9	-57.3	3.0	38	6619	N	-	-	-	-	-	-	-	-		38
		A01-33-3 A01-33-3	A01-33-S10a				S10a 82321	7 836734	99.0	122.5	-49.8 Total SPL,	3.0	52 52	165576	Y	10.2	80.8	41.7	5.2	81.1	42.0	122.5	0.6	15.7 PL, dB(A) ^[4] :	36 40
											TOTAL SEL,	ub(A) .											Total Sr	L, UD(A) .	
A02-32	3	A02-32-3	A02-32-S9 82	23337 836	6739 16			9 836822		290.0	-57.2	3.0	38	6661	N	-	-	-	-	-	-	-	-	-	38
		A02-32-3 A02-32-3	A02-32-S10a			:	S10a 82321	7 836734	99.0	119.9	-49.6	3.0	52	172808	Y	10.2	78.9	41.0	5.2	79.2	41.3	119.9	0.6	15.8	37
		AU2-32-3									Total SPL,	, dB(A) ^(►) :	53										Total SF	PL, dB(A) [4]:	40
A02-33	3	A02-33-3		23335 836	6736 16			9 836822		289.3	-57.2	3.0	38	6692	N	-	-	-	-	-	-	-	-	-	38
		A02-33-3 A02-33-3	A02-33-S10a			!	S10a 82321	7 836734	99.0	117.9	-49.4	3.0	53	178870	Y	10.2	77.6	40.3	5.2	77.9	40.6	117.9	0.6	15.9	37
		AU2-33-3									Total SPL,	, dB(A) [⊷] :	53										Total SF	PL, dB(A) [4]:	41
A06-32	3	A06-32-3	A06-32-S9 82	23320 836	6705 16			9 836822		286.2	-57.1	3.0	38	6839	N	-	-	-	-	-	-		-	-	38
		A06-32-3 A06-32-3	A06-32-S10b				S10b 82321	9 836721	99.0	102.8	-48.2 Total SPL,	3.0 dB(Δ) ^[4] -	54 54	235005	Y	10.2	68.0	34.8	5.2	68.3	35.2	102.8	0.7	16.4 PL, dB(A) ^[4] :	37 44
																								, ()	
A06-33	3	A06-33-3	A06-33-S9 82 A06-33-S10b	23318 836	6701 16			9 836822 9 836721		286.1 101.6	-57.1 -48.1	3.0	38 54	6844 240565	N Y	13.0	65.0	36.6	5.2	65.1	37.4	101.6	0.9	17.7	38 36
			AUD-33-3 IUD				3 100 02321	030121	±3.U	101.0	Total SPL,			240000	1 1	13.0	03.0	30.0	5.2	05.1	31.4	101.0		PL, dB(A) [4]:	43
																								_, \	
E22-21	2	E22-21-2	E22-21-S6 82	23257 836	6693 1			1 836707		256.4	-56.2	3.0	45	30081	N	13.0	14.3	-	-	-	-	-	-	-	45
		E22-21-2 E22-21-2	E22-21-S7 E22-21-S8					6 836729 7 836786		293.6 248.5	-57.4 -55.9	3.0	41 38	13623 7071	N N	13.0	14.3 12.5	-	-	-	-	-	-		41 38
		E22-21-2 E22-21-2	E22-21-S9					9 836822		236.8	-55.5	3.0	40	9988	N N	13.0	12.5	-	-	-	-		-		40
		E22-21-2	E22-21-S10					6 836713		46.0	-41.3	3.0	61	1175524	Y	13.0	12.5	33.5	5.2	12.7	34.4	46.0	1.1	18.5	42
. '		E22-21-2					'				Total SPL,	, dB(A) ^[4] :	61			•							Total SF	PL, dB(A) [4]:	49
E22-24	2	E22-24-2	E22-24-S4 82	23260 836	6681 1	5.3	S4 82308	9 836544	94.4	218.8	-54.8	3.0	43	18250	N	13.0	7.0				-		- 1	-	43
		E22-24-2	E22-24-S6		. .	1	82300	1 836707	98.0	259.6	-56.3	3.0	45	29347	N	13.0	13.5	-	-	-	-	-	-	-	45
		E22-24-2	E22-24-S7					6 836729		297.5	-57.5	3.0	41	13269	N	13.0	13.5	-	-	-	-	-	-	-	41
		E22-24-2	E22-24-S8						91.4	255.1	-56.1	3.0	38	6709	N	13.0	17.6	-	-	-	-		-	-	38
		E22-24-2 E22-24-2	E22-24-S9 E22-24-S10					9 836822 6 836713		245.1 53.9	-55.8 -42.6	3.0	40 59	9323 855724	N Y	13.0	17.6 17.6	36.3	5.2	17.7	37.1	53.9	1.0	17.9	40 41
1 1		E22-24-2 E22-24-2	L22-24-310	I	I	E	023211	0 030/13	5 3 .U	33.9	Total SPL,			000124	1	13.0	17.0	30.3	3.2	11.1	31.1	33.9		PL, dB(A) [4]:	50
											. Juli OF L,	, ub(A) .											i otal Gr	_, ub(A) .	

Assessment Point (AP) Noise Source (NS) Distance Corr From NS to															Consider for	Barrier	Horizontal	Horizontal	NS level (1m	Slant	Slant	Distance from	Path	Path	Mitigated
ID	Floor		x		Н	leight ID			SWL,	from NS to	Distance	Facada	Noise Level,	Intensity	Path	Height,	Distance from	Distance from	above	Distance from		AP to NS, m	Difference	Difference	Noise Level,
						mPD	x		dB(A)	AP, m ^[1]		-	dB(A)		Difference?	mPD	AP to Barrier,	NS to Barrier,	ground	AP to Barrier,	Barrier to NS,	[C]	, m	Correction,	dB(A) ^[7]
E22-25	2	E22-25-2	E22-25-S4 82325	57 836	684	15.3 S4	823089	_		218.2	-54.8	3.0	43	18337	N	13.0	7.9	-	-	-	-	-	-	-	43
		E22-25-2	E22-25-S6			S6	823001	836707		256.6	-56.2	3.0	45	30045	N	13.0	13.3	-	-	-	-	-	-	-	45
		E22-25-2	E22-25-S7			S7	822966			294.3	-57.4	3.0	41	13557	N	13.0	13.3	-	-	-	-	-	-	-	41
		E22-25-2	E22-25-S8			S8	823027	836786		251.5	-56.0	3.0	38	6904	N	13.0	13.3	-	-	-	-	-	-	-	38
		E22-25-2	E22-25-S9			S9	823059	836822		241.3	-55.7	3.0	40	9618	N	13.0	13.3	-	-	-	-	-	-	-	40
		E22-25-2	E22-25-S10			S10	823216	836713	99.0	50.1	-42.0	3.0	60	990218	Y	13.0	13.3	36.8	5.2	13.5	37.6	50.1	1.0	18.1	42
		E22-25-2									Total SPL	, dB(A) ^[4]	60										Total S	PL, dB(A) ^[4] :	50
E41-23	2	E41-23-2	E41-23-S4 82333	30 836	557	15.3 S4		836544		240.7	-55.6	3.0	42	15071	Y	-	-	-	-	-	-	-	-	-	42
		E41-23-2	E41-23-S5			S5	823153	836442	98.5	210.7	-54.5	3.0	47	50309	Y	-	-	-	-	-	-	-	-	-	47
		E41-23-2									Total SPL	, dB(A) ^[4]	48										Total S	PL, dB(A) ^[4] :	48
E41-24	2	E41-24-2	E41-24-S4 82332	28 836	556	15.3 S4	823089	836544	94.4	238.7	-55.6	3.0	42	15329	Y	-	-	-	-	-	-	-	-	-	42
		E41-24-2	E41-24-S5			S5	823153	836442	98.5	208.7	-54.4	3.0	47	51306	Y	-	-	-	-	-	-	-	-	-	47
E41-24-2 To												, dB(A) ^[4]	48										Total S	PL, dB(A) [4]:	48
E42-24	2	E42-24-2	E42-24-S1 82342	25 836	542	15.3 S1	823601	836709	91.4	243.6	-55.7	3.0	39	7359	N			-	-	-	-	-	-	-	39
		E42-24-2	E42-24-S2			S2	823652	836655	94.9	253.6	-56.1	3.0	42	15199	N			-	-	-	-	-	-	-	42
		E42-24-2	E42-24-S3-1			S3-1		836630		200.9	-54.1	3.0	46	37363	Y	15.3	0.5	200.4	4.9	0.5	200.7	200.9	0.3	12.9	33
		E42-24-2	E42-24-S3-2					836649		229.3	-55.2	3.0	47	47256	Y	15.3	0.5	228.8	4.9	0.5	229.0	229.3	0.2	12.4	34
L		E42-24-2	E42-24-S11b			511	823447	836539	99.0	22.5	-35.1	3.0	67	4896798	Y	15.3	0.5	22.0	7.4	0.5	23.4	22.5	1.4	19.4	48
	E42-24-2 Total SPL, dB(A) [4]: 67																Total SPL,	dB(A) [4] & [10]:	49						
E42-25	2	E42-25-2		22 836	539	15.3 S1	823601	836709	91.4	247.3	-55.9	3.0	39	7142	N			-	-	-	-	-	-	-	39
		E42-25-2	E42-25-S2			S2	823652			257.0	-56.2	3.0	42	14799	N			-	-	-	-	-	-	-	42
		E42-25-2	E42-25-S3-1			S3-1		836630		204.3	-54.2	3.0	46	36130	Y	15.3	0.5	203.8	4.9	0.5	204.1	204.3	0.3	12.8	33
		E42-25-2	E42-25-S3-2			S3-2		836649		232.7	-55.3	3.0	47	45871	Y	15.3	0.5	232.2	4.9	0.5	232.5	232.7	0.2	12.3	34
L		E42-25-2	E42-25-S11b			511	823447	836539	99.0	24.8	-35.9	3.0	66	4042547	Y	15.3	0.5	24.3	7.4	0.5	25.5	24.8	1.3	19.0	47
E42-25-2											Total SPL	, dB(A) [4]	66										Total SPL,	dB(A) [4] & [10]:	49
E43-24	2	E43-24-2	E43-24-S1 82342	27 836	548	15.3 S1	823601	836709	91.4	237.2	-55.5	3.0	39	7762	N			-	-	-	-	-	-	-	39
		E43-24-2	E43-24-S2			S2	823652	836655	94.9	248.3	-55.9	3.0	42	15845	N			-	-	-	-	-	-	-	42
		E43-24-2	E43-24-S3-1			S3-1	823605	836630	96.8	195.7	-53.8	3.0	46	39371	Y	15.3	0.5	195.2	4.9	0.5	195.5	195.7	0.3	13.0	33
		E43-24-2	E43-24-S3-2			S3-2	823627	836649	99.0	224.0	-55.0	3.0	47	49536	Y	15.3	0.5	223.5	4.9	0.5	223.7	224.0	0.2	12.5	34
		E43-24-2	E43-24-S11			S11	823449	836546	99.0	21.7	-34.7	3.0	67	5292111	Y	15.3	0.5	21.2	7.4	0.5	22.6	21.7	1.4	19.5	48
E43-24-2 Total S											Total SPL	, dB(A) [4]	67					•					Total SPL,	dB(A) [4] & [10]:	49

			Noise Source (NS)					Correction		Unmitigated		Consider for	Barrier	Horizontal	Horizontal	NS level (1m	Slant	Slant	Distance from	Path	Path	Mitigated				
In.	Floor			l		Height	5		١.,	SWL,	from NS to	Dietenes	Facade	Noise Level,	Intensity	Path	Height,	Distance from	Distance from	above	Distance from	Distance from	AP to NS, m	Difference	Difference	Noise Level,
	FIOOI			_ ×	У	, mPD	טו	X	У	dB(A)	AP, m ^[1]	Distance	raçaue	dB(A) [2][3][4]		Difference?	mPD	AP to Barrier,	NS to Barrier,	ground	AP to Barrier,	Barrier to NS,	[C]	, m	Correction,	dB(A) [7]
E43-2	2	E43-25-2	E43-25-S1	823425	836546	15.3	S1	823601	836709	91.4	240.9	-55.6	3.0	39	7528	N			-	-	-	-	-	-	-	39
		E43-25-2	E43-25-S2	1			S2	823652	836655	94.9	251.7	-56.0	3.0	42	15423	N			-	-	-	-	-	-	-	42
		E43-25-2	E43-25-S3-1				S3-1	823605	836630	96.8	199.1	-54.0	3.0	46	38053	Y	15.3	0.5	198.6	4.9	0.5	198.9	199.1	0.3	12.9	33
		E43-25-2	E43-25-S3-2				S3-2	823627	836649	99.0	227.4	-55.1	3.0	47	48062	Y	15.3	0.5	226.9	4.9	0.5	227.1	227.4	0.2	12.4	34
		E43-25-2	E43-25-S11				S11	823449	836546	99.0	23.9	-35.6	3.0	66	4353133	Y	15.3	0.5	23.4	7.4	0.5	24.7	23.9	1.3	19.1	47
	-	E43-25-2										Total SPL	., dB(A) ^[4]	66										Total SPL,	dB(A) [4] & [10]:	49

E43-25-2 Notes:

The shortest horizontal distance is adopted in the calculation for unmitigated scenario to represent the worst-case scenario.

Assessment is not conducted for NS with no line of sight to the AP (i.e. completely shielded by building structures, or AP is completely not facing the NS), or the whole area of the NS is located more than 300m away from the AP. [2]

Unmitigated Noise Level = Sound Power Level of Noise Source + Distance Correction + Façade Correction

Values in red exceed the night-time noise criteria of 50 dB(A). Site visits were carried out and that the above fixed noise sources had no night-time operation. To be conservative, night-time noise criteria has been referenced.

[4] Path difference is considered for AP exceeding the noise criteria, and with noise barrier proposed between its line of the sight to the NS. [5]

The path difference correct is calculated by Maekawa Equation and capped at 20 dB(A).

[7] Mitigated Noise Level = Unmitigated Noise Level - Path Distance Correction

Line of sight is completely blocked by proposed acoustic fin.

Single aspect design has been adopted as a mitigation measure.

For NSRs at 2/F at E42-24, E42-25, E43-24, E43-25, noise mitigation meaures such as 1.2m high parapet wall (at 15.3mPD) and fixed glazing/ blank façade have been proposed (See Figure 4.6 for illustrastion). Such parapet wall would provide noise shielding to fixed noise sources, which has been considered in the noise calculation. Accordingly, the same noise mitigation measures will also be applied to houses at D01, E42 to E50. The exact noise mitigation measures will be subject to detailed design stage.

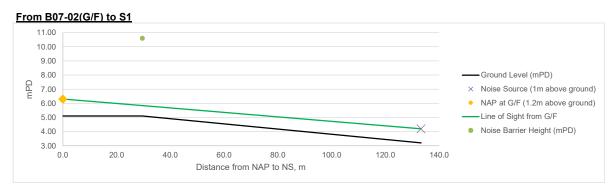
[1]

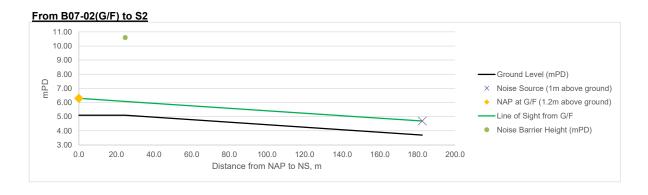
For noise sources at S10 and S11, which are in adjacent to the Subject Site, corresponding notional source locations (i.e. S10a to S10c and S11a to S11b) with respective to their nearest representative NSR locations, are then derived and adopted for the purpose of noise assessment.

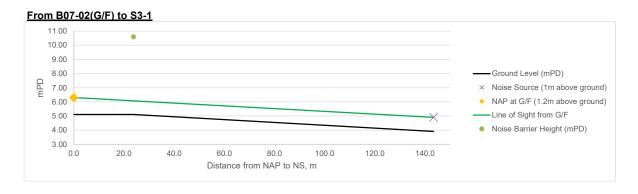
Appendix 4.3

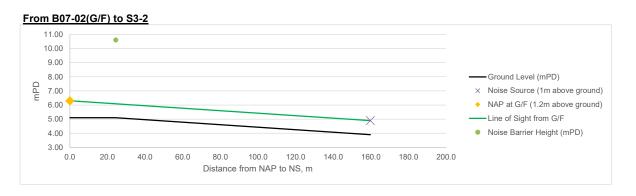
Cross Sections of Assessment Points to Noise Sources with Proposed Noise Barriers

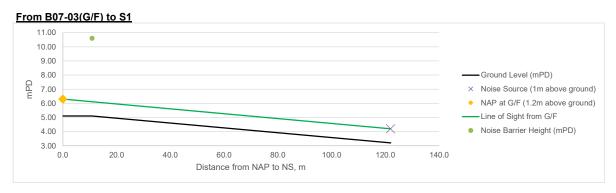


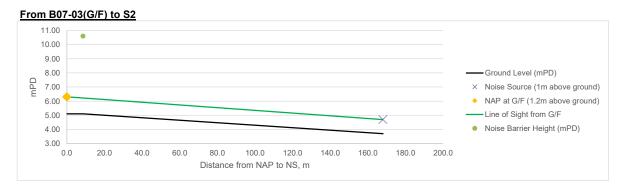


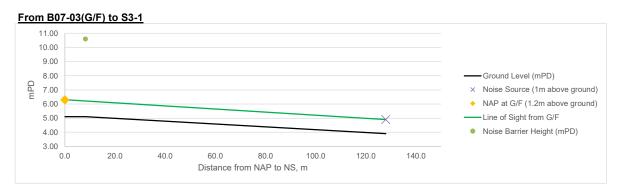


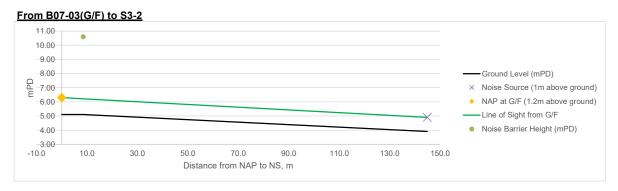


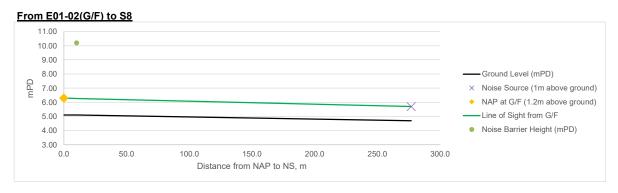


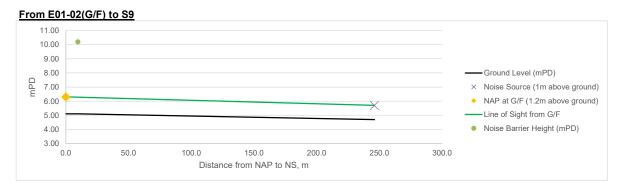


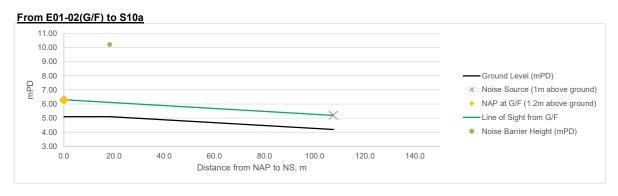


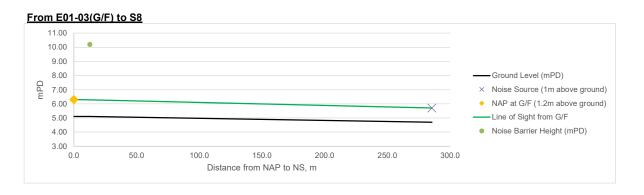


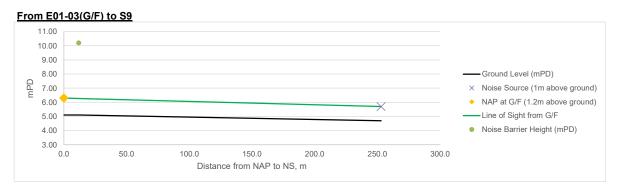


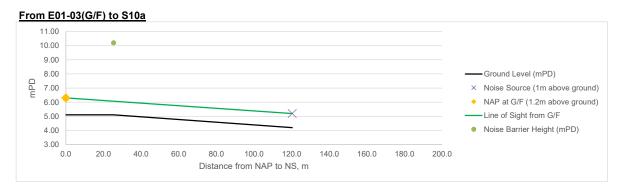


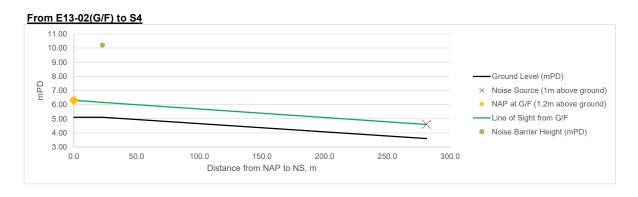


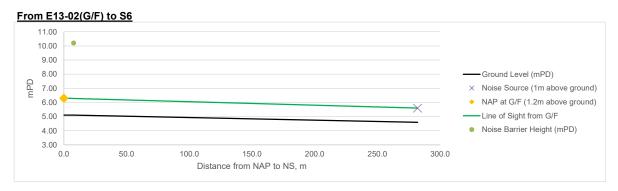


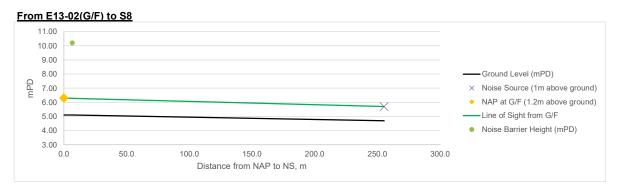


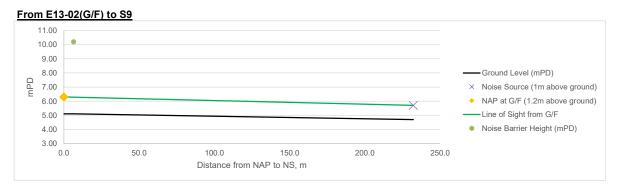


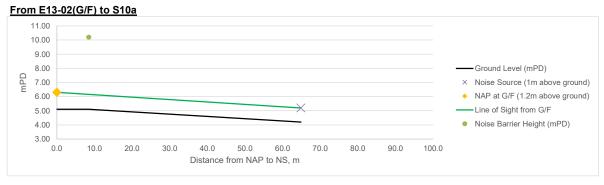


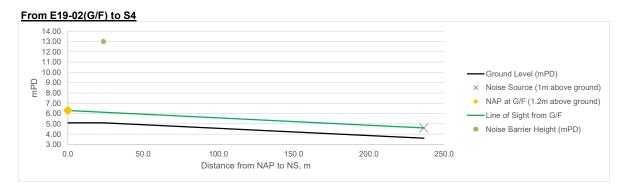


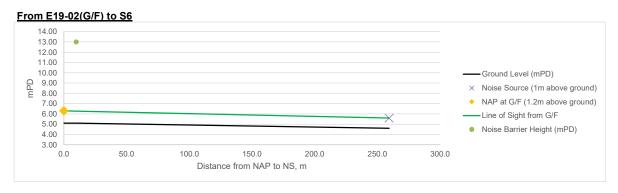


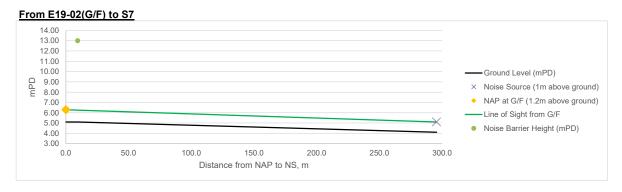


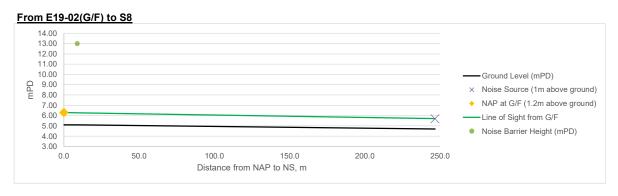


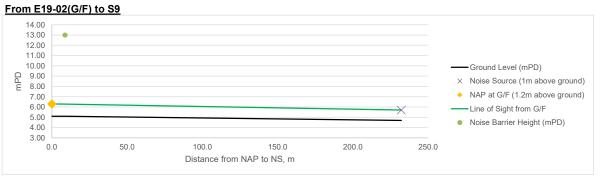


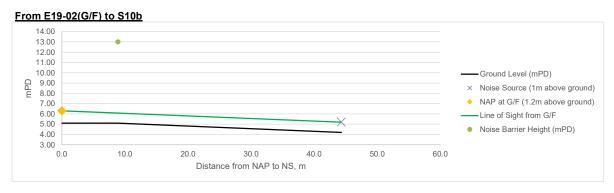


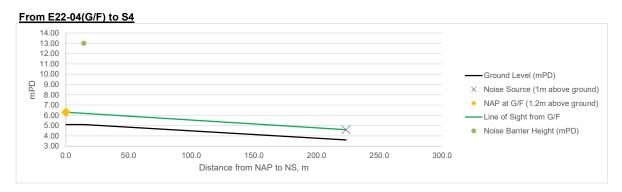


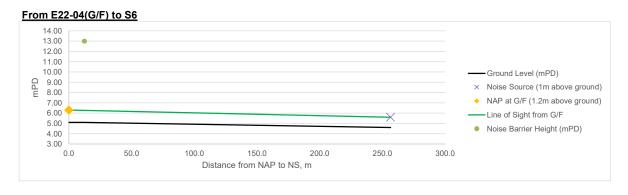


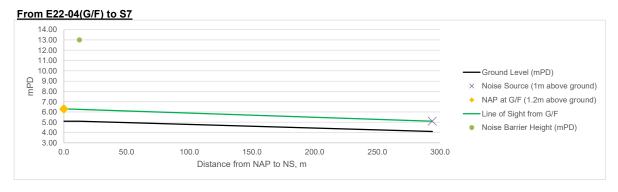


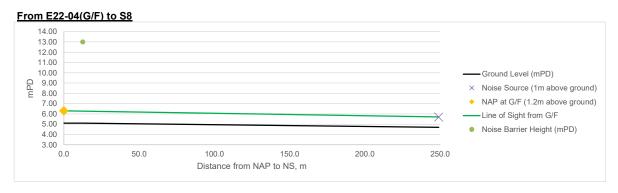


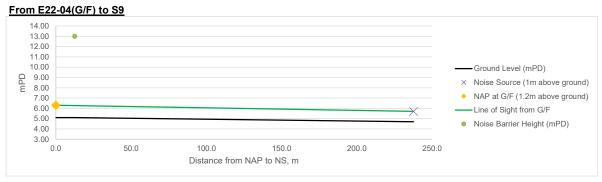


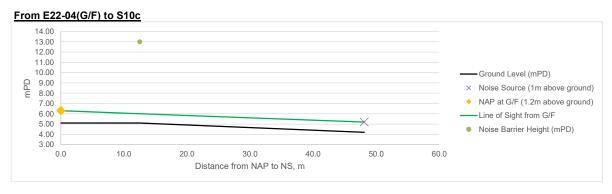


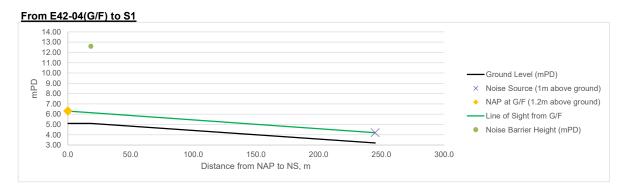


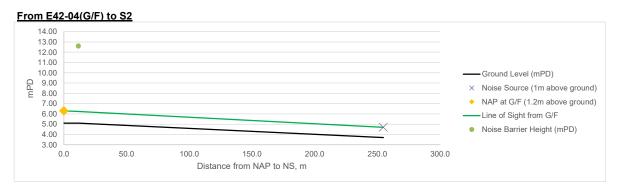


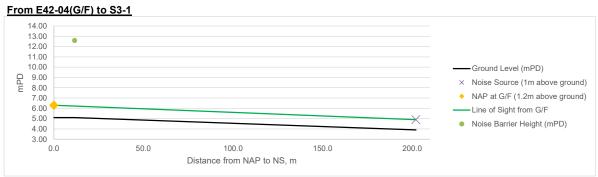


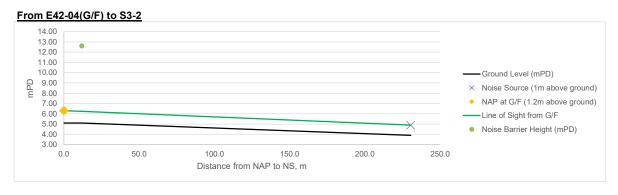


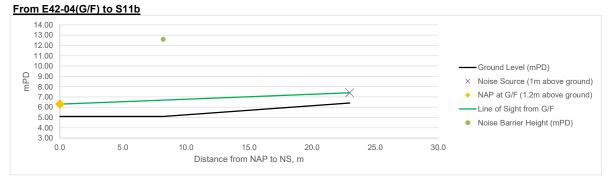


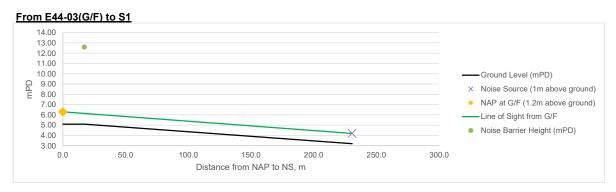


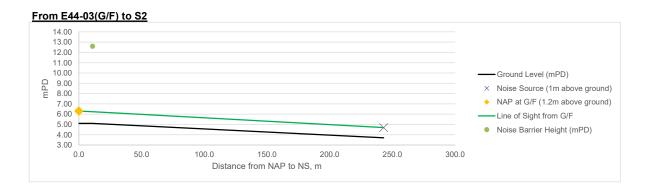


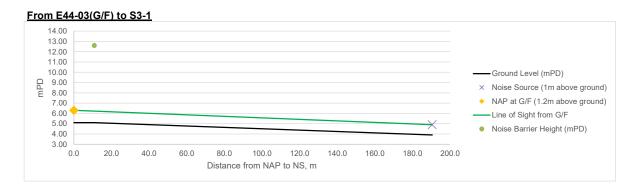


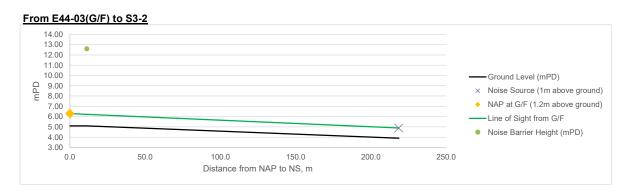


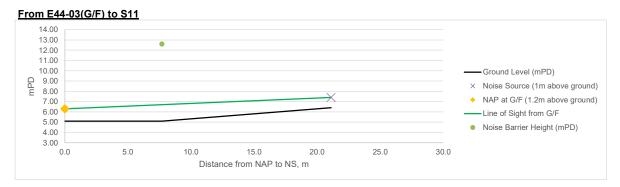


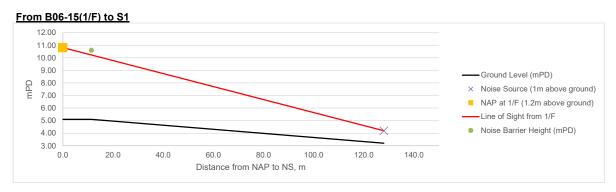


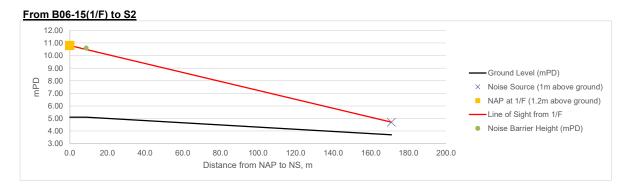


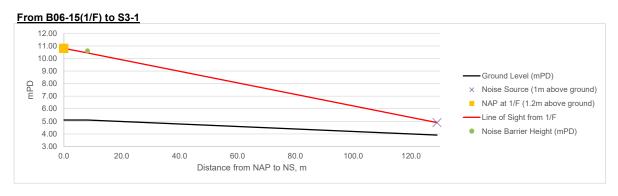


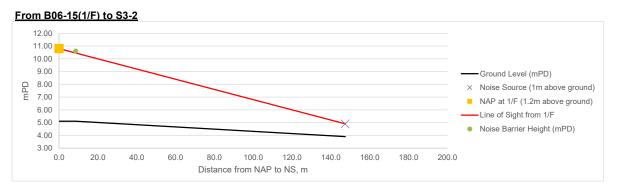


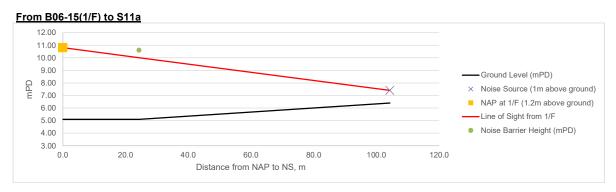


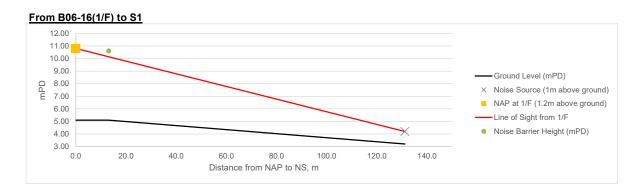


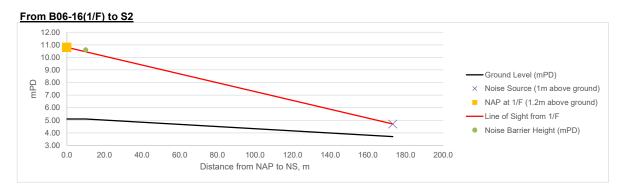


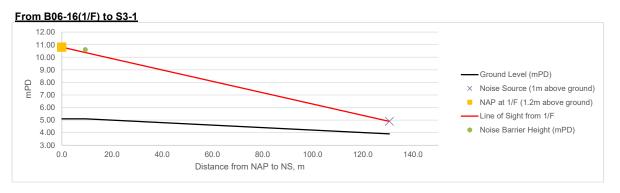


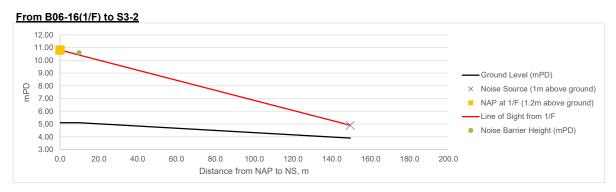


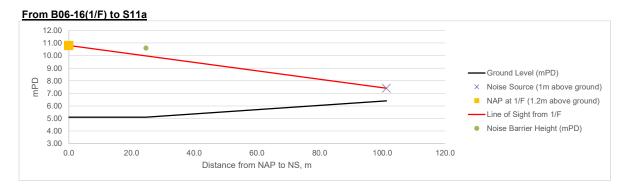


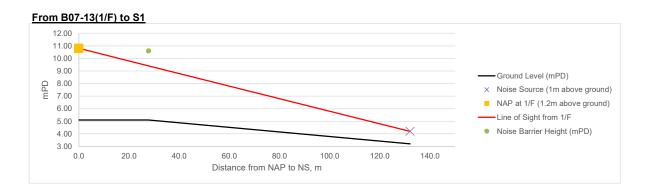


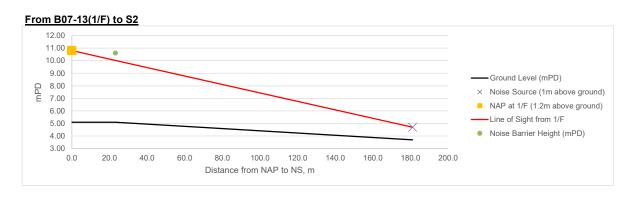


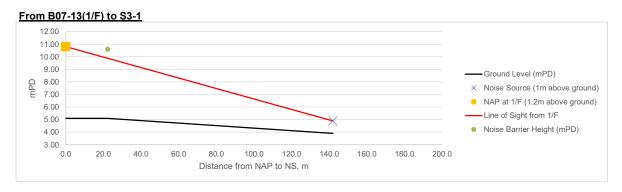


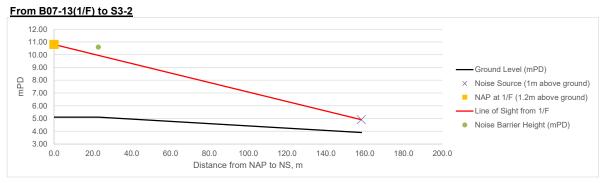


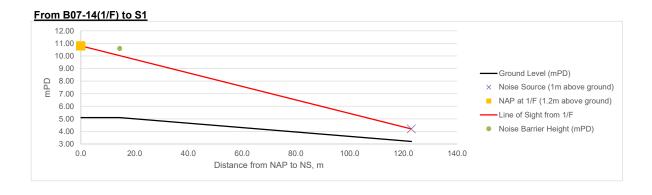


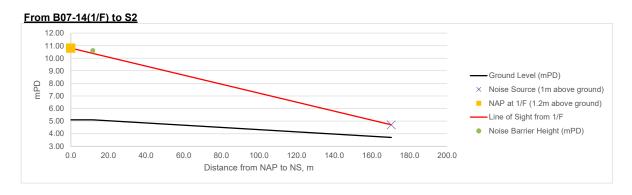


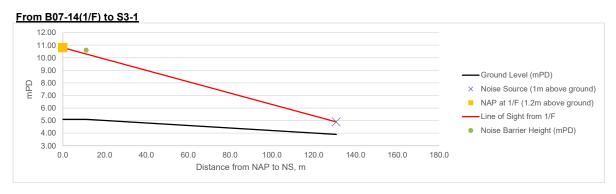


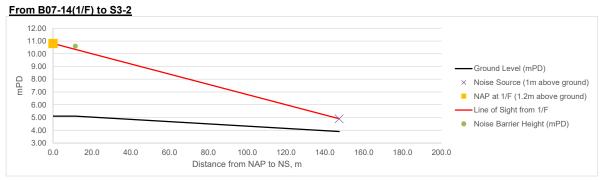


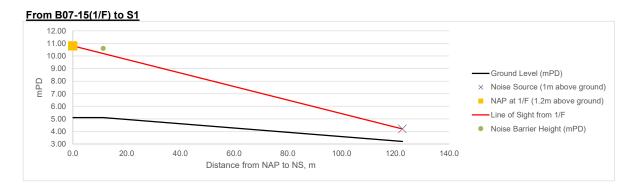


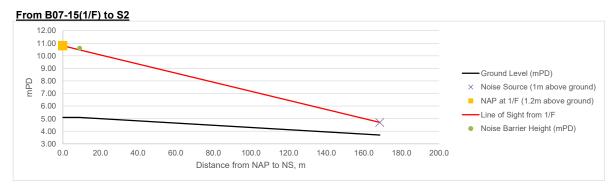


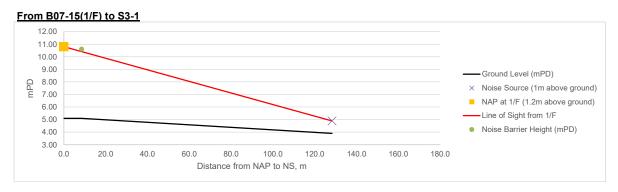


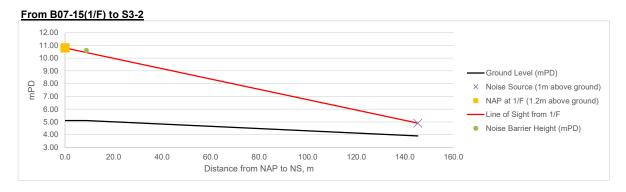


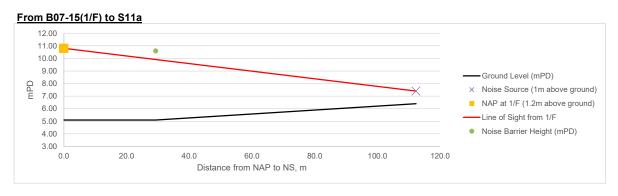


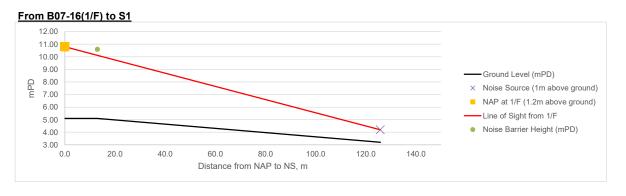


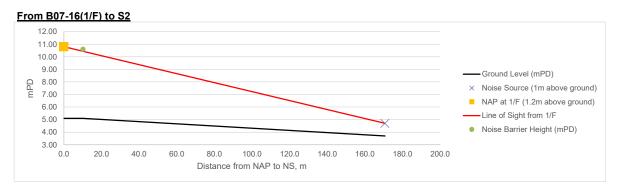


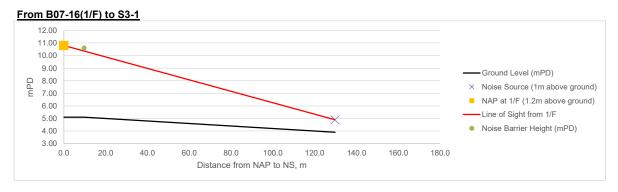


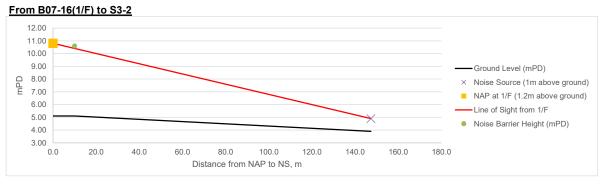


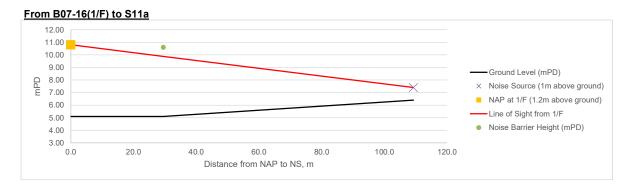


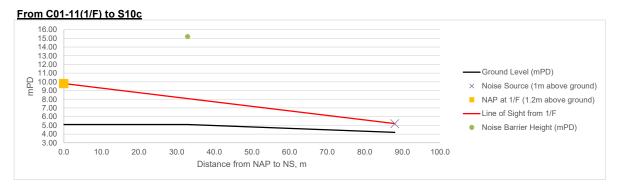


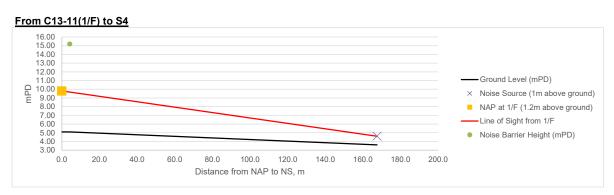


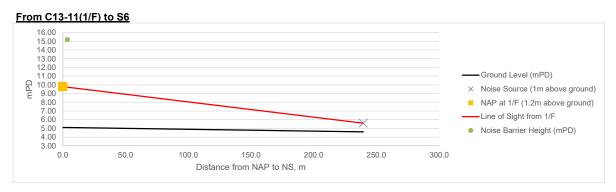


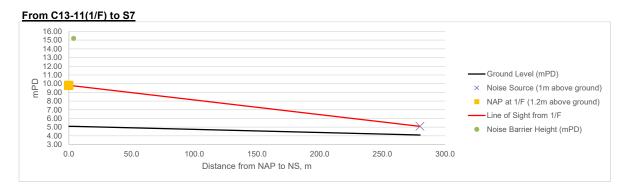


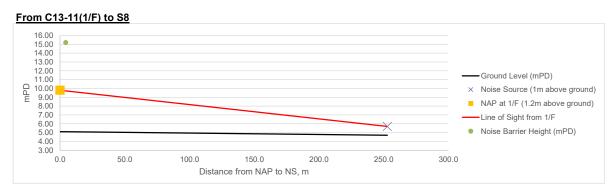


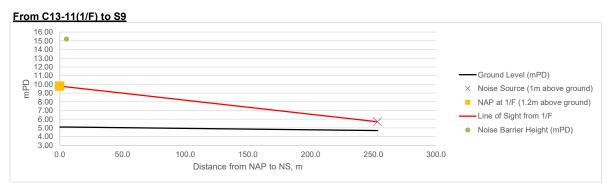


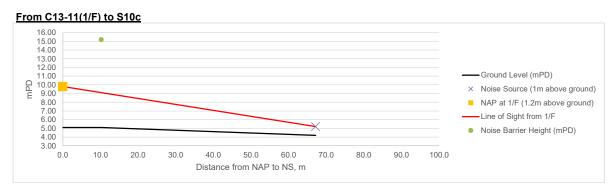


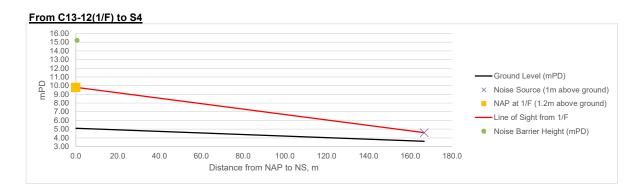


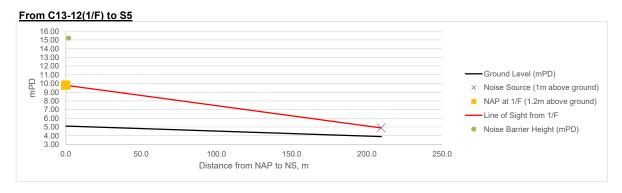


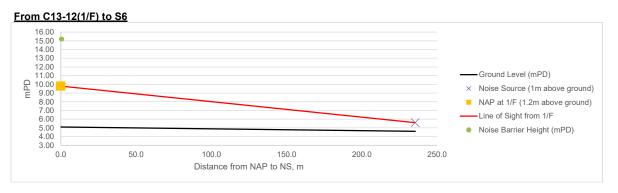


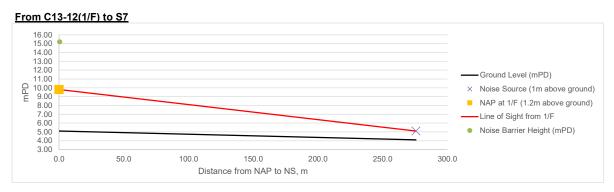


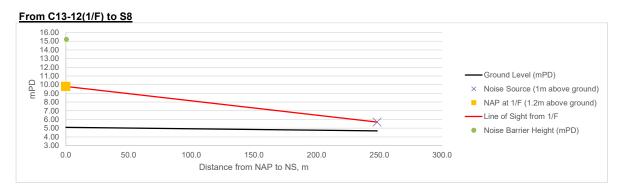


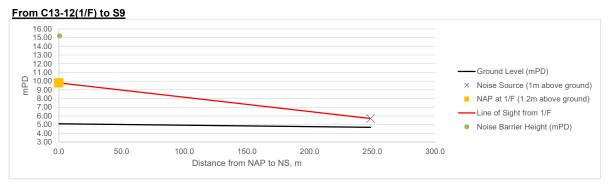


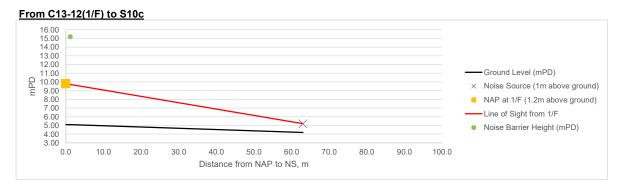


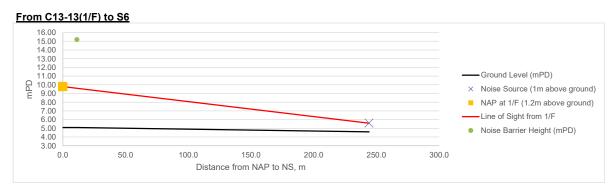


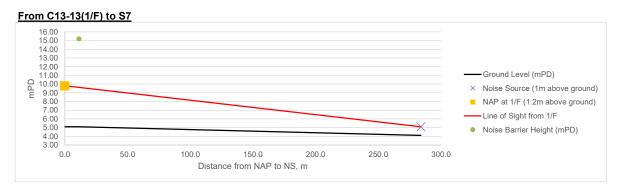


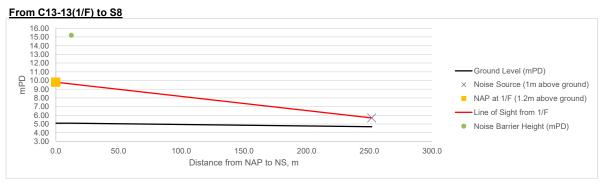


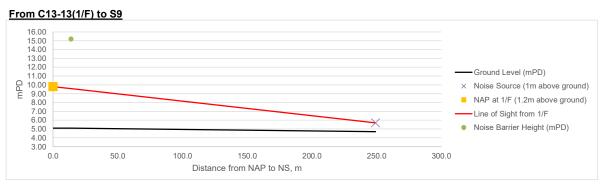


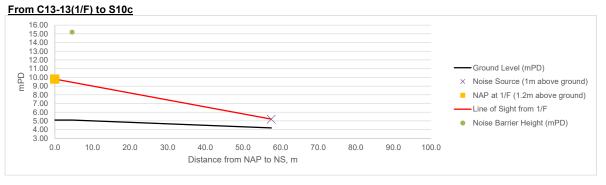


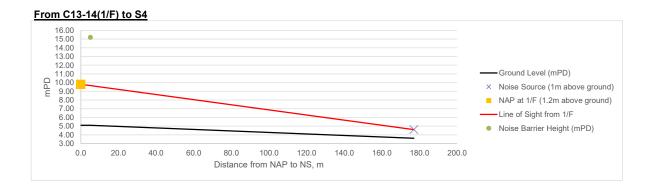


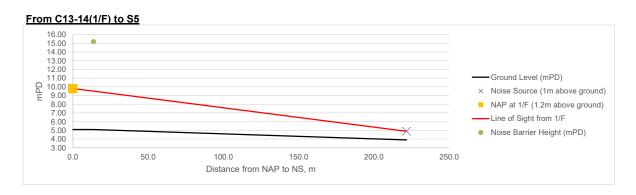


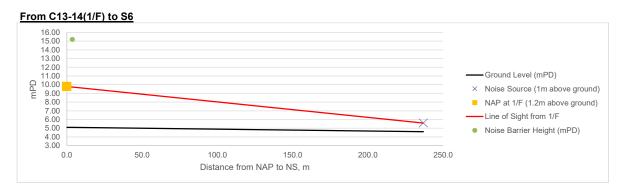


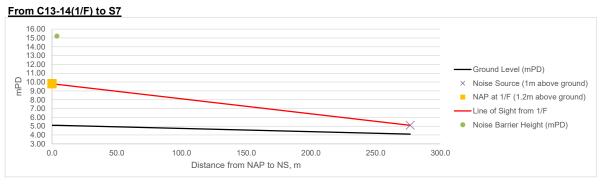


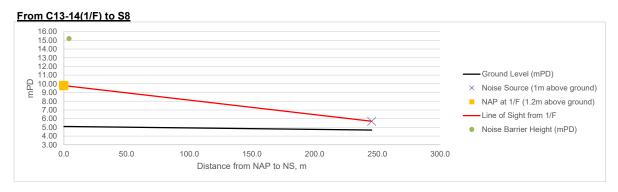


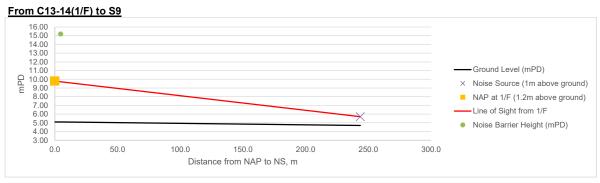


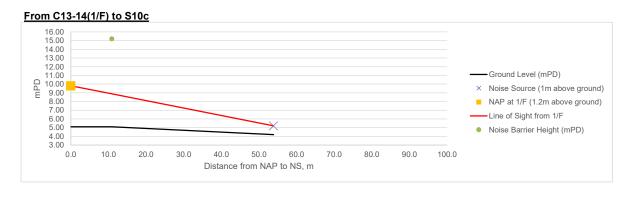


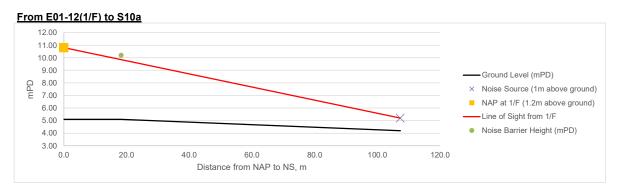


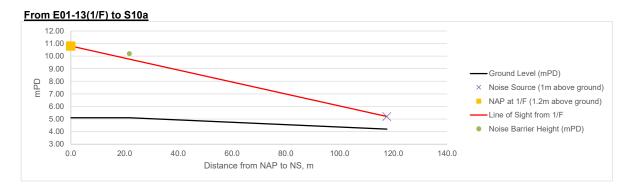


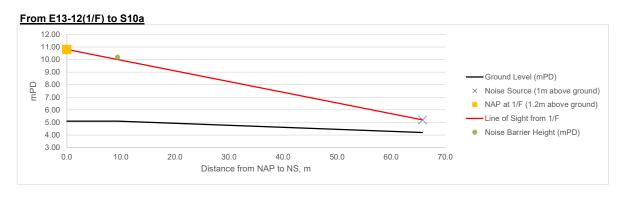


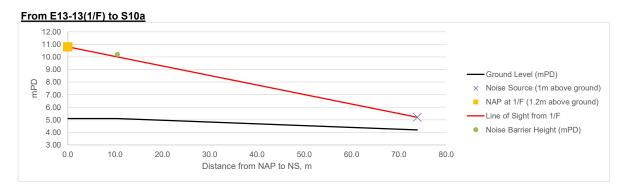


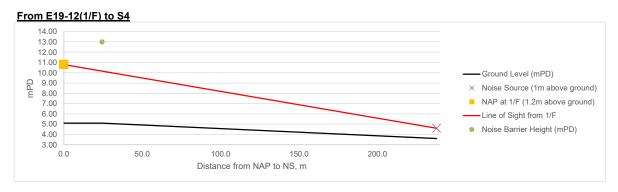


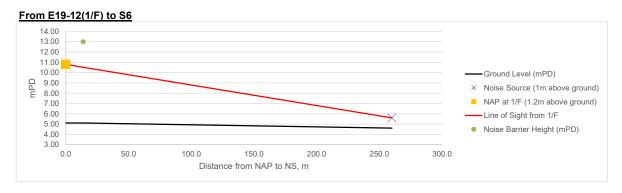


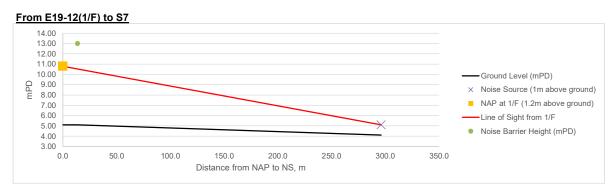


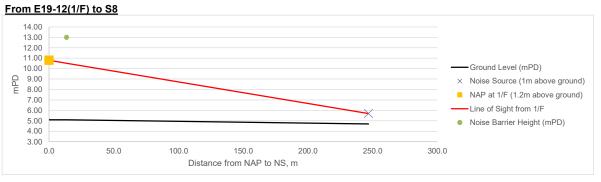


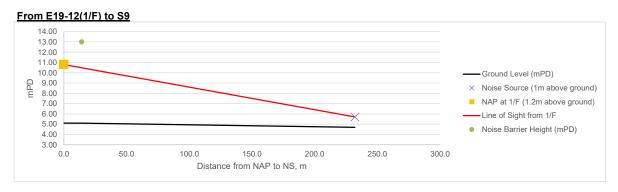


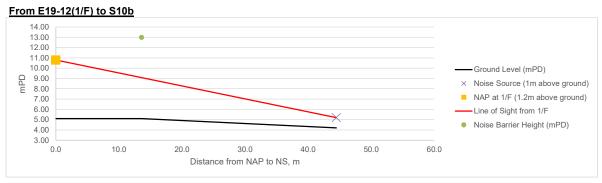


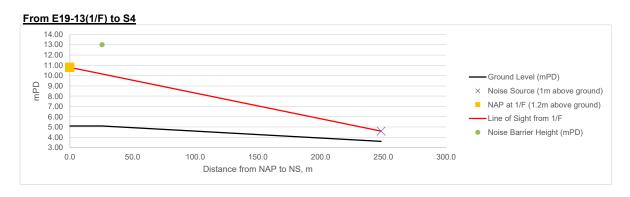


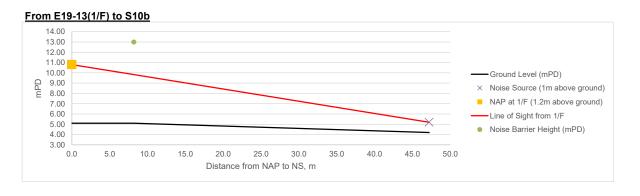


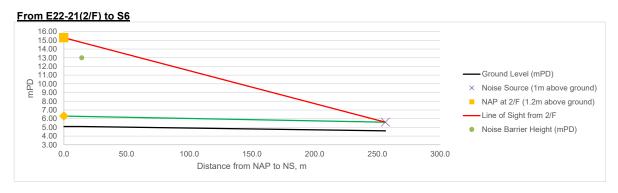


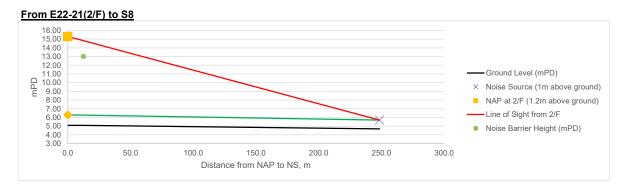


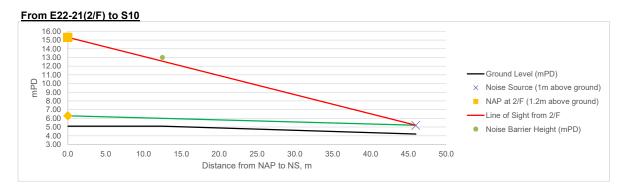




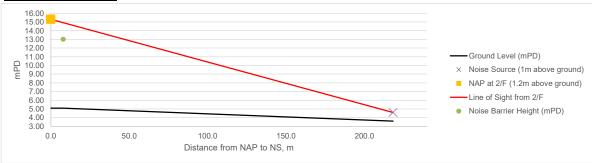




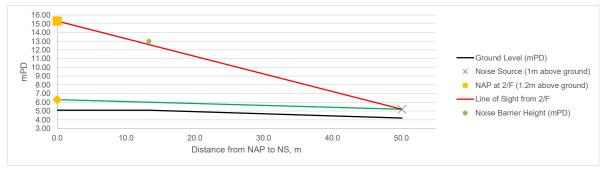


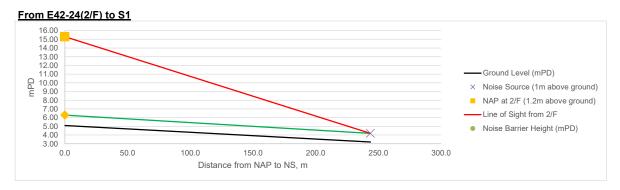


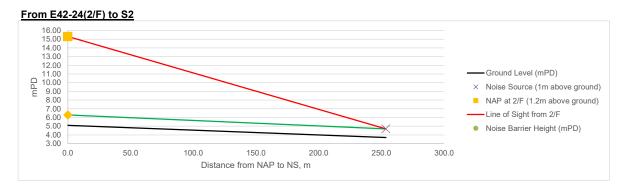
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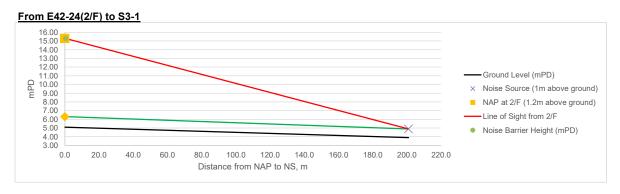


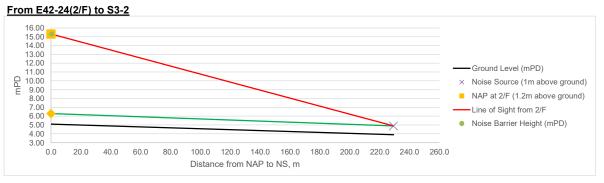
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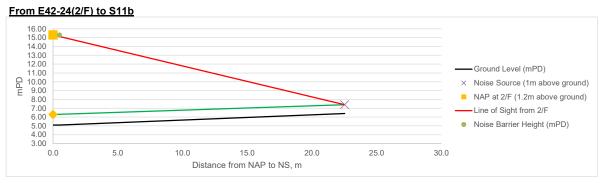


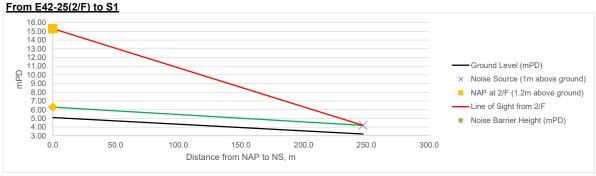


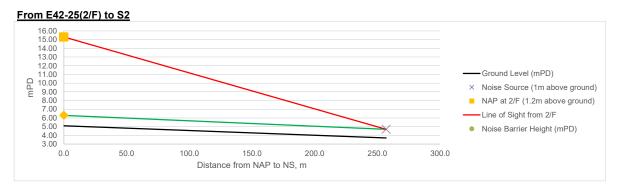


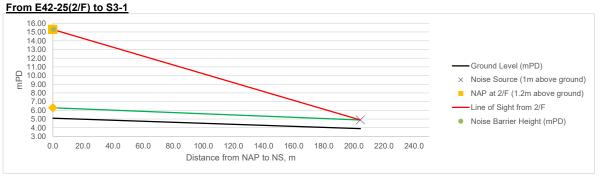


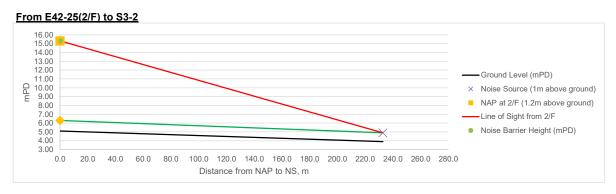


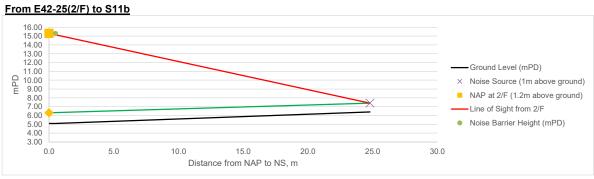


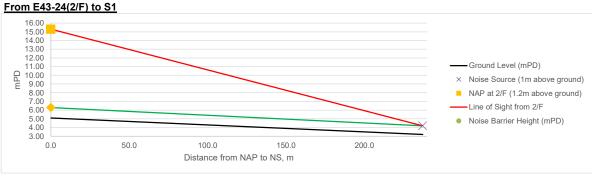


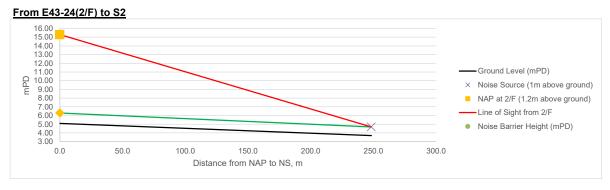


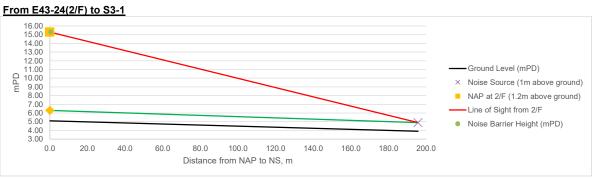


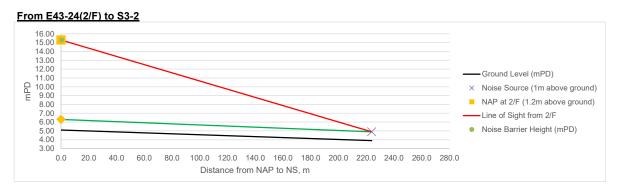


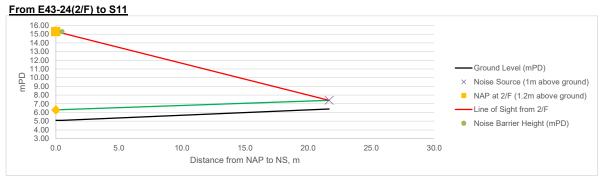


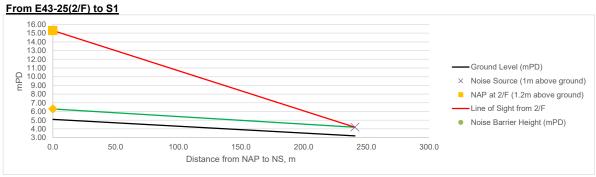


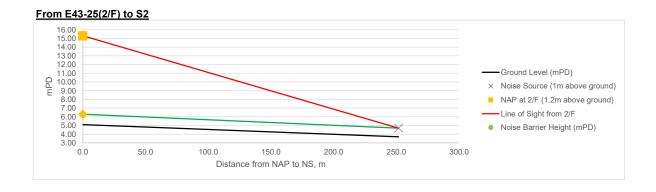


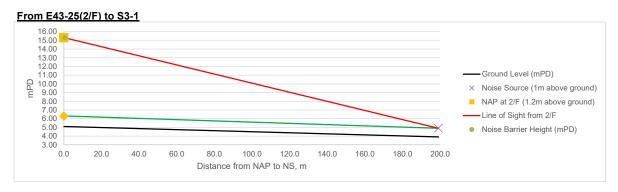


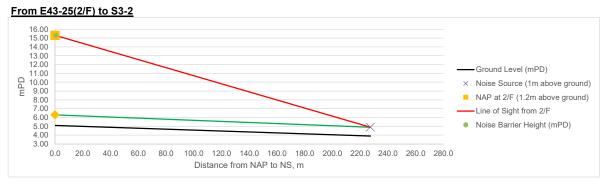


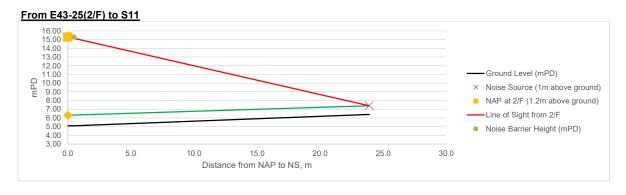


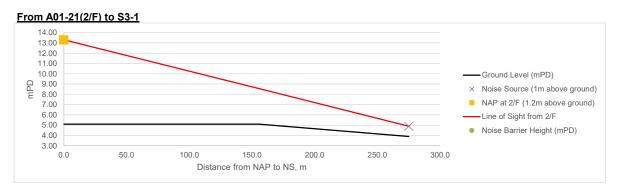


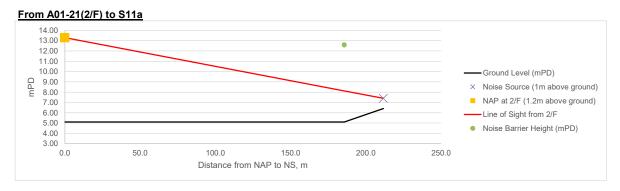


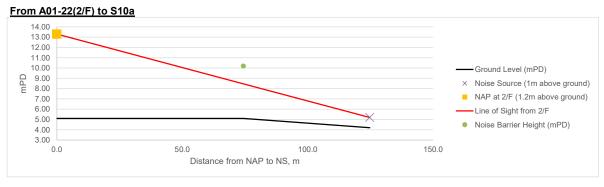


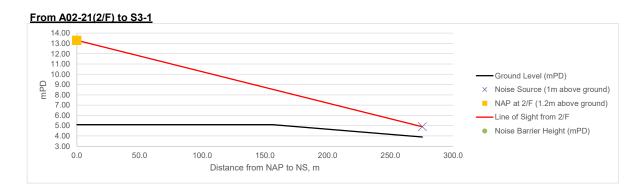


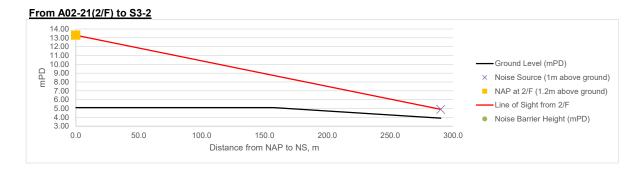


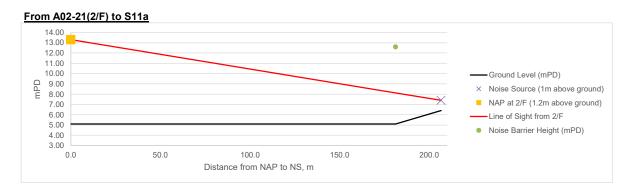


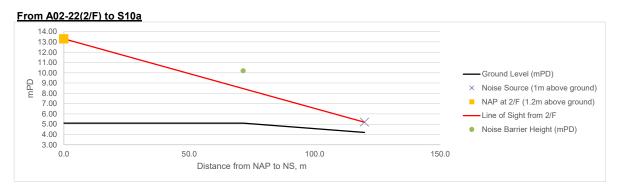


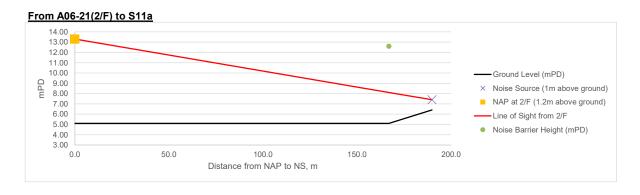


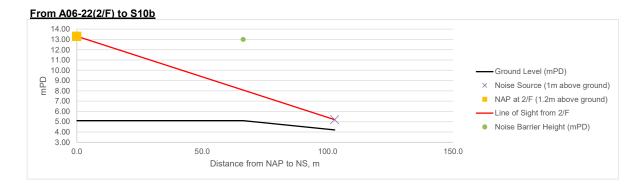


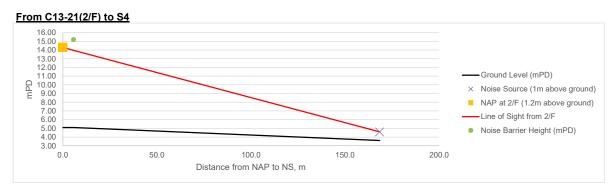


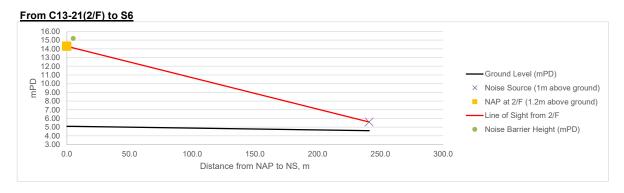


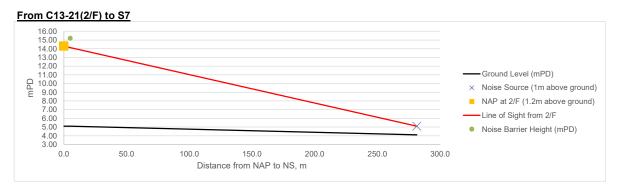


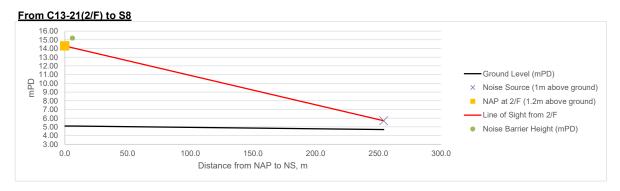


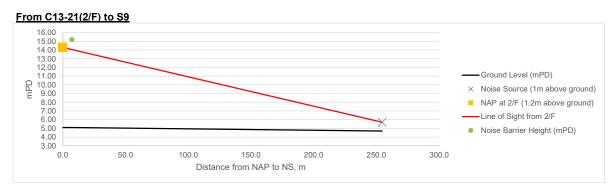


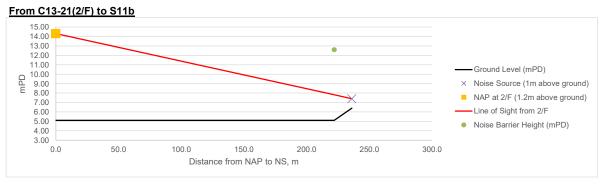


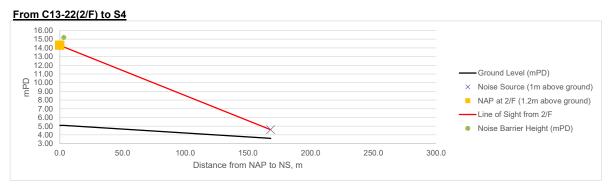


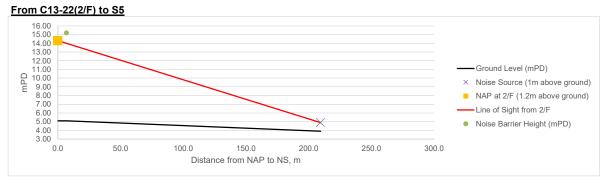


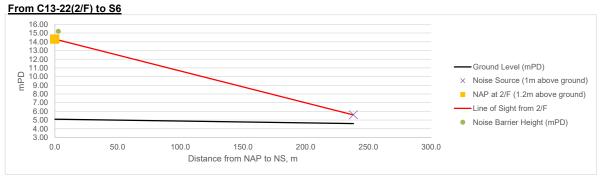


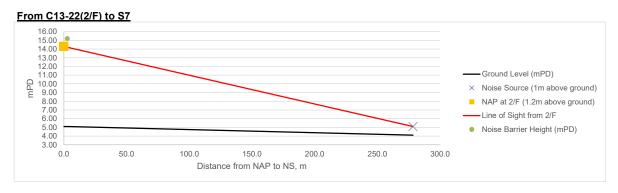


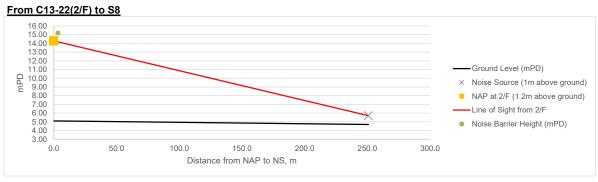


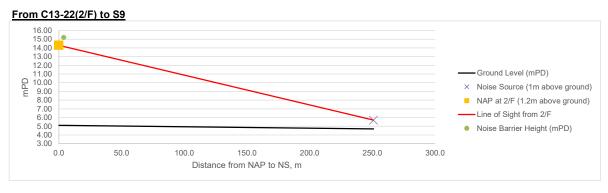


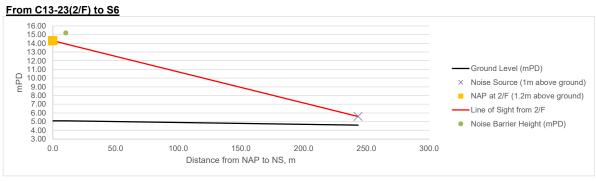


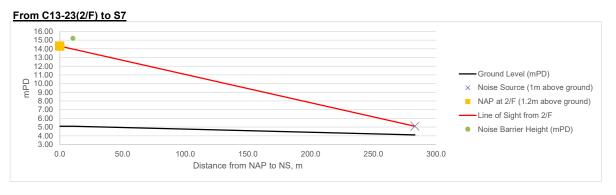


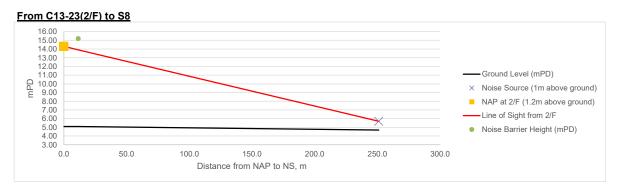


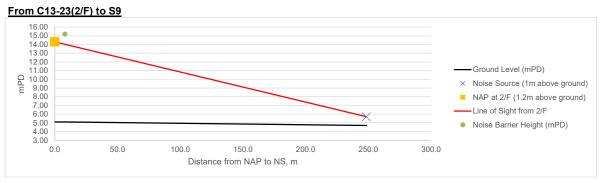


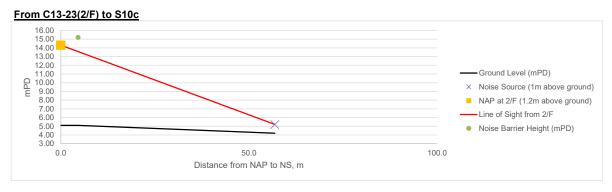


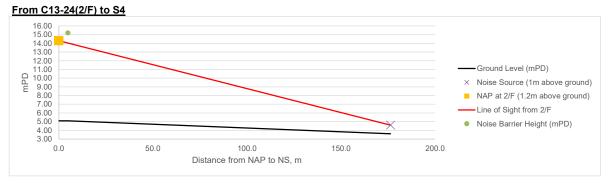


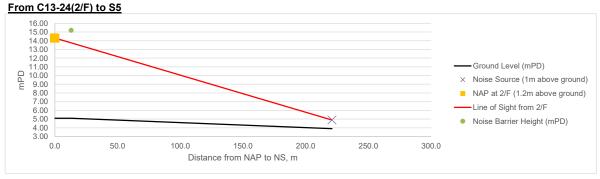


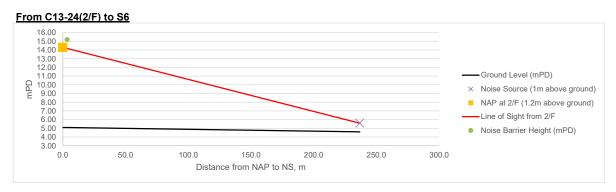


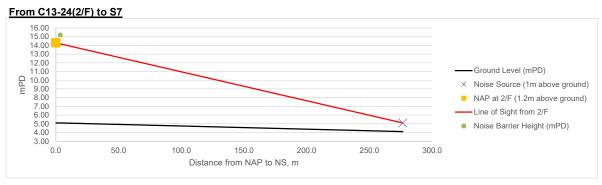


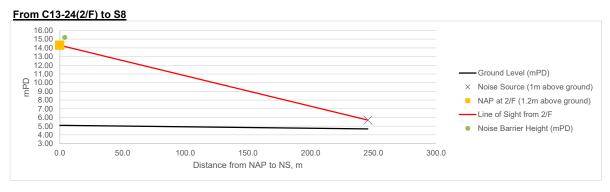


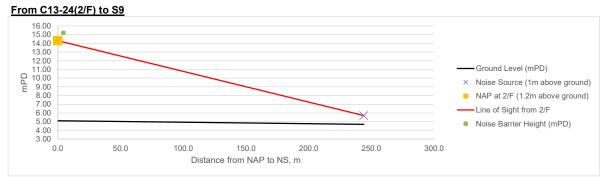


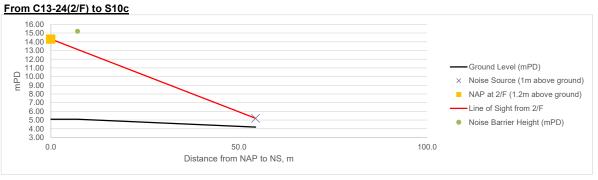


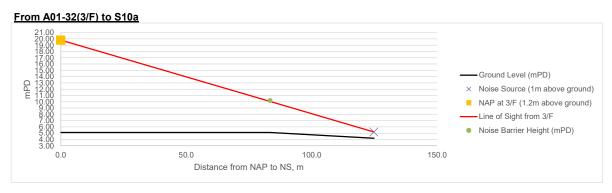


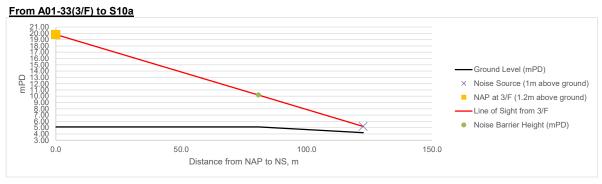


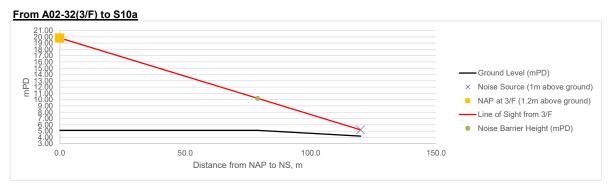


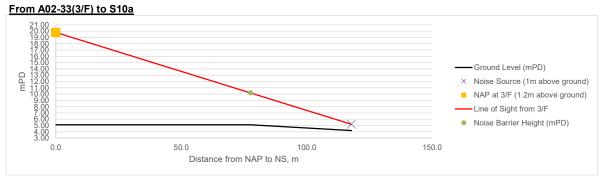


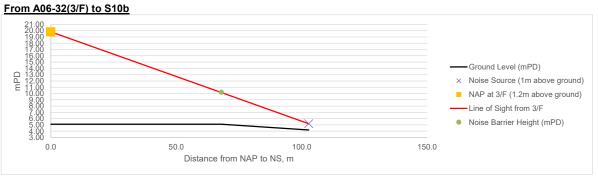


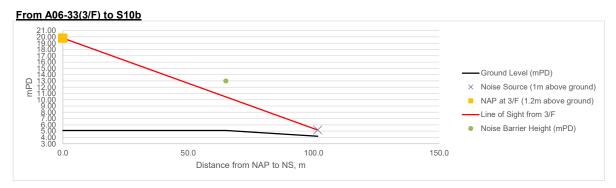












Appendix 5.1

WQOs of Deep Bay WCZ in the Schedule of Cap. 358R



Water Quality Objective Set Out in the Schedule of Cap. 358R (reproduced from Cap. 358R)

Parameter	WQOs	Part of Water Control Zone (WCZ)
A. Aesthetic Appearance	(a) Waste discharges shall cause no objectionable odours or discolouration of the water.	Whole Zone
	(b) Tarry residues, floating wood, articles made of glass, plastic, rubber or of any other substances should be absent.	
	(c) Mineral oil should not be visible on the surface. Surfactants should not give rise to a lasting foam.	
	(d) There should be no recognisable sewage-derived debris.	
	(e) Floating, submerged and semi-submerged objects of a size likely to interfere with the free movement of vessels, or cause damage to vessels, should be absent.	
	(f) Waste discharges shall not cause the water to contain substances which settle to form objectionable deposits.	
B. Bacteria (The level of Escherichia coli)	(a) It should not exceed 610 per 100 mL, calculated as the geometric mean of all samples collected in one calendar year.	Secondary Contact Recreation Subzone and Mariculture Subzone
	(b) It should be zero per 100 mL, calculated as the running median of the most recent 5 consecutive samples taken at intervals of between 7 and 21 days.	Yuen Long & Kam Tin (Upper) Subzone, Beas Subzone, Indus Subzone, Ganges Subzone and Water Gathering Ground Subzones
	(c) It should not exceed 1 000 per 100 mL, calculated as the running median of the most recent 5 consecutive samples taken at intervals of between 7 and 21 days.	Yuen Long & Kam Tin (Lower) Subzone and other inland waters
	(d) It should not exceed 180 per 100 mL, calculated as the geometric mean of all samples collected from March to October inclusive in one calendar year. Samples should be taken at least 3 times in a calendar month at intervals of between 3 and 14 days.	Yung Long Bathing Beach Subzone
C. Colour	(a) Waste discharges shall not cause the colour of water to exceed 30 Hazen units.	Yuen Long & Kam Tin (Upper) Subzone, Beas Subzone, Indus Subzone, Ganges Subzone and Water Gathering Ground Subzones

Parameter	WQOs	Part of Water Control Zone (WCZ)
	(b) Waste discharges shall not cause the colour of water to exceed 50 Hazen units.	Yuen Long & Kam Tin (Lower) Subzone and other inland waters
D. Dissolved Oxygen	(a) Waste discharges shall not cause the level of dissolved oxygen to fall below 4 milligrams per litre for 90% of the sampling occasions during the year; values should be taken at 1 metre below surface.	Inner Marine Subzone excepting Mariculture Subzone
	(b) Waste discharges shall not cause the level of dissolved oxygen to fall below 4 milligrams per litre for 90% of the sampling occasions during the year; values should be calculated as water column average (arithmetic mean of at least 2 measurements at 1 metre below surface and 1 metre above seabed). In addition, the concentration of dissolved oxygen should also not be less than 2 milligrams per litre within 2 metres of the seabed for 90% of the sampling occasions during the year.	Outer Marine Subzone excepting Mariculture Subzone
	(c) The dissolved oxygen level should not be less than 5 milligrams per litre for 90% of the sampling occasions during the year; values should be taken at 1 metre below surface.	Mariculture Subzone
	(d) Waste discharges shall not cause the level of dissolved oxygen to be less than 4 milligrams per litre.	Yuen Long & Kam Tin (Upper and Lower) Subzones, Beas Subzone, Indus Subzone, Ganges Subzone, Water Gathering Ground Subzones and other inland waters of the Zone
E. pH	(a) The pH of the water should be within the range of 6.5–8.5 units. In addition, waste discharges shall not cause the natural pH range to be extended by more than 0.2 units.	Marine waters excepting Yung Long Bathing Beach Subzone
	(b) Waste discharges shall not cause the pH of the water to exceed the range of 6.5–8.5 units.	Yuen Long & Kam Tin (Upper and Lower) Subzones, Beas Subzone, Indus Subzone, Ganges Subzone and Water Gathering Ground Subzones
	(c) The pH of the water should be within the range of 6.0–9.0 units.	Other inland waters
	(d) The pH of the water should be within the range of 6.0–9.0 units for 95% of samples. In addition, waste discharges shall not cause the	Yung Long Bathing Beach Subzone

Parameter	WQOs	Part of Water Control Zone (WCZ)
	natural pH range to be extended by more than 0.5 units.	
F. Temperature	(a) Waste discharges shall not cause the natural daily temperature range to change by more than 2.0 $^{\circ}\!$	Whole Zone
G. Salinity	(a) Waste discharges shall not cause the natural ambient salinity level to change by more than 10%.	Whole Zone
H. Suspended Solids	(a) Waste discharges shall neither cause the natural ambient level to be raised by 30% nor give rise to accumulation of suspended solids which may adversely affect aquatic communities.	Marine waters
	(b) Waste discharges shall not cause the annual median of suspended solids to exceed 20 milligrams per litre.	Yuen Long & Kam Tin (Upper and Lower) Subzones, Beas Subzone, Ganges Subzone, Indus Subzone, Water Gathering Ground Subzones and other inland waters
I. Ammonia	(a) The un-ionized ammoniacal nitrogen level should not be more than 0.021 milligram per litre, calculated as the annual average (arithmetic mean).	Whole Zone
J. Nutrients	(a) It shall not be present in quantities sufficient to cause excessive or nuisance growth of algae or other aquatic plants.	Inner and Outer Marine Subzones
	(b) Without limiting the generality of objective (a) above, the level of inorganic nitrogen should not exceed 0.7 milligram per litre, expressed as annual mean.	Inner Marine Subzone
	(c) Without limiting the generality of objective (a) above, the level of inorganic nitrogen should not exceed 0.5 milligram per litre, expressed as annual water column average (arithmetic mean of at least 2 measurements at 1 metre below surface and 1 metre above seabed).	Outer Marine Subzone
K. 5-day Biochemical Oxygen Demand	(a) Waste discharges shall not cause the 5-day biochemical oxygen demand to exceed 3 milligrams per litre.	Yuen Long & Kam Tin (Upper) Subzone, Beas Subzone, Indus Subzone, Ganges Subzone and Water Gathering Ground Subzones

Parameter	WQOs	Part of Water Control Zone (WCZ)
	(b) Waste discharges shall not cause the 5-day biochemical oxygen demand to exceed 5 milligrams per litre.	Yuen Long & Kam Tin (Lower) Subzone and other inland waters
L. Chemical Oxygen Demand	(a) Waste discharges shall not cause the chemical oxygen demand to exceed 15 milligrams per litre.	Yuen Long & Kam Tin (Upper) Subzone, Beas Subzone, Indus Subzone, Ganges Subzone and Water Gathering Ground Subzones
	(b) Waste discharges shall not cause the chemical oxygen demand to exceed 30 milligrams per litre.	Yuen Long & Kam Tin (Lower) Subzone and other inland waters
M. Toxins	(a) Waste discharges shall not cause the toxins in water to attain such levels as to produce significant toxic carcinogenic, mutagenic or teratogenic effects in humans, fish or any other aquatic organisms, with due regard to biologically cumulative effects in food chains and to toxicant interactions with each other.	Whole Zone
	(b) Waste discharges shall not cause a risk to any beneficial uses of the aquatic environment.	
N. Phenol	It shall not be present in such quantities as to produce a specific odour, or in concentration greater than 0.05 milligrams per litre as C_6H_5OH .	Yung Long Bathing Beach Subzone
O. Turbidity	Waste discharges shall not reduce light transmission substantially from the normal level.	Yung Long Bathing Beach Subzone