Section 12A Rezoning Application - Request for Amendment to the approved Lung Yeuk Tau and Kwan Tei South Outline Zoning Plan No. S/NE-LYT/19 from "Residential (Group C)" Zone and "Agriculture" Zone to "Residential (Group A) 2" Zone at Various Lots in D.D. 83 and Adjoining Government Land, Lung Yeuk Tau, New Territories Ref.: ADCL/PLG-10248/R001a

Appendix 3

Traffic Impact Assessment

> Traffic Impact Assessment Final Report

> > 15<sup>th</sup> December 2022

Prepared by: CKM Asia Limited Prepared for: Carlton Woodcraft Manufacturing Limited c/o Aikon Development Consultancy Limited

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## 1.0 INTRODUCTION

### Background

- The Subject Site is located at Various Lots, i.e. Lot Nos. 755, 756, 782 S.A, 789 S.A, 789 RP, 790 S.A ss.1, 790 S.A RP, 791 S.A ss.1, 791 S.A ss.2, 791 S.A ss.3, 791 S.A RP, 791 RP, 792 S.A RP, 792 RP, 793, 794 S.A, 794 RP, 800 S.A RP, 801 S.A, 803 RP, 835 S.B ss.1 S.A, 835 S.B ss.1 RP, 836 S.A, 836 RP, 837, 838 S.A, 838 RP, 839, 840, 841 S.A, 841 S.B, 841 RP, 842 S.A, 842 S.B, 842 RP, 843, 844 S.A, 844 RP and 854 in D.D. 83 and Adjoining Government Land, in Lung Yeuk Tau, Fanling, New Territories. Figure 1.1 shows the location of the Subject Site.
- 1.2 At present, the Subject Site is occupied by several open storages, which are accessed from either Sha Tau Kok Road Lung Yeuk Tau or Hai Wing Road / Dao Yang Road.
- 1.3 The Owner of the Subject Site intends to develop the Subject Site into a development with 5 residential blocks comprising 3,305 flats, and 5,570 m<sup>2</sup> retail GFA (hereinafter "the Proposed Development").
- 1.4 Against this background, CKM Asia Limited, a traffic and transportation planning consultancy firm, was commissioned to conduct a Traffic Impact Assessment ("TIA") for the Proposed Development for the Section 12A Rezoning Application from "Residential (Group C)" zone and "Agriculture" zone to "Residential (Group A)2". This report presents the findings of the TIA for the Proposed Development.

### Structure of Report

- 1.5 The report is structured as follows:
  - Chapter 1 Gives the background of the project;
  - Chapter 2 Describes the existing situation;
  - Chapter 3 Provides details on the Proposed Development, and presents the proposed provision of internal transport facilities;
  - Chapter 4 Describes the traffic impact analysis; and
  - Chapter 5 Gives the overall conclusion.

# 2.0 EXISTING SITUATION

### The Subject Site

2.1 The Subject Site is located in Ma Liu Shui San Tsuen, Lung Yeuk Tau in Fanling, New Territories. Its site area is approximately 22,500m<sup>2</sup>, and is now being occupied by several open storage areas. Access to the Subject Site is from either Sha Tau Kok Road – Lung Yeuk Tau, or Dao Yang Road / Hai Wing Road.

### Public Transport Services

2.2 At present, the Subject Site is served by franchised bus and green minibus ("GMB"), and the details are presented in Table 2.1 and Figure 2.1.

| TABLE 2.1 | ROAD-BASED                | PUBLIC | TRANSPORT | SERVICES | OPERATING |  |  |
|-----------|---------------------------|--------|-----------|----------|-----------|--|--|
| _         | CLOSE TO THE SUBJECT SITE |        |           |          |           |  |  |

| Route     | Routing   | Frequency (minutes)            |
|-----------|---|--------------------------------|
| KMB 78A   | Queen's Hill ↔ Fanling Station (Circular)                     | 6 - 30                         |
| KMB 78K   | Sheung Shui (Tai Ping) ↔ Sha Tau Kok                          | 15 - 20                        |
| KMB 79K   | Sheung Shui ↔ Ta Kwu Ling (Tsung Yuen Ha)                     | 20 - 30                        |
| KMB 277A  | Sha Tau Kok → Lam Tin Station                                 | 60 <sup>(1)</sup>              |
|           | Lam Tin Station $\rightarrow$ Sha Tau Kok                     | 60 <sup>(2)</sup>              |
| KMB 278A  | Queen's Hill ↔ Tsuen Wan (Nina Tower)                         | 20 - 30                        |
| KMB N78   | Sheung Shui → Sha Tau Kok                                     | 2 trips per day <sup>(3)</sup> |
|           | Sha Tau Kok → Sheung Shui                                     | 2 trips per day <sup>(3)</sup> |
| CTB 78X   | Queen's Hill Estate ↔ Kai Tak                                 | 30 - 60                        |
| CTB 79X   | Queen's Hill Estate ↔ Cheung Sha Wan (West)                   | 30 - 40                        |
| CTB 679   | Queen's Hill Estate →Central (Hong Kong Station)              | 2 per AM <sup>(1)</sup>        |
|           | Central (Hong Kong Station) → Queen's Hill Estate             | 1 per PM <sup>(2)</sup>        |
| CTB 979   | Queen's Hill Estate $\rightarrow$ Central (Hong Kong Station) | 1 per AM <sup>(1)</sup>        |
|           | Central (Hong Kong Station) $\rightarrow$ Queen's Hill Estate | 1 per PM <sup>(2)</sup>        |
| GMB 52K   | Fanling Station ↔ Ping Che                                    | 4 - 10                         |
| GMB 503   | Queen's Hill ↔ North District Hospital                        | 10 - 20                        |
| GMB 503k  | Queen's Hill ↔ Sheung Shui Station                            | 8 - 15                         |
| Note: KMB | – Kowloon Motor Bus CTB – Citybus                             | GMB – Green Minibus            |

In the image: Note:KMB – Kowloon Motor BusCTB – CitybusGMB – Green Minibus(1) AM Peak hour service only(2) PM Peak hour service only(3) Overnight service only

### The Road Network

- 2.3 Sha Tau Kok Road Lung Yeuk Tau is a Rural Road which runs between San Wan Road, Fanling in the west and Ping Che Road in the east. East of Ping Che Road, Sha Tau Kok Road continues towards Sha Tau Kok and the Sha Tau Kok Boundary Control Point. The Sha Tau Kok Interchange with Heung Yuen Wai Highway is located 3km to the east. In the vicinity of the Subject Site between Lau Shui Heung Road and Jockey Club Road, Sha Tau Kok Road Lung Yeuk Tau is of dual-2 carriageway standard.
- 2.4 **Jockey Club Road** is a Primary Distributor running between Man Kam To Road to the north and Pak Wo Road to the south, where it connects with the Wo Hop Shek Interchange of Fanling Highway. It is of a dual-2 carriageway standard.
- 2.5 **So Kwun Po Road** is a Primary Distributor running between Pak Wo Road and Jockey Club Road. It connects with Fanling Highway via the So Kwun Po Interchange. So Kwun Po Road is generally of a dual-2/3 carriageway standard. To the east of Jockey Club Road, it continues as **Ma Sik Road** towards Luen Wo Hui and intersects with Sha Tau Kok Road Lung Yeuk Tau.

### Pedestrian and Cycling Facilities

- 2.6 Footpaths and at-grade signalized pedestrian crossings are provided along Sha Tau Kok Road – Lung Yeuk Tau in the vicinity of the Subject Site. A footbridge is also provided at the Sha Tau Kok Road / Lung Ma Road Roundabout.
- 2.7 Cycle track is provided along the south side of Sha Tau Kok Road Lung Yeuk Tau, i.e. westbound side towards Fanling.

### **Existing Traffic Flows**

- 2.8 To quantify the existing traffic flows in the vicinity, manual classified counts were conducted on weekdays, i.e. Monday, 18<sup>th</sup> July 2022 and Tuesday, 19<sup>th</sup> July 2022, during the AM and PM peak periods at the following junctions:
  - J01 Junction of Sha Tau Kok Road / Lau Shui Heung Road
  - J02 Junction of Sha Tau Kok Road / Lung Ma Road
  - J03 Junction of Sha Tau Kok Road / Ma Sik Road
  - J04 Junction of Sha Tau Kok Road / Jockey Club Road
  - J05 Junction of So Kwun Po Road / Jockey Club Road / Ma Sik Road
  - J06 Roundabout of So Kwun Po Interchange
- 2.9 Figure 2.2 shows the locations of the surveyed junctions, and Figures 2.3 2.8 show their existing layouts.
- 2.10 The traffic counts are classified by vehicle type to enable traffic flows in passenger car units ("pcu") to be calculated. The AM and PM peak hours identified from the surveys are found to be between 0745 0845 and 1730 1830 hours respectively, and the traffic flows in are shown in Figure 2.9.

### Potential Influence on Traffic Flow due to COVID-19 Pandemic

2.11 To determine if the observed peak hour traffic flows obtained in July 2022 are representative and not affected by the COVID-19 pandemic, reference is made to the 2019 observed peak hour traffic flows obtained from CKM's in-house database. Table 2.2 summarises and compares the 2019 and 2022 peak hour traffic flow.

| Section                          | Observed 2-way Traffic Flow (pcu/hour)   |  |  | cu/hour)  |
|----------------------------------|--|--|--|---|
|                                  | AM Pea   | ak Hour  | PM Pe  | ak Hou  |
|                                  | 2019   | 2022   | 2019   | 2022  |
| Between Fan Leng Lau Road / Lok  | 1,711 <sup>(2)</sup>   | 1,915 <sup>(1)</sup>   | 1,655 <sup>(2)</sup>   | 1,857 <sup>(1)</sup>  |
| Yip Road and Ma Sik Road / On    |  |  |  |   |
| Kui Street                       |  |  |  |   |
| Between Ma Sik Road and Sha Tau  | 1,260  | 1,100  | 766  | 941   |
| Kok Road – Lung Yeuk Tau         |  |  |  |   |
| Between Po Shek Wu Interchange   | 2,825  | 2,745  | 2,500  | 2,529   |
| and Jockey Club Road             |  | ,  | ,  | *   |
| TOTAL                            | 5,796  | 5,760  | 4,921  | 5,327   |
| % Difference between 2019 & 2022 | -0.6%  |  | +8.3%  |   |
|                                  | Between Fan Leng Lau Road / Lok<br>Yip Road and Ma Sik Road / On<br>Kui Street<br>Between Ma Sik Road and Sha Tau<br>Kok Road – Lung Yeuk Tau<br>Between Po Shek Wu Interchange<br>and Jockey Club Road<br>TOTAL | AM Pea<br>2019 Between Fan Leng Lau Road / Lok<br>Yip Road and Ma Sik Road / On<br>Kui Street Between Ma Sik Road and Sha Tau<br>Kok Road – Lung Yeuk Tau Between Po Shek Wu Interchange<br>and Jockey Club Road TOTAL 5,796 | AM Peak Hour20192022Between Fan Leng Lau Road / Lok<br>Yip Road and Ma Sik Road / On<br>Kui Street1,711 <sup>(2)</sup> 1,915 <sup>(1)</sup> Between Ma Sik Road and Sha Tau<br>Kok Road – Lung Yeuk Tau1,2601,100Between Po Shek Wu Interchange<br>and Jockey Club Road2,8252,745TOTAL5,7965,760 | AM Peak HourPM Pea201920222019Between Fan Leng Lau Road / Lok<br>Yip Road and Ma Sik Road / On<br>Kui Street1,7111,9151,6551Between Ma Sik Road and Sha Tau<br>Kok Road – Lung Yeuk Tau1,2601,100766Between Po Shek Wu Interchange<br>and Jockey Club Road2,8252,7452,500TOTAL5,7965,7604,921 |

TABLE 2.2 COMPARISON OF PEAK HOUR TRAFFIC FLOWS

Note:

(1) With On Kui Street between On Chuen Street and Sha Tau Kok Road – Lung Yeuk Tau temporarily closed to facilitate construction of the Fanling Bypass Eastern Section.

<sup>(2)</sup> Adjusted to include additional traffic flow of On Kui Street for comparison purpose.

2.12 As shown in Table 2.2, the 2022 observed AM peak hour traffic flow is only 0.6% less than the 2019 AM peak hour traffic flow, which is negligible, and is 8.3% higher for the PM peak hour; hence, the 2022 observed peak hour traffic flow is representable, and no adjustment was necessary.

### Performance of the Surveyed Junctions

2.13 The existing performance of the surveyed junctions is calculated based on the observed traffic flows, and the analyses were undertaken using the methods outlined in Volume 2 of Transport Planning and Design Manual ("TPDM"). Table 2.3 summarises the analysis results and the detailed calculations are found in Appendix A.

| Ref. | Junction  | Type of<br>Junction | Parameter | AM Peak<br>Hour | PM Peak<br>Hour |
|------|---|---------------------|-----------|-----------------|-----------------|
| J01  | Sha Tau Kok Road / Lau Shui Heung Road              | Roundabout          | RFC       | 0.379           | 0.414           |
| J02  | Sha Tau Kok Road / Lung Ma Road                     | Roundabout          | RFC       | 0.481           | 0.54            |
| J03  | Sha Tau Kok Road / Ma Sik Road                      | Signal              | RC        | 75%             | 64%             |
| J04  | Sha Tau Kok Road / Jockey Club Road                 | Roundabout          | RFC       | 0.5148          | 0.4608          |
| J05  | So Kwun Po Road / Jockey Club Road / Ma<br>Sik Road | Signal              | RC        | 33%             | 46%             |
| J06  | So Kwun Po Interchange                              | Roundabout          | RFC       | 0.8485          | 0.8491          |

### TABLE 2.3EXISTING JUNCTION PERFORMANCE

Note: RFC - Ratio of Flow to Capacity RC – Reserve Capacity

2.14 The above results indicate the surveyed junctions operate with capacities.

### Performance of the Surveyed Road Links

2.15 The existing performance, in terms of Peak Hourly Flows / Design Flow Ratio ("P/Df") of the surveyed road links is calculated based on the observed traffic flows, and the analyses were undertaken based on the design flow of different road type outlined in Volume 2 of the TPDM. Details of the surveyed road links and the analysis results are summarized in Table 2.4.

| Ref. | Road<br>Link        | Sec<br>From            | tion<br>To             | Type<br>(Note 1) | Config-<br>uration. | Design<br>Flow<br>(vph) | Adjusted<br>Design<br>Flow | Peak Hou<br>Design Fl<br>(P/I | ow Ratio           |
|------|---------------------|------------------------|------------------------|------------------|---------------------|-------------------------|----------------------------|-------------------------------|--------------------|
|      |                     |                        |                        |                  |                     |                         | (vph)<br>(Note 2)          | AM<br>Peak<br>Hour            | PM<br>Peak<br>Hour |
| L01  | Sha Tau<br>Kok Road | Lung Ma<br>Road        | Lau Shui<br>Heung Road | RR               | Dual-2              | 2,800                   | 2,520                      | 0.3566                        | 0.3863             |
| L02  | Sha Tau<br>Kok Road | Lau Shui<br>Heung Road | Lung Ma<br>Road        | RR               | Dual-2              | 2,800                   | 2,520                      | 0.3957                        | 0.4454             |
| L03  | Sha Tau<br>Kok Road | Ma Sik Road            | Lung Ma<br>Road        | RR               | Dual-2              | 2,800                   | 2,520                      | 0.5390                        | 0.5138             |
| L04  | Sha Tau<br>Kok Road | Lung Ma<br>Road        | Ma Sik Road            | RR               | Dual-2              | 2,800                   | 2,520                      | 0.5253                        | 0.6282             |
| L05  | Sha Tau<br>Kok Road | Jockey Club<br>Road    | Ma Sik Road            | RR               | Dual-2              | 2,800                   | 2,520                      | 0.5324                        | 0.5599             |

TABLE 2.4EXISTING P/Df OF SURVEYED ROAD LINKS

Note 1: RR – Rural Road DD – District Distributor PD – Primary Distributor

Note 2: Reduced design flow by 10% due to percentage of heavy vehicles exceeds 20%

| Ref. | Road                |                                     | tion                                | Type       | Config. | Design        | Adjusted          | Peak Hou           |                    |
|------|---------------------|-------------------------------------|-------------------------------------|------------|---------|---------------|-------------------|--------------------|--------------------|
|      | Link                | From                                | То                                  | (Note 1)   |         | Flow<br>(vph) | Design<br>Flow    | Design Fl<br>(P/I  |                    |
|      |                     |                                     |                                     |            |         |               | (vph)<br>(Note 2) | AM<br>Peak<br>Hour | PM<br>Peak<br>Hour |
| L06  | Sha Tau<br>Kok Road | Ma Sik Road                         | Jockey Club<br>Road                 | RR         | Dual-2  | 2,800         | 2,520             | 0.4674             | 0.4128             |
| L07  | Ma Sik<br>Road      | Jockey Club<br>Road                 | Sha Tau Kok<br>Road                 | DD         | Dual-2  | 2,000         | 1,800             | 0.6161             | 0.5934             |
| L08  | Ma Sik<br>Road      | Sha Tau Kok<br>Road                 | Jockey Club<br>Road                 | DD         | Dual-2  | 2,000         | 1,800             | 0.5753             | 0.4838             |
| L09  | Jockey Club<br>Road | Ma Sik Road /<br>So Kwun Po<br>Road | Sha Tau Kok<br>Road                 | PD         | Dual-2  | 2,800         | 2,520             | 0.2095             | 0.1836             |
| L10  | Jockey Club<br>Road | Sha Tau Kok<br>Road                 | Ma Sik Road /<br>So Kwun Po<br>Road | PD         | Dual-2  | 2,800         | 2,520             | 0.2268             | 0.1893             |
| L11  | So Kwun<br>Po Road  | Jockey Club<br>Road                 | So Kwun Po<br>Interchange           | PD         | Dual-2  | 2,800         | 2,520             | 0.4960             | 0.3993             |
| L12  | So Kwun<br>Po Road  | So Kwun Po<br>Interchange           | Jockey Club<br>Road                 | PD         | Dual-2  | 2,800         | 2,520             | 0.5928             | 0.6041             |
| Note | 1: RR – Rura        | l Road                              | DD – Distri                         | ct Distril | outor   |               | PD – Prima        | ry Distributor     |                    |

| TABLE 2.4 | EXISTING P/Df OF SURVEYED ROAD LINKS (CONT'D) |
|-----------|---|
|-----------|---|

Note 2: Reduced design flow by 10% due to percentage of heavy vehicles exceeds 20%

2.16 The above results indicate the surveyed road links operate with capacities.

### Historic Traffic Growth

2.17 The annual average daily traffic ("AADT") of roads located in the vicinity of the Subject Site was obtained from the Annual Traffic Census ("ATC") published by Transport Department, and Table 2.5 summarises the AADT between 2015 and 2021, i.e. the latest 7 years.

|  | TABLE 2.5 | HISTORIC TRAFFIC INFORMATION FROM THE ATC |
|--|-----------|---|
|--|-----------|---|

| Station                                      | 5453    | 5824      | 5622       | 5623         | 5660         | 5860     | Overall |
|--|---------|-----------|------------|--------------|--------------|----------|---------|
| Road   |         |           |            | Kok Road     |              |          |         |
| From   | Jockey  | Jockey    | Lok Yip    | Luen         | On Kui       | Ping Che |         |
|  | Club    | Club Road | Road       | Shing        | Street       | Road     |         |
|  | Road    |           |            | Street       |              |          |         |
| То   | San Wan | Lok Yip   | Luen       | On Kui       | Ping Che     | Shun     |         |
|  | Road    | Road      | Shing St   | Street       | Road         | Lung     |         |
|  |         |           |            |              |              | Street   |         |
| Year   |         | A٧        | erage Annu | al Daily Tra | ffic ("AADT' | ")       |         |
| 2015   | 18,750  | 29,240*   | 17,300*    | 17,780       | 30,380       | 6,320*   | 113,450 |
| 2016   | 19,530* | 29,270    | 21,540     | 20,840       | 33,580       | 6,550    | 124,760 |
| 2017   | 19,230* | 27,180    | 21,390*    | 20,700*      | 33,050*      | 6,460    | 121,550 |
| 2018   | 19,700* | 28,050*   | 22,070*    | 21,350*      | 33,870*      | 6,620    | 125,040 |
| 2019   | 20,320  | 29,170*   | 22,950*    | 22,200       | 33,630*      | 6,570*   | 128,270 |
| 2020   | 17,680  | 27,760*   | 18,260     | 17,080       | 23,740       | 6,300*   | 104,520 |
| 2021   | 18,380* | 30,230    | 19,410     | 18,530       | 22,980       | 5,970    | 109,530 |
| Average<br>Annual<br>Growth<br>(2015 – 2019) | 2.0%    | -0.1%     | 7.3%       | 5.7%         | 2.6%         | 3.1%     | 3.1%    |

Note: \* - Estimated by Growth Factor

- 2.18 It should be noted that "*The Annual Traffic Census 2020*" and "*The Annual Traffic Census 2021*" stated that due to the outbreak of COVID-19 in 2020 and 2021, normal traffic flow pattern across Hong Kong were affected with reduction in traffic flows in view of work-from-home arrangement for many offices, suspension of face-to-face classes for schools, and disruption of tourism, etc. Hence, the 2020 and 2021 traffic data were not adopted to determine the average annual growth, but included in Table 2.5 for reference only.
- 2.19 Table 2.5 shows that the traffic growth in the vicinity of the Subject Site is some 0.1% to 7.3% per annum, and overall annual growth of 3.1% per annum between 2015 and 2019.

# 3.0 THE PROPOSED DEVELOPMENT

### Proposed Development

3.1 Table 3.1 summarises the parameters of the Proposed Development.

| TABLE 3.1 | PARAMETERS OF THE PROPOSED DEVELOPMENT |
|-----------|--|
| INDLE J.I |  |

| Use         | Development Parameters  |                   |   |                          |  |  |  |  |  |
|-------------|---|-------------------|---|--------------------------|--|--|--|--|--|
| Residential | Domestic Plot Ratio:<br>Number of blocks:<br>Total number of flats: | 6.5<br>5<br>3,305 | $\frac{\text{Flat Mix:}}{\text{GFA} \le 40\text{m}^2}$ $40\text{m}^2 < \text{GFA} \le 70\text{m}^2$ | 2,991 units<br>314 units |  |  |  |  |  |
| Retail      | 5,570 m <sup>2</sup> GFA  |                   |   |                          |  |  |  |  |  |

### Proposed Internal Transport Facilities

### Provision of Internal Transport Facilities for the Residential Flats

3.2 The internal transport facilities for the residential flats are provided based on the recommendation of the Hong Kong Planning Standards and Guidelines ("HKPSG"). Table 3.2 compares the the HKPSG recommendation and the proposed provision.

# TABLE 3.2COMPARISON OF INTERNAL TRANSPORT FACILITIES FOR<br/>RESIDENTIAL USE

|     | HKPSG Recommendation   | Proposed Provision |
|-----|--|--------------------|
|     | Private Car Parking Spaces   |                    |
| (i) | Residential:   | 422 nos.           |
|     | Parking Requirement = GPS x R1 x R2 x R3   |                    |
|     |  | (=HKPSG Max., OK)  |
|     | Global Parking Standard (GPS):   |                    |
|     | Min: 1 space per 7 flats   |                    |
|     | Max: 1 space per 4 flats   |                    |
|     | Demand Adjustment Ratio (R1):  |                    |
|     | • Flat Size $< 40m^2$ = 0.5  |                    |
|     | • $40 < Flat Size \le 70 m^2 = 1.2$  |                    |
|     | Accessibility Adjustment Ratio (R2):   |                    |
|     | • Outside a 500m-radius of rail station = 1.0  |                    |
|     | Development Intensity Adjustment Ratio (R3)<br>• 5.0 < Domestic Plot Ratio ≤ 8.0 = 0.9 |                    |
|     | For Flat Size < 40m <sup>2</sup> (2,991 flats)   |                    |
|     | Min: $(2,991 / 7 \times 0.5 \times 1.0 \times 0.9) = 192.3$ , say 193 nos.             |                    |
|     | Max: $(2,991 / 4 \times 0.5 \times 1.0 \times 0.9) = 336.5$ , say 337 nos.             |                    |
|     | For 40 < Flat Size $\leq$ 70 m <sup>2</sup> : (314 flats)                              |                    |
|     | Min: $(314 / 7 \times 1.2 \times 1.0 \times 0.9) = 48.4$ , say 49 nos.                 |                    |
|     | Max: $(314 / 4 \times 1.2 \times 1.0 \times 0.9) = 84.8$ , say 85 nos.                 |                    |
|     | Overall  |                    |
|     | $\overline{\text{Min:}}  193 + 49 = 242 \text{ nos.}$                                  |                    |
|     | Max: 337 + 85 = <b>422 nos.</b>  |                    |
|     | •  | •                  |

# TABLE 3.2COMPARISON OF PROVISION ON INTERNAL TRANSPORT<br/>FACILITIES FOR RESIDENTIAL USE (CONT'D)

|       | HKPSG Recommendation  | Proposed Provision   |  |  |  |  |  |
|-------|---|--|--|--|--|--|--|
|       | Private Car Parking Spaces  |  |  |  |  |  |  |
| (ii)  | Visitor Car Parking Spaces  | 25 nos.  |  |  |  |  |  |
|       | <ul> <li>1 - 5 no. per residential block with more than 75 units, or as determined by the Authority</li> <li>At least 1 no. visitor car parking space shall be accessible peaking space.</li> </ul> | <u>(=HKPSG Max., OK)</u>   |  |  |  |  |  |
|       | For 5 blocks with 3,305 flats:  |  |  |  |  |  |  |
|       | $\begin{array}{rcl} \text{Min:} & 1 \times 5 = 5 \text{ nos.} \\ \text{Max:} & 5 \times 5 = \textbf{25 nos.} \end{array}$   |  |  |  |  |  |  |
| (iii) | (i) + (ii)<br>Min: $242 + 5 = 247 \text{ nos.},$<br>(including 242 nos. regular and 4 nos. accessible)  | <b>447 nos.,</b> including:<br>- 442 nos. regular , and<br>- 5 nos. accessible |  |  |  |  |  |
|       | (including 243 nos. regular, and 4 nos. accessible)<br>Max: 422 + 25 = 447 nos.,<br>(including 441 nos. regular, and 5 nos. accessible)   | <u>(=HKPSG Max., OK)</u>   |  |  |  |  |  |
|       | Motorcycle Parking Spaces   |  |  |  |  |  |  |
| (iv)  | At the rate of 1 motorcycle parking space per 100 - 150 flats   | 34 nos.  |  |  |  |  |  |
|       | Min: 3,305 / 150 = 22.03, say 23 nos.<br>Max: 3,305 / 100 = 33.05, say 34 nos.  | <u>(=НКРЅG Max., ОК)</u>   |  |  |  |  |  |
|       | Goods Vehicle Loading / Unloading ("L/UL  | ″) Bay   |  |  |  |  |  |
| (v)   | 1 bay per residential block   | 5 nos. HGV   |  |  |  |  |  |
|       | For 5 residential blocks: $5 \times 1 = 5$ nos.   | <u>(=НКРSG, ОК)</u>  |  |  |  |  |  |
|       | Bicycle Parking Spaces  |  |  |  |  |  |  |
| (vi)  | At the rate of 1 cycle parking space for every 30 flats smaller than 70m <sup>2</sup> GFA for outside 2km radius of a rail station.   | 111 nos.<br>( <u>=HKPSG, OK)</u>   |  |  |  |  |  |
|       | 3,305 / 30 = 110.2, says 111 nos.@ 1.65m (L) x 0.8m (W) or provided with parking racks.   |  |  |  |  |  |  |

Provision of Internal Transport Facilities for Retail

3.4 The internal transport facilities for the retail use are provided based on the recommendation of the HKPSG, and Table 3.3 compares the HKPSG recommendation and the proposed provision.

| TABLE 3.3 | PROPOSED PROVISION OF INTERNAL TRANSPORT FACILITIES |
|-----------|---|
|           | FOR RETAIL  |

|        | HKPSG Reco                  | Proposed Provision        |                        |
|--------|-----------------------------|---------------------------|------------------------|
|        |                             | Private Car Parking Space | es                     |
| (vii)  | For 5,570m <sup>2</sup> GFA |                           | 38 nos., including:    |
|        | Min.: 5,570 / 300           | = 18.6, say 19 nos.       | - 37 nos. regular, and |
|        | Max.: 5,570 / 150           | = 37.1, say 38 nos.       | - 1 no. accessible     |
|        |                             |                           | (=HKPSG Max., OK)      |
|        |                             | Motorcycle Parking Space  | es                     |
| (viii) | At 5% to 10% of car pa      | arking spaces provided    | 4 nos.                 |
|        | Min.: 19 x 5%               | = 1.0, say 1 nos.         |                        |
|        | Max.: 38 x 10%              | = 3.8, say 4 nos.         | (=HKPSG Max., OK)      |

# TABLE 3.3PROPOSED PROVISION OF INTERNAL TRANSPORT FACILITIES<br/>FOR RETAIL

|      | HKPSG Recommendation                          | Proposed Provision |
|------|---|--------------------|
|      | Goods Vehicle Loading / Unloading             | ; ("L/UL") Bay     |
| (ix) | 1 L/UL bay per 800 – 1,200 m <sup>2</sup> GFA | 7 nos., including: |
|      | 65% LGV and 35% HGV                           | - 3 nos. HGV, and  |
|      |   | - 4 nos. LGV       |
|      | For 5,570 m <sup>2</sup> GFA:                 |                    |
|      | Min.: 5,570 / 1,200 = 4.68, say 5 nos.        | (=HKPSG Max., OK)  |
|      | HGV: $5 \times 35\% = 1.75$ , say 2 nos.      |                    |
|      | LGV: $5 - 2 = 3$ nos.                         |                    |
|      |   |                    |
|      | Max.: $5,570 / 800 = 6.96$ , say 7 nos.       |                    |
|      | HGV: $7 \times 35\% = 2.45$ , say 3 nos.      |                    |
|      | LGV: $7 - 3 = 4$ nos.                         |                    |
|      |   |                    |

Overall Provision of Internal Transport

3.5 Table 3.4 summarises the overall provision of internal transport, which meets the high-end recommendation of the HKPSG.

| TABLE 3.4 | OVERALL PROVISION OF INTERNAL TRANSPORT FACILITIES |
|-----------|--|
|           |  |

| Туре  | Proposed Provision |        |     |     |
|---|--------------------|--------|-----|-----|
|   | Residential        | Retail | Tot | tal |
| Car Parking Space                           | 442                | 37     | 479 |     |
| @ 5.0m (L) x 2.5m (W) x 2.4m (H)            |                    |        |     | 485 |
| Accessible Car Parking Space                | 5                  | 1      | 6   | 405 |
| @ 5.0m (L) x 2.5m (W) x 2.4m (H)            |                    |        |     |     |
| Motorcycle Parking Space                    | 34                 | 4      | 38  | 8   |
| @ 2.4m (L) x 2.5m (W) x 2.4m (H)            |                    |        |     |     |
| LGV Loading / Unloading Bay                 | -                  | 4      | 4   |     |
| @ 11.0m (L) x 3.5m (W) x 4.7m (H)           |                    |        |     |     |
| HGV Loading / Unloading Bay                 | 5                  | 3      | 8   |     |
| @ 11.0m (L) x 3.5m (W) x 4.7m (H)           |                    |        |     |     |
| Bicycle Parking Space                       | 111                | -      | 11  | 1   |
| @ 1.65m (L) x 0.8m (W) or with parking rack |                    |        |     |     |

## 4.0 TRAFFIC IMPACT

### Design Year

4.1 The Proposed Development is anticipated to be completed no later than 2031. Hence, the design year adopted is 2034, i.e. 3 years after completion.

### Traffic Generation of the Proposed Development

4.2 To estimate the traffic generation associated with the Proposed Development, the TPDM trip rates are adopted, and are summarized in Table 4.1.

### TABLE 4.1TRIP RATES ADOPTED FROM THE TPDM

| ltem  | AM Peak Hour |            | PM Peak Hour |            |
|---|--------------|------------|--------------|------------|
|   | Generation   | Attraction | Generation   | Attraction |
| Private Housing: High-Density / R(A)<br>60 m <sup>2</sup> GFA (pcu/hour/flat) | 0.0718       | 0.0425     | 0.0286       | 0.037      |
| Retail (pcu/100m <sup>2</sup> GFA/hour)                                       | 0.2296       | 0.2434     | 0.3100       | 0.3563     |

4.3 Table 4.2 presents the traffic generation for the Proposed Development.

| ltem                             |       | AM Peak Hour (pcu/hour) |            | PM Peak Hour (pcu/hour) |            |  |
|----------------------------------|-------|-------------------------|------------|-------------------------|------------|--|
|                                  | ſ     | Generation              | Attraction | Generation              | Attraction |  |
| Residential (3,305 flats)        |       | 238                     | 141        | 95                      | 123        |  |
| Retail (5,570m <sup>2</sup> GFA) |       | 13                      | 14         | 18                      | 20         |  |
|                                  | TOTAL | 251                     | 155        | 113                     | 143        |  |
|                                  | -     | 406 (2-Way)             |            | 256 (2-Way)             |            |  |

4.4 Table 4.2 shows that the Proposed Development is expected to generate some 406 and 256 pcu (2-way) during the AM and PM peak hours respectively.

### Traffic Forecasting

- 4.5 Year 2034 traffic flows used for the capacity analysis are derived as follows: (i) with reference to the 2026 traffic flows from the NTE1 Base District Traffic Model ("BDTM") which is produced by Transport Department, (ii) the estimated traffic growths from 2026 to 2034, (iii) the expected traffic generation associated with other known planned / committed major developments, (iv) the planned traffic improvement works to be carried by other projects, and (v) the expected traffic generation associated to the Proposed Development
- 4.6 The traffic growth from 2026 to 2034 are calculated using the following equations, with X<sub>1</sub> being the annual population growth obtained from the "2014based Territorial Population and Employment Data Matrix" published by Planning Department rates for 2026 – 2034.

### 2026 to 2034 traffic growth factor = $(1 + X_1)^5$

4.7 The total growths were applied to the trips ends of the 2026 NTE1 BDTM model to develop the 2034 traffic model for producing the 2034 traffic flows.

## Other Known Planned / Committed Major Developments in the Vicinity

4.8 Traffic generations associated with the other known planned / committed major developments located in the vicinity summarised in Table 4.3 were considered and included in the 2034 traffic forecast. The locations of these other developments are shown in Figure 4.1.

TABLE 4.3LIST OF OTHER KNOWN PLANNED / COMMITTED MAJOR<br/>DEVELOPMENTS

| Ref. | Developments   | Development Parame  |   |
|------|--|---|---|
| А.   | Fanling North New Development Area<br>(including Proposed Minor Relaxation of<br>Plot Ratio and Building Height approved<br>under TPB No. A/KTN/54, A/FLN/28, &<br>A/FLN/30) <sup>(1)</sup>                | Private Housing: 8<br>G/IC: 3<br>Other non-domestic use (e  | 29,657 m <sup>2</sup> GFA   |
| В.   | Private Residential Development at<br>Sheung Shui Town Lot 262,8 Ma Sik<br>Road, Fanling, (namely "One Innovale") <sup>(2)</sup>   | Private Housing: 1  | ,576 flats  |
| C.   | Proposed Public Housing Development at Queen's Hill Extension <sup>(3)</sup>   | G/IC  | ,000 flats  |
| D.   | New Territories East Cultural Centre in<br>Area 11, Sha Tau Kok Road – Lung Yeuk<br>Tau, Fanling <sup>(4)</sup>  | 67,000 m <sup>2</sup> CFA with 2,500<br>Public Vehicle Park |   |
| E.   | Public Housing Development at San Wan<br>Road <sup>(5)</sup>   | G/IC, Kindergarten, Primai<br>Secondary School              |   |
| F.   | Mixed Housing Development Project at<br>Pak Wo Road (TPB No. A/FSS/254) <sup>(6) (9)</sup>   | Subsidized Sale Flat:6Elderly Housing:2RCHE:2               | 510 flats<br>596 flats<br>261 flats<br>210 beds<br>5,500 m <sup>2</sup> GFA |
| G.   | Redevelopment of Junior Police Officers<br>Married Quarters, Fan Garden, Fanling <sup>(7)</sup>  |   | ,184 flats  |
| H.   | Subsidized Sale Flats at Jockey Club Road  |   | 644 flats<br>8,000 m² CFA   |
| I.   | Public Housing Development at Sheung<br>Shui Areas 4 and 30 Site 1 & 2 (including<br>Proposed Minor Relaxation of Plot Ratio<br>and Building Height approved under TPB<br>No. A/FSS/280) <sup>(B)(9)</sup> | Public Housing: 3   | 8,644 flats<br>,100 m <sup>2</sup> CFA                                      |
| J.   | Public Housing Development at Po Shek<br>Wu Road <sup>(8)</sup>  |   | ,800 flats<br>3,000 m <sup>2</sup> CFA                                      |
| K.   | Proposed House and Social Welfare<br>Facility (Residential Care Home for the<br>Elderly) at Ma Sik Road, Fanling (TPB No.<br>A/FSS/276) <sup>(9)</sup>   | RCHE: 60 beds <sup>(9)</sup>                                | i0 houses   |
| L.   | Proposed Social Welfare Facility<br>(Residential Care Home for the Elderly)<br>and Flat at Tin Ping Road, Sheung Shui<br>(TPB No. A/FSS/279) <sup>(9)</sup>  | RCHE: 143 beds<br>Private Housing: 2                        | 28 flats  |

# TABLE 4.3LIST OF OTHER KNOWN PLANNED / COMMITTED MAJOR<br/>DEVELOPMENTS (CONT'D)

| Ref. | Developments   | Development Parameters (Approx.)                                 |  |  |
|------|--|--|--|--|
| M.   | Proposed Minor Relaxation of Domestic<br>PR Restriction for Permitted Residential<br>Development with Commercial Uses at<br>1 Luen Fat Street, Fanling (TPB No.<br>A/FSS/282) <sup>(9)</sup> | Private Housing: 119 flats<br>Commercial: 161 m <sup>2</sup> GFA |  |  |
| N.   | Proposed Shop and Services<br>(Showroom) and Office (Wholesale<br>Conversion of an Existing Industrial<br>Building) at 5 Lok Yip Road, Fanling<br>(TPB No. A/FSS/283) <sup>(9)</sup>         | Retail: 4,075 m <sup>2</sup> GFA                                 |  |  |
| О.   | Proposed Shop and Services, Eating<br>Place and Other Uses at 33 On Lok Mun<br>Street, Fanling (TPB No. A/FSS/284) <sup>(9)</sup>  | Retail: 2,392 m <sup>2</sup> GFA                                 |  |  |

Source:

(1) Rural and New Town Planning Committee ("RNTPC") Paper No. A/FLN/30

(2) One Innovale. < http://www.oneinnovale.com.hk >

(3) North Committees Meetings Discussion Paper 9/2022. *"Proposed Public Housing Development at Queen's Hill Extension"*. Dated 15 May 2022. North District Council.

(4) LC Paper No. CB(2)614/2022(01). Legislative Council.

(5) Planning Brief. Hong Kong Housing Authority.

<https://www.pland.gov.hk/pland\_en/access/pec/planning\_brief/San%20Wan%20Road%20PB.pdf>

(6) HKHS Annual Report 2022. Hong Kong Housing Society.

(7) PWSC(2016-17)42. Legislative Council.

(8) North Committees Meetings Discussion Paper 5/2019. "Public Housing Development Programmes at Sites 1 and 2 in Sheung Shui Areas 4 and 30, a Site to the North of Po Shek Wu Road and a Site on Jockey Club Road, Fanling, and Proposed Amendments to the Approved Fanling/Sheung Shui Outline Zoning Plan No. S/FSS/22." Dated 21 January 2019. North District Council.

(9) Statutory Planning Portal 2. Town Planning Board.

### Future Road Network

4.9 Various traffic improvement works have been planned for implementation, including the Fanling Bypass Eastern and Western Sections, Lung Yeuk Tau Interchange of the Fanling Bypass Eastern Section at Sha Tau Kok Road – Lung Yeuk Tau, various local junction improvements along Ma Sik Road, Jockey Club Road associated with the FLN NDA and other developments located within Fanling / Sheung Shui area, and the Improvement of So Kwun Po Interchange etc. Figure 4.1 also shows an overview of the road network adopted in the 2034 traffic model.

### 2034 Traffic Flows

4.10 Year 2034 traffic flows with the Proposed Development are derived as follows:

| 2034 Traffic Flows with the = | 2034 Traffic Flows without the Proposed |
|-------------------------------|---|
| Proposed Development          | Development + Traffic Generated by the  |
|                               | Proposed Development                    |

4.11 Figures 4.2 and 4.3 show the 2034 AM and PM peak hour traffic flows without and with the Proposed Development respectively.

### 2034 Junction Capacity Analysis

4.12 Year 2034 junction capacity analysis for the case without and with the Proposed Development are summarised in Table 4.4 and detailed calculations are found in the Appendix A.

| Ref. | Junction   | Type<br>of<br>Junction | Parameter | Without the<br>Proposed<br>Development |                    | With the<br>Proposed<br>Development |                    |
|------|--|------------------------|-----------|--|--------------------|-------------------------------------|--------------------|
|      |  |                        |           | AM<br>Peak<br>Hour                     | PM<br>Peak<br>Hour | AM<br>Peak<br>Hour                  | PM<br>Peak<br>Hour |
| J01  | Sha Tau Kok Road /<br>Lau Shui Heung<br>Road                               | Roundabout             | RFC       | 0.4509                                 | 0.5116             | 0.5164                              | 0.5757             |
| J02  | Sha Tau Kok Road /<br>Lung Ma Road   | Roundabout             | RFC       | 0.6124                                 | 0.6559             | 0.7415                              | 0.7133             |
| J03  | Sha Tau Kok Road /<br>Ma Sik Road <sup>(Note 1)</sup>                      | Priority               | RFC       | 0.7857                                 | 0.7340             | 0.8190                              | 0.7453             |
| J04  | Sha Tau Kok Road /<br>Jockey Club Road                                     | Roundabout             | RFC       | 0.6547                                 | 0.5939             | 0.6800                              | 0.5945             |
| J05  | So Kwun Po Road /<br>Jockey Club Road /<br>Ma Sik Road <sup>(Note 1)</sup> | Signal                 | RC        | 17%                                    | 33%                | 16%                                 | 31%                |
| J06  | So Kwun Po<br>Interchange <sup>(Note 1)</sup>                              | Roundabout             | RFC       | 0.7697                                 | 0.7656             | 0.7993                              | 0.7763             |
| J07  | Lung Yeuk Tau<br>Interchange <sup>(Note 1)</sup>                           | Roundabout             | RFC       | 0.6617                                 | 0.6691             | 0.7002                              | 0.7411             |

| TABLE 4.4 2034 JUI | NCTION PERFORMANCE |
|--------------------|--------------------|
|--------------------|--------------------|

Note 1: With planned traffic improvement works to be carried by Others.

RFC - Ratio of Flow to Capacity RC – Reserve Capacity

4.13 Table 4.4 shows that the junctions analyzed have capacity to accommodate the expected traffic growth to 2034, and the traffic generated by the Proposed Development will have no adverse impact to the surrounding road network.

### 2034 Road Link Capacity Analysis

4.14 Year 2034 road link capacity analysis for the cases without and with the Proposed Development are summarised in Table 4.5.

| Ref. | Road<br>Link        | Section<br>From To     |                        |    |                           | Type<br>(Note 1)                       | Adjusted<br>Design | D                                   | Peak Hou<br>esign Flow |  | rf) |
|------|---------------------|------------------------|------------------------|----|---------------------------|--|--------------------|-------------------------------------|------------------------|--|-----|
|      |                     |                        |                        |    | Flow<br>(vph)<br>(Note 2) | Without the<br>Proposed<br>Development |                    | With the<br>Proposed<br>Development |                        |  |     |
|      |                     |                        |                        |    |                           | AM<br>Peak<br>Hour                     | PM<br>Peak<br>Hour | AM<br>Peak<br>Hour                  | PM<br>Peak<br>Hour     |  |     |
| L01  | Sha Tau<br>Kok Road | Lung Ma<br>Road        | Lau Shui<br>Heung Road | RR | 2,520                     | 0.4232                                 | 0.4747             | 0.4847                              | 0.5342                 |  |     |
| L02  | Sha Tau<br>Kok Road | Lau Shui<br>Heung Road | Lung Ma<br>Road        | RR | 2,520                     | 0.4722                                 | 0.5120             | 0.5718                              | 0.5568                 |  |     |
| L03  | Sha Tau<br>Kok Road | Ma Sik Road            | Lung Ma<br>Road        | RR | 2,520                     | 0.6789                                 | 0.6338             | 0.7356                              | 0.6878                 |  |     |
| L04  | Sha Tau<br>Kok Road | Lung Ma<br>Road        | Ma Sik Road            | RR | 2,520                     | 0.6850                                 | 0.6724             | 0.7799                              | 0.7116                 |  |     |

TABLE 4.5 2034 P/Df OF SURVEYED ROAD LINKS

| Ref. | Road<br>Link           | Section<br>From To                  |                                     | Type<br>(Note 1) | Adjusted<br>Design<br>Flow<br>(vph)<br>(Note 2) | Witho<br>Prop<br>Develo | esign Flow<br>out the<br>osed<br>opment | With<br>Prop<br>Develo | n the<br>osed<br>opment |
|------|------------------------|-------------------------------------|-------------------------------------|------------------|---|-------------------------|---|------------------------|-------------------------|
|      |                        |                                     |                                     |                  |   | AM<br>Peak<br>Hour      | PM<br>Peak<br>Hour                      | AM<br>Peak<br>Hour     | PM<br>Peak<br>Hour      |
| L05  | Sha Tau<br>Kok Road    | Jockey Club<br>Road                 | Ma Sik Road                         | RR               | 2,520   | 0.5686                  | 0.5911                                  | 0.5686                 | 0.5911                  |
| L06  | Sha Tau<br>Kok Road    | Ma Sik Road                         | Jockey Club<br>Road                 | RR               | 2,520   | 0.6168                  | 0.5363                                  | 0.6429                 | 0.5474                  |
| L07  | Ma Sik<br>Road         | Jockey Club<br>Road                 | Sha Tau Kok<br>Road                 | DD               | 1,800   | 0.8167                  | 0.8117                                  | 0.8350                 | 0.8367                  |
| L08  | Ma Sik<br>Road         | Sha Tau Kok<br>Road                 | Jockey Club<br>Road                 | DD               | 1,800   | 0.8076                  | 0.5966                                  | 0.8076                 | 0.5966                  |
| L09  | Jockey<br>Club<br>Road | Ma Sik Road<br>/ So Kwun<br>Po Road | Sha Tau Kok<br>Road                 | PD               | 2,520   | 0.2483                  | 0.2126                                  | 0.2483                 | 0.2126                  |
| L10  | Jockey<br>Club<br>Road | Sha Tau Kok<br>Road                 | Ma Sik Road<br>/ So Kwun<br>Po Road | PD               | 2,520   | 0.2873                  | 0.2461                                  | 0.2889                 | 0.2473                  |
| L11  | So Kwun<br>Po Road     | Jockey Club<br>Road                 | So Kwun Po<br>Interchange           | PD               | 2,520   | 0.6867                  | 0.4998                                  | 0.6867                 | 0.4998                  |
| L12  | So Kwun<br>Po Road     | So Kwun Po<br>Interchange           | Jockey Club<br>Road                 | PD               | 2,520   | 0.7518                  | 0.7825                                  | 0.7629                 | 0.7984                  |

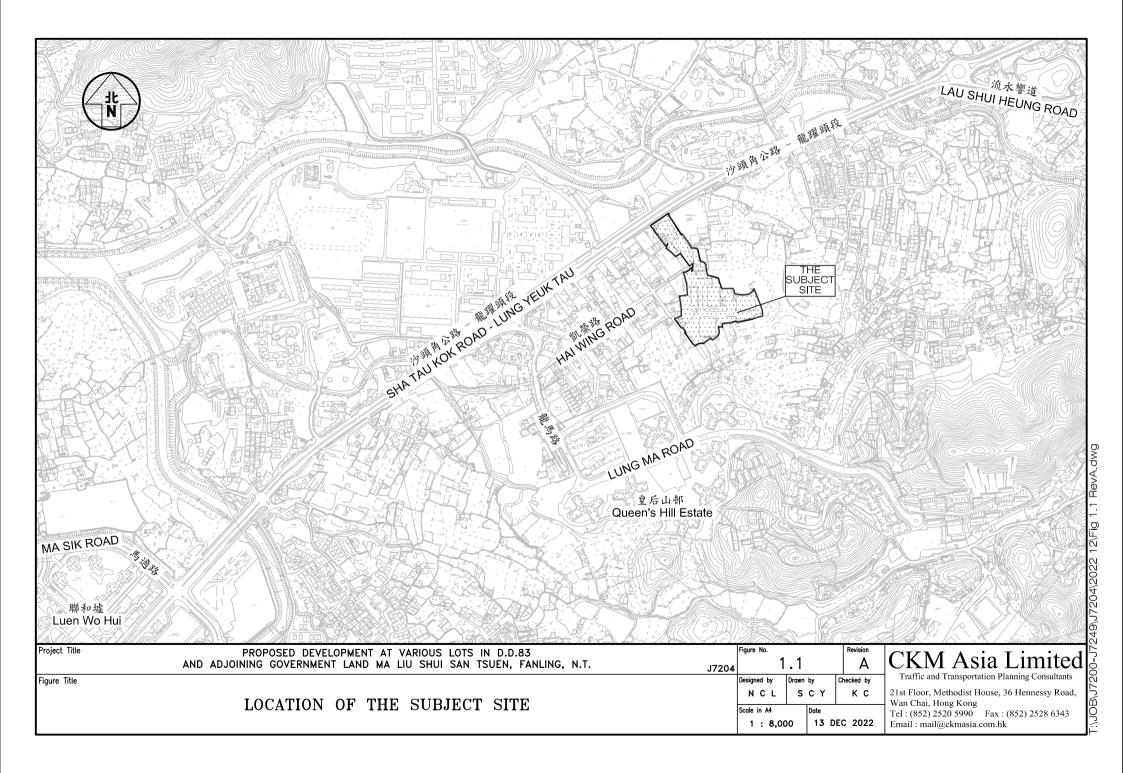
### TABLE 4.5 2034 P/Df OF SURVEYED ROAD LINKS (CONT')

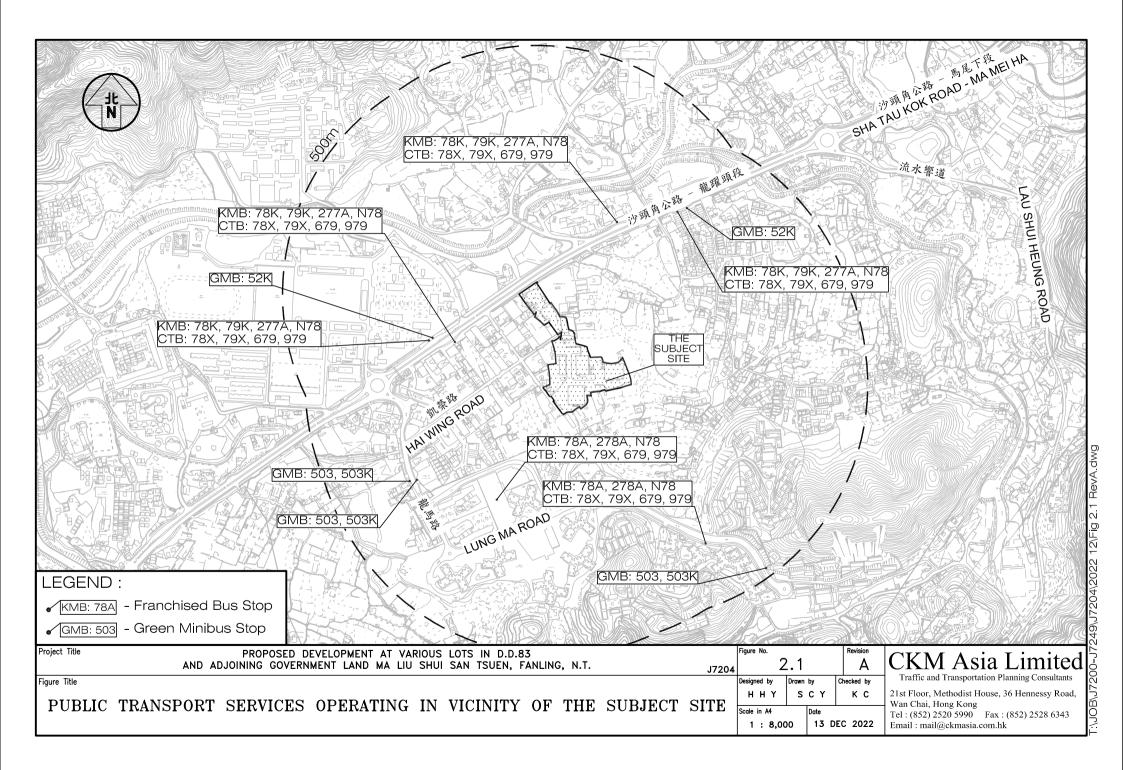
4.15 Table 4.5 shows that, the road links analyzed have capacity to accommodate the expected traffic growth to 2034 and the traffic generated by the Proposed Development will have no adverse negative impact to the surrounding road network.

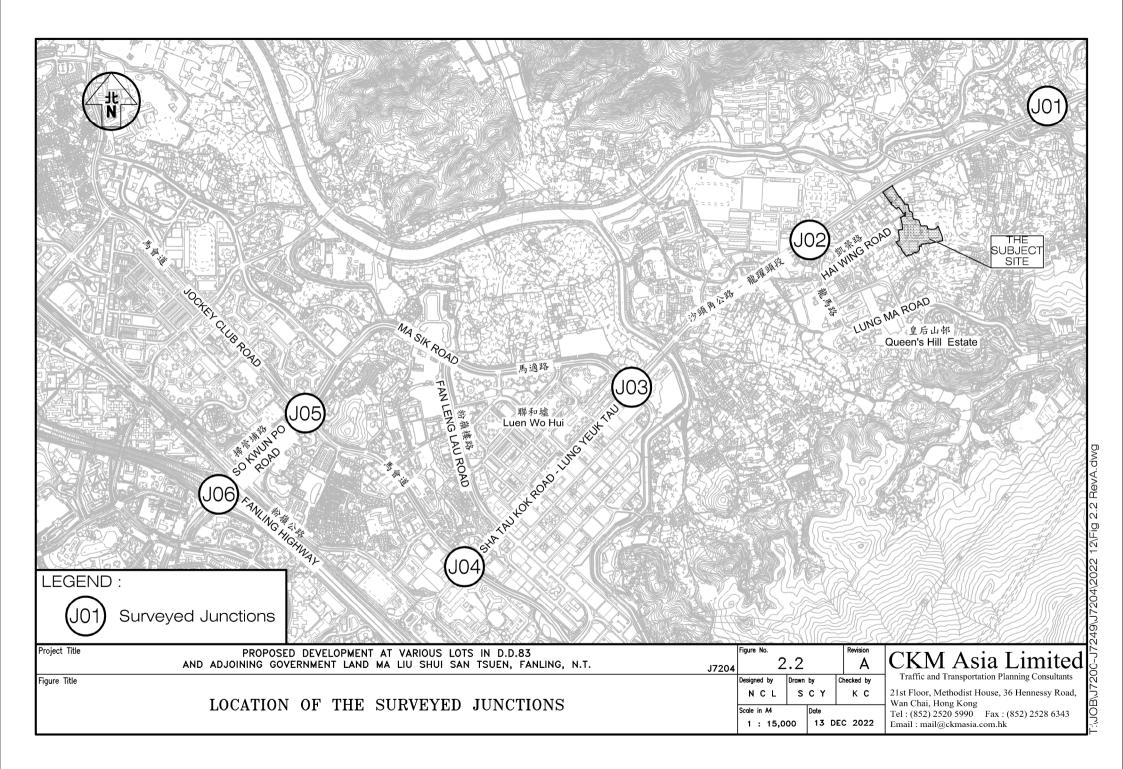
## 5.0 SUMMARY

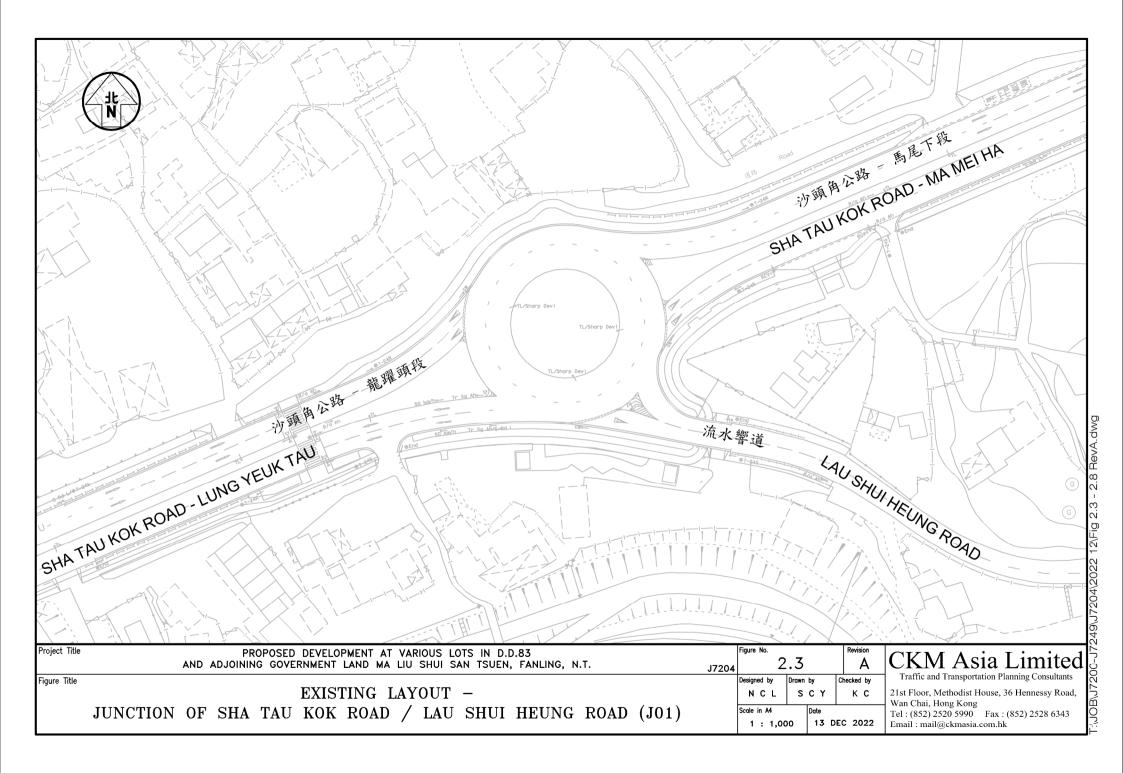
- 5.1 The Subject Site is located in various lots in D.D. 83, Lung Yeuk Tau in Fanling,
- 5.2 The Proposed Development has 5 residential blocks with 3,305 flats and 5,570 m<sup>2</sup> retail GFA.
- 5.3 The proposed internal transport facilities meets the high-end recommendation of the HKPSG, and include the following:
  - i) 479 car parking spaces @ 5.0m (L) x 2.5m (W) x Min. 2.4m (H),
  - ii) 6 accessible car parking spaces @ 5.0m (L) x 3.5m (W) x Min. 2.4 (H),
  - iii) 38 motorcycle parking spaces @ 2.4m (L) x 1.0m (W) x Min. 2.4m (H),
  - iv) 4 LGV loading / unloading bays @ 7.0m (L) x 3.5m (W) x Min. 3.6m (H),
  - v) 8 HGV loading / unloading bays @ 11.0m (L) x 3.5m (W) x Min. 4.7m (H),
  - vi) 111 bicycle parking spaces @ 1.65m (L) x 0.8m (W) or with parking rack.
- 5.4 Manual classified counts were conducted at selected junctions located in the vicinity in order to establish the existing traffic flows during the AM and PM peak hours. The design year 2034 traffic flows were derived with reference to the BDTM, and have also taken into account the traffic generation and planned traffic improvement works associated with other known planned / committed major developments located in the vicinity.
- 5.5 Traffic generation for the Proposed Development is calculated based on the trip rates adopted from the TPDM, and is expected to generate some 406 and 256 pcu (2-way) during the AM and PM peak hours respectively.
- 5.6 The traffic analysis found that the surveyed junctions and road links analyzed currently operate with capacity. With the planned traffic improvement works to be implemented by others, the analyzed junction will have sufficient capacity to accommodate the expected traffic growth to 2034 and the traffic generated by the Proposed Development. Hence, traffic generated by the Proposed Development will result in no adverse impact to the surrounding road network.
- 5.7 In view of the above, it is concluded that the Proposed Development is acceptable from traffic engineering viewpoint.

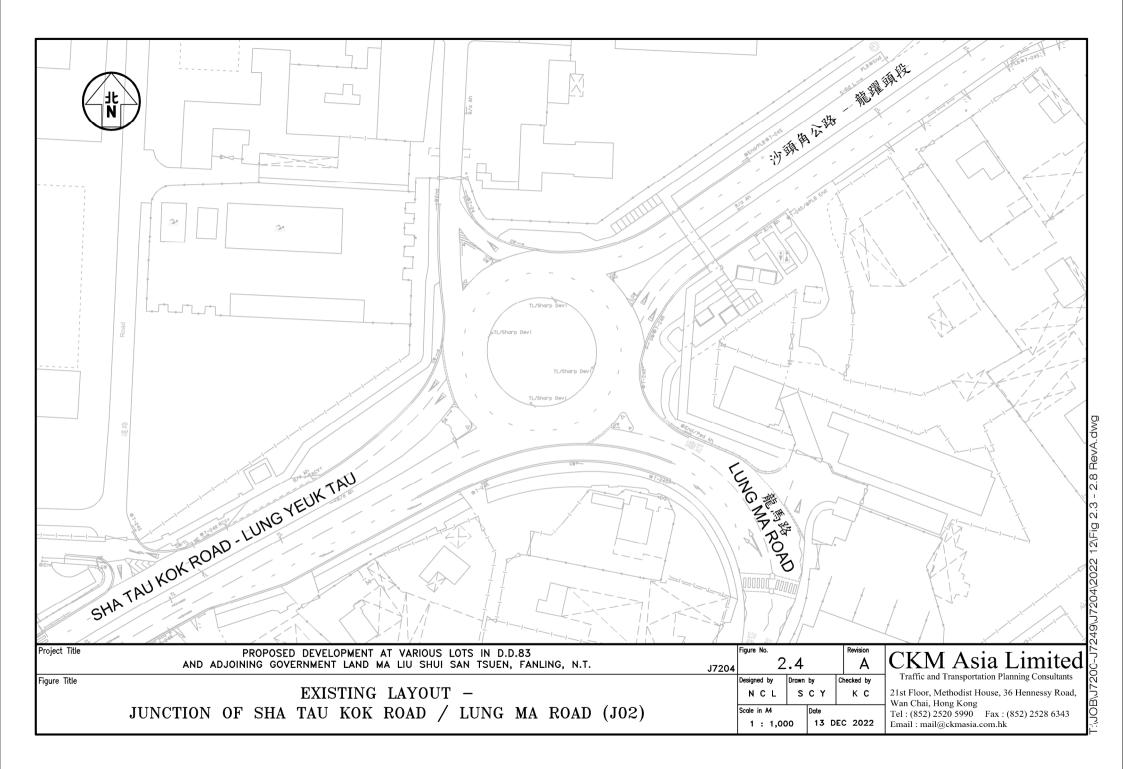
# **FIGURES**



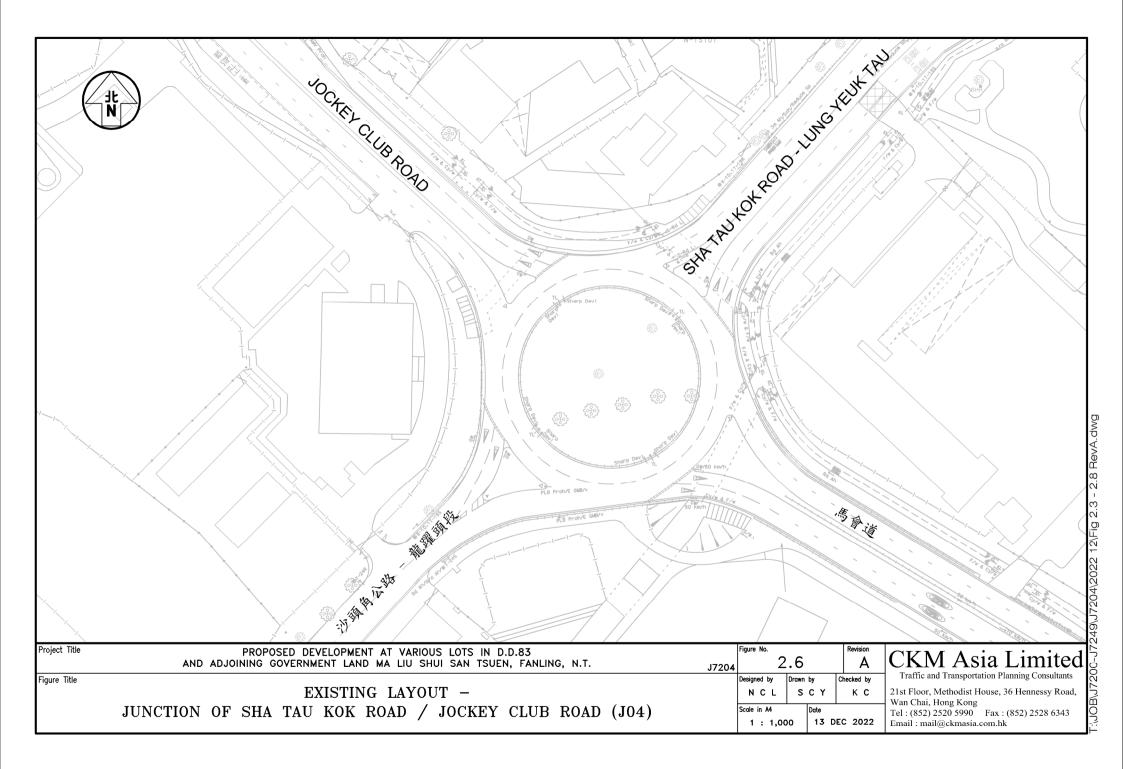


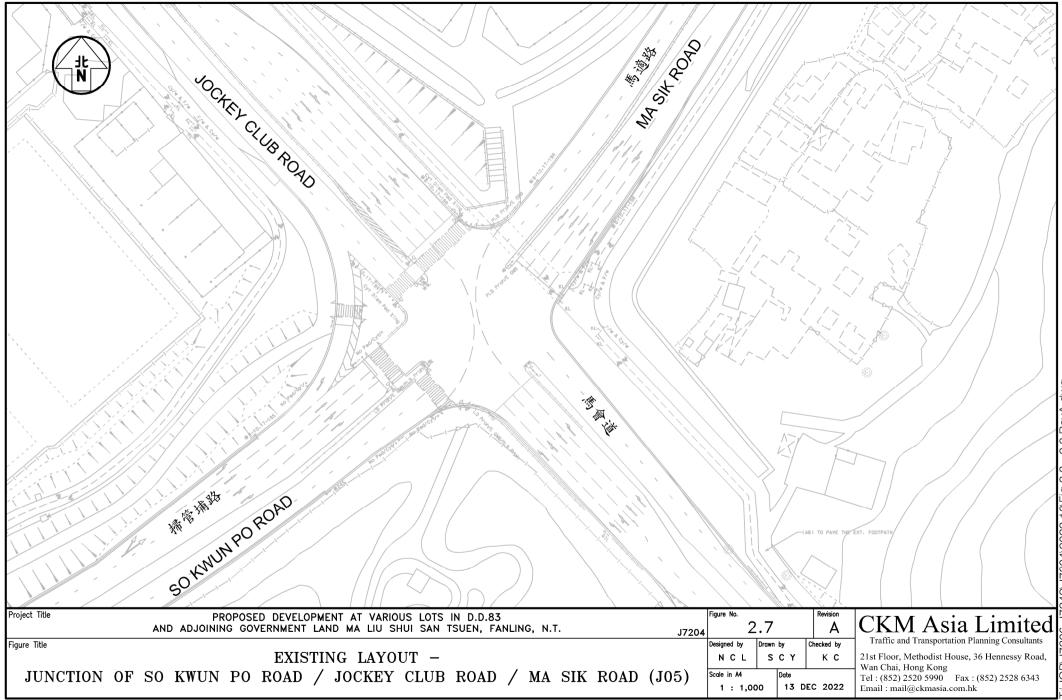


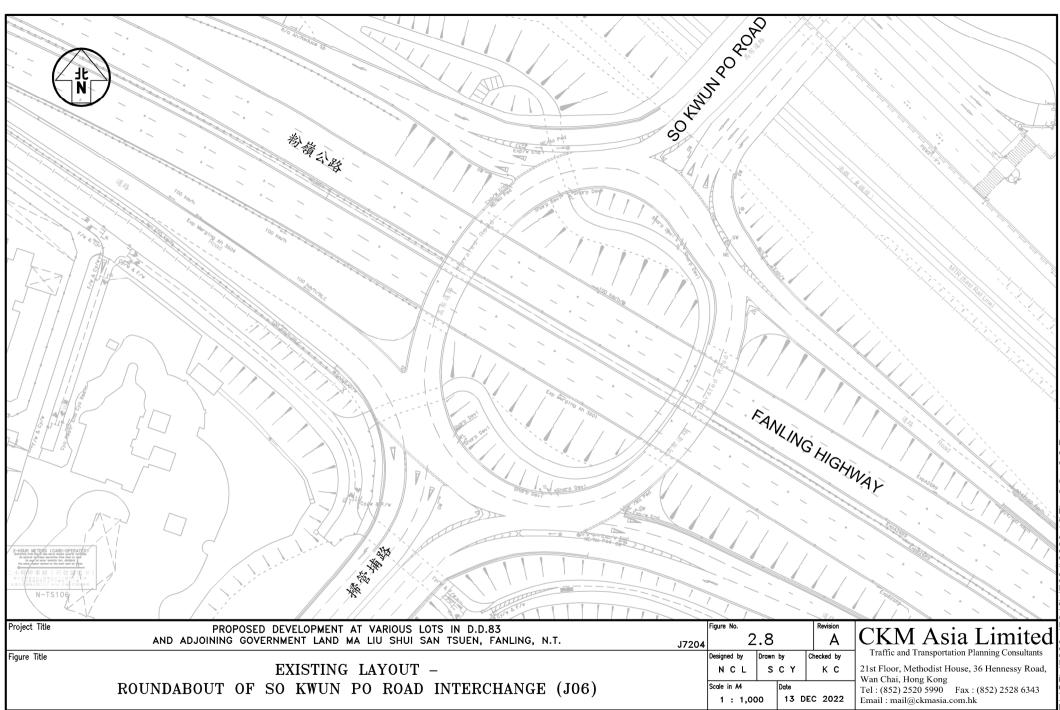




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| Project Title | PROPOSED DEVELOPMENT AT VARIOUS LOTS IN D.D.83<br>AND ADJOINING GOVERNMENT LAND MA LIU SHUI SAN TSUEN, FANLING, N.T. | Figure No.<br>2.5 A CKM Asia Limited   |
| Figure Title  | EXISTING LAYOUT –<br>JUNCTION OF SHA TAU KOK ROAD / MA SIK ROAD (J03)  | NCL SCY KC 21st Floor, Methodist House, 36 Hennessy Road,  |

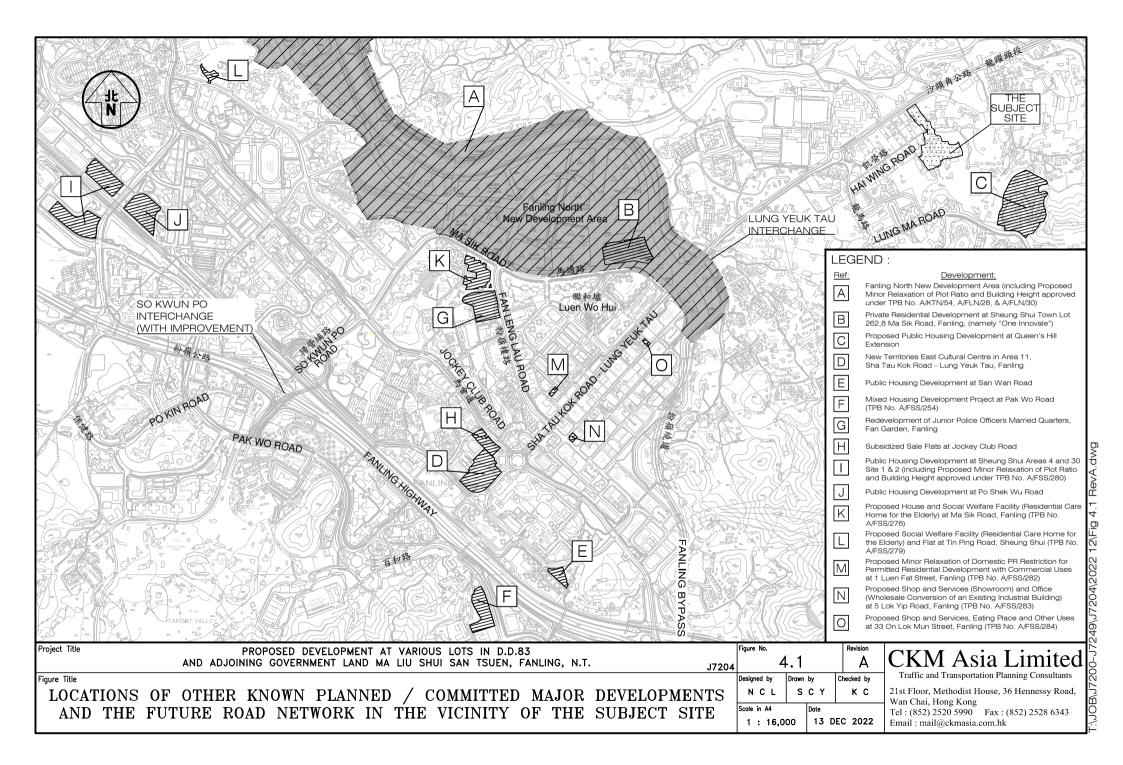


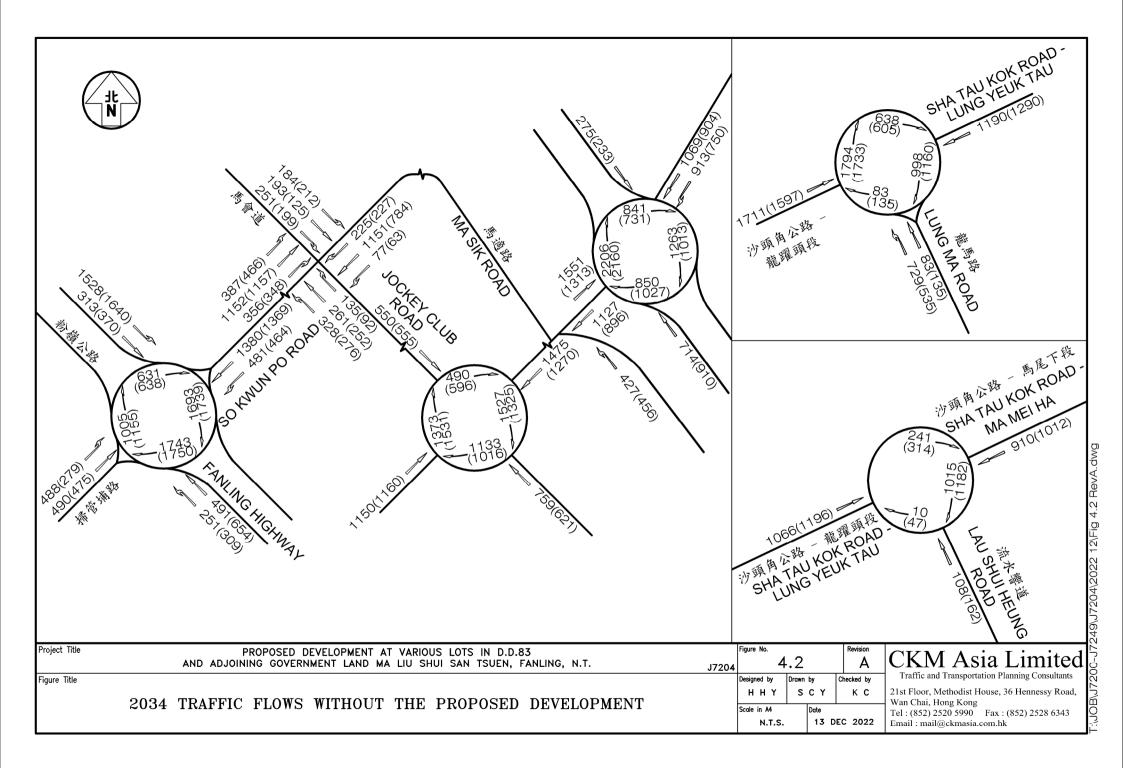


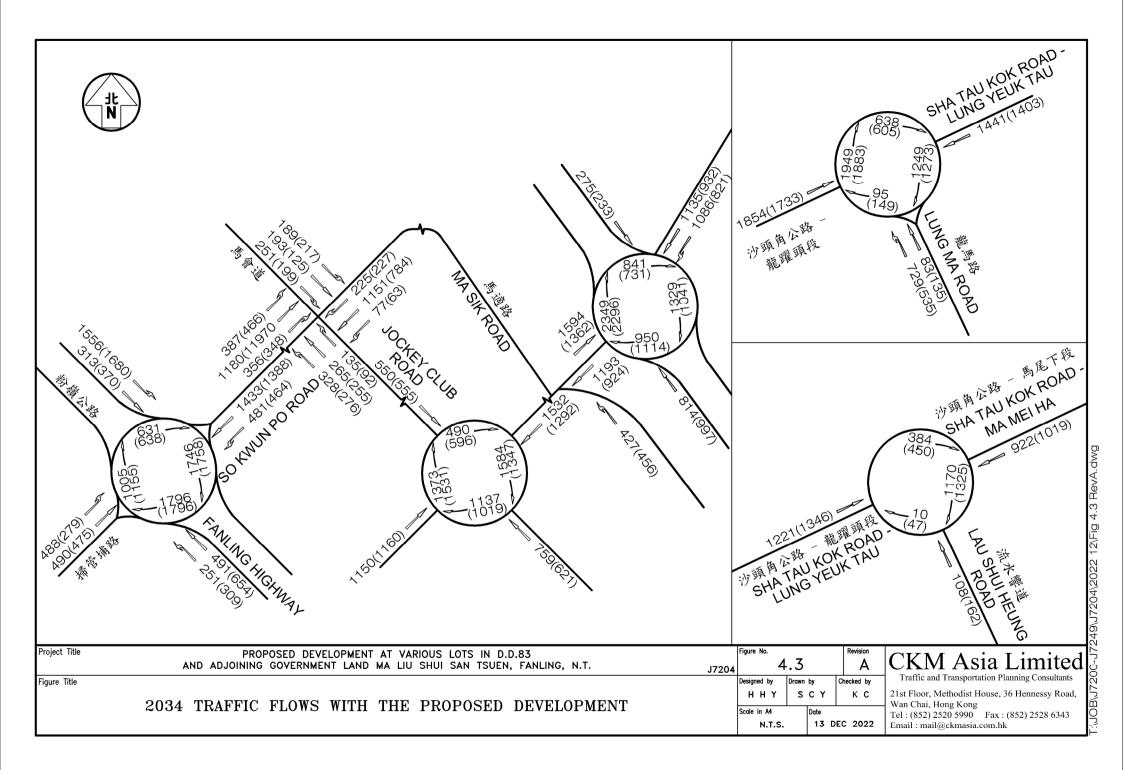


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| $\begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 $ |  |
| Project Title PROPOSED DEVELOPMENT AT VARIOUS LOTS IN D.D.83       | ジ頭角な路、KOK TAU<br>ジ頭角な路、KOK TAU<br>SHAUNG YEUK TAU<br>SHAUNG YEUK TAU   |
| Figure Title<br>EXISTING PEAK HOUR TRAFFIC FLOWS                   | J7204 2.9 A Designed by H H Y S C Y K C Scale in A4 N.T.S. Date N.T.S. Date N.T.S. N.T |







APPENDIX A JUNCTION CAPACITY ANALYSIS

## **Roundabout Analysis**

| Junction: |      | Sha Tau k          | Kok Road / I | Lau Shui He | eung Road |      |            |      |       | J              | ob Number: J7204 |
|-----------|------|--------------------|--------------|-------------|-----------|------|------------|------|-------|----------------|------------------|
| Scenario: |      | Existing Condition |              |             |           |      |            |      |       |                | J1 - P. 1        |
| Design Ye | ear: | 2022               | De           | signed By:  | NCL       | C    | hecked By: | WCH  | -     | Date:          | 13 December 2022 |
| AM Peak   |      |                    |              |             |           |      |            |      |       |                |                  |
| Arm       | To A | To B               | To C         | To D        | To E      | To F | To G       | To H | Total | q <sub>c</sub> | 7                |
| From A    | 1    | 11                 | 771          |             |           |      |            |      | 783   | 195            |                  |
| From B    | 5    |                    | 86           |             |           |      |            |      | 91    | 864            |                  |
| From C    | 703  | 103                | 92           |             |           |      |            |      | 899   | 6              |                  |
| From D    |      |                    |              |             |           |      |            |      |       |                |                  |
| From E    |      |                    |              |             |           |      |            |      |       |                |                  |
| From F    |      |                    |              |             |           |      |            |      |       |                |                  |
| From G    |      |                    |              |             |           |      |            |      |       |                |                  |
| From H    |      |                    |              |             |           |      |            |      |       |                |                  |
| Total     | 709  | 114                | 949          |             |           |      |            |      | 1772  |                |                  |

#### PM Peak

| i wi i cuk |      |      |      |      |      |      |      |      |       |                |
|------------|------|------|------|------|------|------|------|------|-------|----------------|
| Arm        | To A | To B | To C | To D | To E | To F | To G | To H | Total | q <sub>c</sub> |
| From A     | 6    | 17   | 880  |      |      |      |      |      | 902   | 235            |
| From B     | 20   |      | 104  |      |      |      |      |      | 124   | 1032           |
| From C     | 738  | 89   | 146  |      |      |      |      |      | 974   | 26             |
| From D     |      |      |      |      |      |      |      |      |       |                |
| From E     |      |      |      |      |      |      |      |      |       |                |
| From F     |      |      |      |      |      |      |      |      |       |                |
| From G     |      |      |      |      |      |      |      |      |       |                |
| From H     |      |      |      |      |      |      |      |      |       |                |
| Total      | 764  | 106  | 1130 |      |      |      |      |      | 2000  |                |

#### Legend

| Arm | Road (in clockwise order) |  |
|-----|---------------------------|--|
| А   | Sha Tau Kok Road - East   |  |
| В   | Lau Shui Heung Road       |  |
| С   | Sha Tau Kok Road - West   |  |
| D   |                           |  |
| Е   |                           |  |
| F   |                           |  |
| G   |                           |  |
| н   |                           |  |

### Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 7.5   | 7.0   | 55.0  | 1.0   | 55    | 15    | 0.8 |
| From B | 6.0   | 3.5   | 100.0 | 8.0   | 55    | 25    | 0.5 |
| From C | 7.5   | 7.0   | 80.0  | 1.0   | 55    | 15    | 0.8 |
| From D |       |       |       |       |       |       |     |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_{c}$               | Circulating Flow across the Entry   |
| K                     | = 1-0.00347(∅-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| f <sub>c</sub>        | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>        | = 1+0.5/(1+M)                       |
| М                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |
|                       |                                     |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |
|---|---------------------------|---------------|
| v | Approach Half Width       | 2.0 - 7.3 m   |
| r | Entry Radius              | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m    |
| Ø | Entry Angle               | 10° - 60°     |
| S | Sharpness of Flare        | 0.0 - 3.0     |

#### Ratio-of-Flow to Capacity (RFC)

|        |                       |       |                |       |      |                | $Q_E$ |      | Entry Flow |     | RFC   |       |
|--------|-----------------------|-------|----------------|-------|------|----------------|-------|------|------------|-----|-------|-------|
| Arm    | <b>x</b> <sub>2</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM  | AM    | PM    |
| From A | 7.192                 | 0.607 | 1.311          | 1.083 | 2179 | 0.671          | 2218  | 2190 | 783        | 902 | 0.353 | 0.412 |
| From B | 4.750                 | 0.607 | 1.311          | 1.056 | 1439 | 0.537          | 1030  | 935  | 91         | 124 | 0.088 | 0.132 |
| From C | 7.192                 | 0.607 | 1.311          | 1.089 | 2179 | 0.671          | 2368  | 2354 | 899        | 974 | 0.379 | 0.414 |
| From D |                       |       |                |       |      |                |       |      |            |     |       |       |
| From E |                       |       |                |       |      |                |       |      |            |     |       |       |
| From F |                       |       |                |       |      |                |       |      |            |     |       |       |
| From G |                       |       |                |       |      |                |       |      |            |     |       |       |
| From H |                       |       |                |       |      |                |       |      |            |     |       |       |

| Junction:    |      | Sha Tau K  | Kok Road / I | Lau Shui He     | eung Road |                 |      |      |       | Job Number: <u>J7204</u><br>J1 - P. 2 |                  |  |
|--------------|------|------------|--------------|-----------------|-----------|-----------------|------|------|-------|---------------------------------------|------------------|--|
| Scenario:    |      | Without Pr | roposed De   | velopment       |           |                 |      |      |       |                                       |                  |  |
| Design Year: |      | 2034 D     |              | esigned By: NCL |           | Checked By: WCH |      |      | Date: |                                       | 13 December 2022 |  |
| AM Peak      |      |            |              |                 |           |                 |      |      |       |                                       |                  |  |
| Arm          | To A | To B       | To C         | To D            | To E      | To F            | To G | To H | Total | q <sub>c</sub>                        |                  |  |
| From A       | 1    | 21         | 889          |                 |           |                 |      |      | 910   | 241                                   |                  |  |
| From B       | 9    |            | 99           |                 |           |                 |      |      | 108   | 1015                                  |                  |  |
| From C       | 825  | 117        | 125          |                 |           |                 |      |      | 1066  | 10                                    |                  |  |
| From D       |      |            |              |                 |           |                 |      |      |       |                                       |                  |  |
| From E       |      |            |              |                 |           |                 |      |      |       |                                       |                  |  |
| From F       |      |            |              |                 |           |                 |      |      |       |                                       |                  |  |
| From G       |      |            |              |                 |           |                 |      |      |       |                                       |                  |  |
| From H       |      |            |              |                 |           |                 |      |      |       |                                       |                  |  |
| Total        | 835  | 137        | 1113         |                 |           |                 |      |      | 2085  |                                       |                  |  |

#### PM Peak

| i wi i cuk |      |      |      |      |      |      |      |      |       |                |
|------------|------|------|------|------|------|------|------|------|-------|----------------|
| Arm        | To A | To B | To C | To D | To E | To F | To G | To H | Total | q <sub>c</sub> |
| From A     | 6    | 9    | 996  |      |      |      |      |      | 1012  | 314            |
| From B     | 40   |      | 122  |      |      |      |      |      | 162   | 1182           |
| From C     | 882  | 136  | 179  |      |      |      |      |      | 1196  | 47             |
| From D     |      |      |      |      |      |      |      |      |       |                |
| From E     |      |      |      |      |      |      |      |      |       |                |
| From F     |      |      |      |      |      |      |      |      |       |                |
| From G     |      |      |      |      |      |      |      |      |       |                |
| From H     |      |      |      |      |      |      |      |      |       |                |
| Total      | 929  | 145  | 1297 |      |      |      |      |      | 2371  |                |

#### Legend

| Arm | Road (in clockwise order) |  |
|-----|---------------------------|--|
| А   | Sha Tau Kok Road - East   |  |
| В   | Lau Shui Heung Road       |  |
| С   | Sha Tau Kok Road - West   |  |
| D   |                           |  |
| Е   |                           |  |
| F   |                           |  |
| G   |                           |  |
| н   |                           |  |

## Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 7.5   | 7.0   | 55.0  | 1.0   | 55    | 15    | 0.8 |
| From B | 6.0   | 3.5   | 100.0 | 8.0   | 55    | 25    | 0.5 |
| From C | 7.5   | 7.0   | 80.0  | 1.0   | 55    | 15    | 0.8 |
| From D |       |       |       |       |       |       |     |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

## Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_{c}$               | Circulating Flow across the Entry   |
| K                     | = 1-0.00347(∅-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| f <sub>c</sub>        | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>        | = 1+0.5/(1+M)                       |
| М                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |
|                       |                                     |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |  |
|---|---------------------------|---------------|--|
| v | Approach Half Width       | 2.0 - 7.3 m   |  |
| r | Entry Radius              | 6.0 - 100.0 m |  |
| L | Effective Length of Flare | 1.0 - 100.0 m |  |
| D | Inscribed Circle Diameter | 15 - 100 m    |  |
| Ø | Entry Angle               | 10° - 60°     |  |
| S | Sharpness of Flare        | 0.0 - 3.0     |  |

|        |                |       |                |       |      |                | Q <sub>E</sub> |      | Entry Flow |      | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|----------------|------|------------|------|-------|-------|
| Arm    | X <sub>3</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM             | PM   | AM         | PM   | AM    | PM    |
| From A | 7.192          | 0.607 | 1.311          | 1.083 | 2179 | 0.671          | 2185           | 2132 | 910        | 1012 | 0.417 | 0.475 |
| From B | 4.750          | 0.607 | 1.311          | 1.056 | 1439 | 0.537          | 945            | 850  | 108        | 162  | 0.115 | 0.191 |
| From C | 7.192          | 0.607 | 1.311          | 1.089 | 2179 | 0.671          | 2365           | 2338 | 1066       | 1196 | 0.451 | 0.512 |
| From D |                |       |                |       |      |                |                |      |            |      |       |       |
| From E |                |       |                |       |      |                |                |      |            |      |       |       |
| From F |                |       |                |       |      |                |                |      |            |      |       |       |
| From G |                |       |                |       |      |                |                |      |            |      |       |       |
| From H |                |       |                |       |      |                |                |      |            |      |       |       |

| Junction:<br>Scenario:<br>Design Year: |      | Sha Tau K | ok Road / L      | .au Shui He | ung Road        |      |      |      |       | Job Number: <u>J7204</u><br>J1 - P. 3 |   |  |
|--|------|-----------|------------------|-------------|-----------------|------|------|------|-------|---------------------------------------|---|--|
|  |      | With Prop | osed Devel       | opment      |                 |      |      |      |       |                                       |   |  |
|  |      | 2034      | Designed By: NCL |             | Checked By: WCH |      |      |      | Date: | 13 December 2022                      |   |  |
| AM Peak                                |      |           |                  |             |                 |      |      |      |       |                                       |   |  |
| Arm                                    | To A | To B      | To C             | To D        | To E            | To F | To G | To H | Total | q <sub>c</sub>                        | ] |  |
| From A                                 | 1    | 21        | 901              |             |                 |      |      |      | 922   | 384                                   |   |  |
| From B                                 | 9    |           | 99               |             |                 |      |      |      | 108   | 1170                                  |   |  |
| From C                                 | 837  | 117       | 268              |             |                 |      |      |      | 1221  | 10                                    |   |  |
| From D                                 |      |           |                  |             |                 |      |      |      |       |                                       |   |  |
| From E                                 |      |           |                  |             |                 |      |      |      |       |                                       |   |  |
| From F                                 |      |           |                  |             |                 |      |      |      |       |                                       |   |  |
| From G                                 |      |           |                  |             |                 |      |      |      |       |                                       |   |  |

#### PM Peak

From H

847

137

Total

| i wi i cuk |      |      |      |      |      |      |      |      |       |                |
|------------|------|------|------|------|------|------|------|------|-------|----------------|
| Arm        | To A | To B | To C | To D | To E | To F | To G | To H | Total | q <sub>c</sub> |
| From A     | 6    | 9    | 1003 |      |      |      |      |      | 1019  | 450            |
| From B     | 40   |      | 122  |      |      |      |      |      | 162   | 1325           |
| From C     | 896  | 136  | 315  |      |      |      |      |      | 1346  | 47             |
| From D     |      |      |      |      |      |      |      |      |       |                |
| From E     |      |      |      |      |      |      |      |      |       |                |
| From F     |      |      |      |      |      |      |      |      |       |                |
| From G     |      |      |      |      |      |      |      |      |       |                |
| From H     |      |      |      |      |      |      |      |      |       |                |
| Total      | 943  | 145  | 1440 |      |      |      |      |      | 2528  |                |

1268

#### Legend

| Arm | Road (in clockwise order) |  |
|-----|---------------------------|--|
| А   | Sha Tau Kok Road - East   |  |
| В   | Lau Shui Heung Road       |  |
| С   | Sha Tau Kok Road - West   |  |
| D   |                           |  |
| Е   |                           |  |
| F   |                           |  |
| G   |                           |  |
| н   |                           |  |

## Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 7.5   | 7.0   | 55.0  | 1.0   | 55    | 15    | 0.8 |
| From B | 6.0   | 3.5   | 100.0 | 8.0   | 55    | 25    | 0.5 |
| From C | 7.5   | 7.0   | 80.0  | 1.0   | 55    | 15    | 0.8 |
| From D |       |       |       |       |       |       |     |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

2252

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_{c}$               | Circulating Flow across the Entry   |
| K                     | = 1-0.00347(∅-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| f <sub>c</sub>        | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>        | = 1+0.5/(1+M)                       |
| Μ                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |
|                       |                                     |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |
|---|---------------------------|---------------|
| v | Approach Half Width       | 2.0 - 7.3 m   |
| r | Entry Radius              | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m    |
| Ø | Entry Angle               | 10° - 60°     |
| S | Sharpness of Flare        | 0.0 - 3.0     |

|        |                |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | x <sub>6</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.192          | 0.607 | 1.311          | 1.083 | 2179 | 0.671          | 2081  | 2033 | 922        | 1019 | 0.443 | 0.501 |
| From B | 4.750          | 0.607 | 1.311          | 1.056 | 1439 | 0.537          | 857   | 769  | 108        | 162  | 0.127 | 0.211 |
| From C | 7.192          | 0.607 | 1.311          | 1.089 | 2179 | 0.671          | 2365  | 2338 | 1221       | 1346 | 0.516 | 0.576 |
| From D |                |       |                |       |      |                |       |      |            |      |       |       |
| From E |                |       |                |       |      |                |       |      |            |      |       |       |
| From F |                |       |                |       |      |                |       |      |            |      |       |       |
| From G |                |       |                |       |      |                |       |      |            |      |       |       |
| From H |                |       |                |       |      |                |       |      |            |      |       |       |

| Junction:      |      | Sha Tau K   | kok Road / I | Lung Ma Ro | ad   |      |            |      |       | Job Number: J7204 |                  |  |
|----------------|------|-------------|--------------|------------|------|------|------------|------|-------|-------------------|------------------|--|
| Scenario:      |      | Existing Co | ondition     | J2 - P. 1  |      |      |            |      |       |                   |                  |  |
| Design Ye      | ar:  | 2022        | De           | signed By: | NCL  | CI   | necked By: | WCH  |       | Date:             | 13 December 2022 |  |
| AM Peak<br>Arm | To A | To B        | To C         | To D       | To E | To F | To G       | To H | Total | q <sub>c</sub>    | 1                |  |
| From A         |      | 64          | 934          |            |      |      |            |      | 997   | 461               |                  |  |
| From B         | 54   |             |              |            |      |      |            |      | 54    | 1010              |                  |  |
| From C         | 897  | 385         | 76           |            |      |      |            |      | 1358  | 54                |                  |  |
| From D         |      |             |              |            |      |      |            |      |       | 1412              |                  |  |

| From E |     |     |      |      |  |
|--------|-----|-----|------|------|--|
| From F |     |     |      |      |  |
| From G |     |     |      |      |  |
| From H |     |     |      |      |  |
| Total  | 952 | 449 | 1010 | 2410 |  |

#### PM Peak

| Arm    | To A | To B | To C | To D | To E | To F | To G | To H | Total | q <sub>c</sub> |
|--------|------|------|------|------|------|------|------|------|-------|----------------|
| From A |      | 61   | 1061 |      |      |      |      |      | 1122  | 454            |
| From B | 78   |      |      |      |      |      |      |      | 78    | 1175           |
| From C | 841  | 340  | 114  |      |      |      |      |      | 1295  | 78             |
| From D |      |      |      |      |      |      |      |      |       | 1373           |
| From E |      |      |      |      |      |      |      |      |       |                |
| From F |      |      |      |      |      |      |      |      |       |                |
| From G |      |      |      |      |      |      |      |      |       |                |
| From H |      |      |      |      |      |      |      |      |       |                |
| Total  | 919  | 401  | 1175 |      |      |      |      |      | 2495  |                |

## Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| А   | Sha Tau Kok Road - East   |
| В   | Lung Ma Road              |
| С   | Sha Tau Kok Road - West   |
| D   | San Wai Barracks          |
| Е   |                           |
| F   |                           |
| G   |                           |
| Н   |                           |

## Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 7.5   | 7.0   | 40.0  | 6.0   | 55    | 15    | 0.1 |
| From B | 4.0   | 3.5   | 70.0  | 15.0  | 55    | 10    | 0.1 |
| From C | 9.5   | 7.5   | 35.0  | 25.0  | 55    | 10    | 0.1 |
| From D | 5.5   | 4.5   | 20.0  | 10.0  | 55    | 10    | 0.2 |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                     | Entry Capacity                      |
|---------------------------|-------------------------------------|
| $\mathbf{q}_{\mathrm{c}}$ | Circulating Flow across the Entry   |
| К                         | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F                         | = 303x <sub>2</sub>                 |
| $f_{c}$                   | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>            | = 1+0.5/(1+M)                       |
| М                         | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub>     | = v+(e-v)/(1+2S)                    |
| S                         | = 1.6(e-v)/L                        |
|                           |                                     |

#### Limitation

|   | ***                       |               |
|---|---------------------------|---------------|
| е | Entry Width               | 4.0 - 15.0 m  |
| v | Approach Half Width       | 2.0 - 7.3 m   |
| r | Entry Radius              | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m    |
| Ø | Entry Angle               | 10° - 60°     |
| S | Sharpness of Flare        | 0.0 - 3.0     |

|        |                       |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|-----------------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | <b>x</b> <sub>2</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.395                 | 0.607 | 1.311          | 1.077 | 2241 | 0.683          | 2073  | 2078 | 997        | 1122 | 0.481 | 0.540 |
| From B | 3.952                 | 0.607 | 1.311          | 1.104 | 1197 | 0.493          | 773   | 683  | 54         | 78   | 0.070 | 0.114 |
| From C | 9.092                 | 0.607 | 1.311          | 1.090 | 2755 | 0.776          | 2958  | 2938 | 1358       | 1295 | 0.459 | 0.441 |
| From D | 5.258                 | 0.607 | 1.311          | 1.069 | 1593 | 0.565          | 850   | 874  | 0          | 0    | 0.000 | 0.000 |
| From E |                       |       |                |       |      |                |       |      |            |      |       |       |
| From F |                       |       |                |       |      |                |       |      |            |      |       |       |
| From G |                       |       |                |       |      |                |       |      |            |      |       |       |
| From H |                       |       |                |       |      |                |       |      |            |      |       |       |

| Junction:    | Sha Tau Ko  | k Road / Lung Ma Road |                 |       | Job Number: J7204 |
|--------------|-------------|-----------------------|-----------------|-------|-------------------|
| Scenario:    | Without Pro | posed Development     |                 |       | J2 - P. 2         |
| Design Year: | 2034        | Designed By: NCL      | Checked By: WCH | Date: | 13 December 2022  |

AM Peak

| AW Peak |      |      |      |      |      |      |      |      |       |                |
|---------|------|------|------|------|------|------|------|------|-------|----------------|
| Arm     | To A | To B | To C | To D | To E | To F | To G | To H | Total | q <sub>c</sub> |
| From A  | 1    | 192  | 997  |      |      |      |      |      | 1190  | 638            |
| From B  | 83   |      |      |      |      |      |      |      | 83    | 998            |
| From C  | 1073 | 638  |      |      |      |      |      |      | 1711  | 83             |
| From D  |      |      |      |      |      |      |      |      |       | 1794           |
| From E  |      |      |      |      |      |      |      |      |       |                |
| From F  |      |      |      |      |      |      |      |      |       |                |
| From G  |      |      |      |      |      |      |      |      |       |                |
| From H  |      |      |      |      |      |      |      |      |       |                |
| Total   | 1156 | 830  | 997  |      |      |      |      |      | 2983  |                |

#### PM Peak

| 1 millioun |      |      |      |      |      |      |      |      |       |                |
|------------|------|------|------|------|------|------|------|------|-------|----------------|
| Arm        | To A | To B | To C | To D | To E | To F | To G | To H | Total | q <sub>c</sub> |
| From A     | 1    | 134  | 1156 |      |      |      |      |      | 1290  | 605            |
| From B     | 135  |      |      |      |      |      |      |      | 135   | 1160           |
| From C     | 992  | 602  | 3    |      |      |      |      |      | 1597  | 135            |
| From D     |      |      |      |      |      |      |      |      |       | 1733           |
| From E     |      |      |      |      |      |      |      |      |       |                |
| From F     |      |      |      |      |      |      |      |      |       |                |
| From G     |      |      |      |      |      |      |      |      |       |                |
| From H     |      |      |      |      |      |      |      |      |       |                |
| Total      | 1127 | 736  | 1159 |      |      |      |      |      | 3022  |                |

#### Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| А   | Sha Tau Kok Road - East   |
| В   | Lung Ma Road              |
| С   | Sha Tau Kok Road - West   |
| D   | San Wai Barracks          |
| Е   |                           |
| F   |                           |
| G   |                           |
| н   |                           |

## Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 7.5   | 7.0   | 40.0  | 6.0   | 55    | 15    | 0.1 |
| From B | 4.0   | 3.5   | 70.0  | 15.0  | 55    | 10    | 0.1 |
| From C | 9.5   | 7.5   | 35.0  | 25.0  | 55    | 10    | 0.1 |
| From D | 5.5   | 4.5   | 20.0  | 10.0  | 55    | 10    | 0.2 |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                                 |
|-----------------------|--|
| q <sub>c</sub>        | Circulating Flow across the Entry              |
| K<br>F                | = 1-0.00347(∅-30)-0.978[(1/r)-0.05]<br>= 303x₂ |
| f <sub>c</sub>        | $= 0.210t_{\rm D}(1+0.2x_2)$                   |
| t <sub>D</sub>        | = 1+0.5/(1+M)                                  |
| М                     | = exp[(D-60)/10]                               |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                               |
| S                     | = 1.6(e-v)/L                                   |
|                       |  |

#### Limitation

| eEntry Width4.0 - 15.0 mvApproach Half Width2.0 - 7.3 mrEntry Radius6.0 - 100.0 mLEffective Length of Flare1.0 - 100.0 mDJascribed Circle Diameter15, 100 m |   |                           |               |
|---|---|---------------------------|---------------|
| r Entry Radius 6.0 - 100.0 m<br>L Effective Length of Flare 1.0 - 100.0 m   | е | Entry Width               | 4.0 - 15.0 m  |
| L Effective Length of Flare 1.0 - 100.0 m   | v | Approach Half Width       | 2.0 - 7.3 m   |
| 5   | r | Entry Radius              | 6.0 - 100.0 m |
| D Inscribed Circle Diameter 15, 100 m   | L | Effective Length of Flare | 1.0 - 100.0 m |
|   | D | Inscribed Circle Diameter | 15 - 100 m    |
| $\varnothing$ Entry Angle 10° - 60°   | Ø | Entry Angle               | 10° - 60°     |
| S Sharpness of Flare 0.0 - 3.0  | S | Sharpness of Flare        | 0.0 - 3.0     |

|        |                |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | x <sub>3</sub> | Μ     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.395          | 0.607 | 1.311          | 1.077 | 2241 | 0.683          | 1943  | 1967 | 1190       | 1290 | 0.612 | 0.656 |
| From B | 3.952          | 0.607 | 1.311          | 1.104 | 1197 | 0.493          | 779   | 691  | 83         | 135  | 0.106 | 0.195 |
| From C | 9.092          | 0.607 | 1.311          | 1.090 | 2755 | 0.776          | 2933  | 2889 | 1711       | 1597 | 0.583 | 0.553 |
| From D | 5.258          | 0.607 | 1.311          | 1.069 | 1593 | 0.565          | 620   | 657  | 0          | 0    | 0.000 | 0.000 |
| From E |                |       |                |       |      |                |       |      |            |      |       |       |
| From F |                |       |                |       |      |                |       |      |            |      |       |       |
| From G |                |       |                |       |      |                |       |      |            |      |       |       |
| From H |                |       |                |       |      |                |       |      |            |      |       |       |

| Junction:    | Sha Tau Ko  | k Road / Lung Ma Road | Job Number: J7204 |           |                  |  |
|--------------|-------------|-----------------------|-------------------|-----------|------------------|--|
| Scenario:    | With Propos | sed Development       |                   | J2 - P. 3 |                  |  |
| Design Year: | 2034        | Designed By: NCL      | Checked By: WCH   | Date:     | 13 December 2022 |  |

AM Peak

| Arm    | To A | To B | To C | To D | To E | To F | To G | To H | Total | qc   |
|--------|------|------|------|------|------|------|------|------|-------|------|
| From A | 13   | 192  | 1236 |      |      |      |      |      | 1441  | 638  |
| From B | 83   |      |      |      |      |      |      |      | 83    | 1249 |
| From C | 1216 | 638  |      |      |      |      |      |      | 1854  | 95   |
| From D |      |      |      |      |      |      |      |      |       | 1949 |
| From E |      |      |      |      |      |      |      |      |       |      |
| From F |      |      |      |      |      |      |      |      |       |      |
| From G |      |      |      |      |      |      |      |      |       |      |
| From H |      |      |      |      |      |      |      |      |       |      |
| Total  | 1311 | 830  | 1236 |      |      |      |      |      | 3377  |      |

#### PM Peak

| 1 m i oun |      |      |      |      |      |      |      |      |       |      |
|-----------|------|------|------|------|------|------|------|------|-------|------|
| Arm       | To A | To B | To C | To D | To E | To F | To G | To H | Total | qc   |
| From A    | 15   | 134  | 1255 |      |      |      |      |      | 1403  | 605  |
| From B    | 135  |      |      |      |      |      |      |      | 135   | 1273 |
| From C    | 1128 | 602  | 3    |      |      |      |      |      | 1733  | 149  |
| From D    |      |      |      |      |      |      |      |      |       | 1883 |
| From E    |      |      |      |      |      |      |      |      |       |      |
| From F    |      |      |      |      |      |      |      |      |       |      |
| From G    |      |      |      |      |      |      |      |      |       |      |
| From H    |      |      |      |      |      |      |      |      |       |      |
| Total     | 1277 | 736  | 1258 |      |      |      |      |      | 3271  |      |

#### Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| А   | Sha Tau Kok Road - East   |
| В   | Lung Ma Road              |
| С   | Sha Tau Kok Road - West   |
| D   | San Wai Barracks          |
| Е   |                           |
| F   |                           |
| G   |                           |
| н   |                           |

## Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 7.5   | 7.0   | 40.0  | 6.0   | 55    | 15    | 0.1 |
| From B | 4.0   | 3.5   | 70.0  | 15.0  | 55    | 10    | 0.1 |
| From C | 9.5   | 7.5   | 35.0  | 25.0  | 55    | 10    | 0.1 |
| From D | 5.5   | 4.5   | 20.0  | 10.0  | 55    | 10    | 0.2 |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                     | Entry Capacity                      |
|---------------------------|-------------------------------------|
| $\mathbf{q}_{\mathrm{c}}$ | Circulating Flow across the Entry   |
| К                         | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F                         | = 303x <sub>2</sub>                 |
| $f_{c}$                   | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>            | = 1+0.5/(1+M)                       |
| М                         | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub>     | = v+(e-v)/(1+2S)                    |
| S                         | = 1.6(e-v)/L                        |
|                           |                                     |

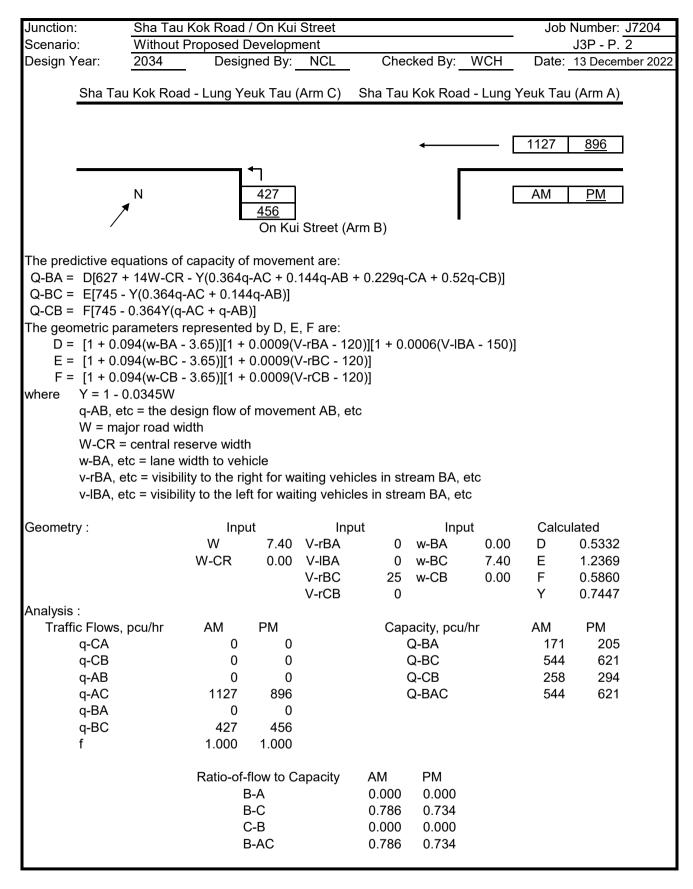
#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |
|---|---------------------------|---------------|
| v | Approach Half Width       | 2.0 - 7.3 m   |
| r | Entry Radius              | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m    |
| Ø | Entry Angle               | 10° - 60°     |
| S | Sharpness of Flare        | 0.0 - 3.0     |

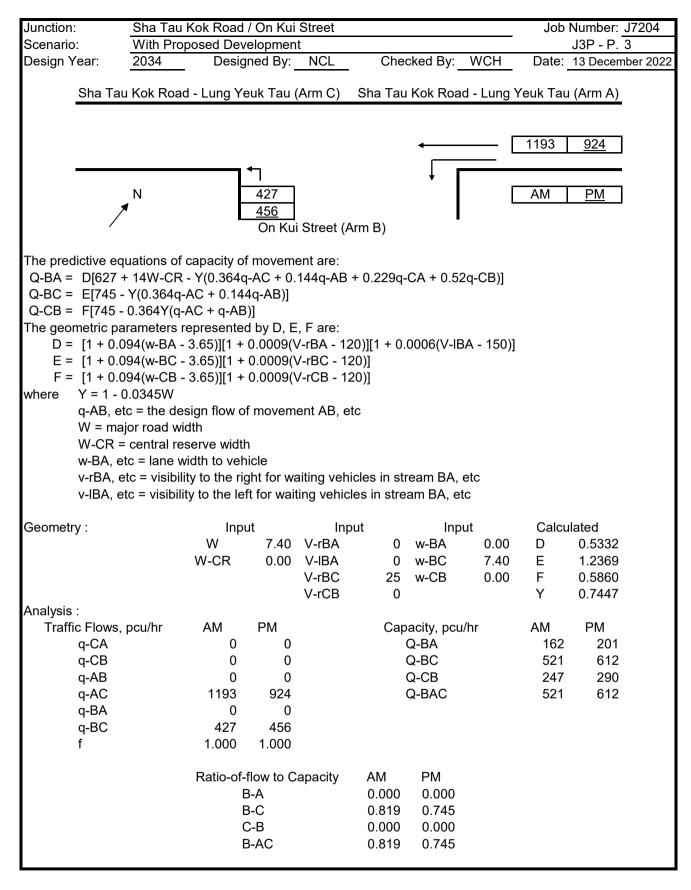
|        |                |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | x <sub>6</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.395          | 0.607 | 1.311          | 1.077 | 2241 | 0.683          | 1943  | 1967 | 1441       | 1403 | 0.742 | 0.713 |
| From B | 3.952          | 0.607 | 1.311          | 1.104 | 1197 | 0.493          | 642   | 629  | 83         | 135  | 0.129 | 0.214 |
| From C | 9.092          | 0.607 | 1.311          | 1.090 | 2755 | 0.776          | 2923  | 2878 | 1854       | 1733 | 0.634 | 0.602 |
| From D | 5.258          | 0.607 | 1.311          | 1.069 | 1593 | 0.565          | 526   | 566  | 0          | 0    | 0.000 | 0.000 |
| From E |                |       |                |       |      |                |       |      |            |      |       |       |
| From F |                |       |                |       |      |                |       |      |            |      |       |       |
| From G |                |       |                |       |      |                |       |      |            |      |       |       |
| From H |                |       |                |       |      |                |       |      |            |      |       |       |

| Junction:<br>Scenario:   | Sha Tau Kok<br>Existing Cond |         | a Sik Ro                             | ad         |               |            |                                      |           |                  |                       |                |            |                |                  | Job Nu          | mber:<br>J3 - P. |                |
|--------------------------|------------------------------|---------|--------------------------------------|------------|---------------|------------|--------------------------------------|-----------|------------------|-----------------------|----------------|------------|----------------|------------------|-----------------|------------------|----------------|
| Design Year:             |                              | Designe | ed By:                               |            | NCL           |            | <u>.</u>                             | Checke    | d By:            |                       | WCH            |            |                | Date:            | 13 De           | ecember          |                |
|                          | Approach                     |         | Phase                                | Stage      | Width (m)     | Radius (m) | % Up-hill<br>Gradient                | Turning % | Sat. Flow        | AM Peak<br>Flow       | y value        | Critical y | Turning %      | Sat. Flow        | PM Peak<br>Flow | y value          | Critical y     |
| Sha Tau Kok Road -       | Lung Yeuk Tau SB             | SA      | A1                                   | 2          | 3.20          |            | Gradient                             |           | (pcu/hr)<br>1935 | (pcu/hr)<br>532       | 0.275          |            |                | (pcu/hr)<br>1935 | (pcu/hr)<br>501 | 0.259            |                |
|                          |                              | SA+RT   | A2                                   | 2          | 3.20          | 26.00      |                                      | 0         | 2075             | 571                   | 0.275          |            | 10             | 2063             | 534             | 0.259            |                |
|                          |                              | RT      | A3                                   | 2          | 3.20          | 23.00      |                                      | 100       | 1948             | 476                   | 0.244          |            | 100            | 1948             | 504             | 0.259            |                |
| Ma Sik Road EB           |                              | LT      | B1                                   | 2,3        | 3.50          | 15.0       |                                      | 100       | 1786             | 613                   | 0.343          | 0.343      | 100            | 1786             | 649             | 0.363            | 0.363          |
|                          |                              | RT      | B2                                   | 3          | 3.50          | 20.0       |                                      | 100       | 1958             | 75                    | 0.038          |            | 100            | 1958             | 61              | 0.031            |                |
| Sha Tau Kok Road -       | Lung Yeuk Tau NB             | LT+SA   | C1                                   | 1          | 3.50          | 15.0       |                                      | 31        | 1906             | 230                   | 0.121          | 0.121      | 52             | 1868             | 251             | 0.134            | 0.134          |
|                          |                              | SA      | C2                                   | 1          | 3.50          |            |                                      |           | 2105             | 254                   | 0.121          |            |                | 2105             | 283             | 0.134            |                |
|                          |                              | SA      | C3                                   | 1          | 3.50          |            |                                      |           | 2105             | 254                   | 0.121          |            |                | 2105             | 283             | 0.134            |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
| pedestrian pha           | ise                          |         | D <sub>(P)</sub>                     | 1          |               |            | rossing                              |           | 5                |                       | GM +           | 8          |                | GM =             | 13              | sec              |                |
|                          |                              |         | E <sub>(P)</sub><br>F <sub>(P)</sub> | 3<br>2,3   |               |            | rossing<br>rossing                   |           | 5<br>5           |                       | GM +<br>GM +   | 10<br>9    |                | GM =             | 15<br>14        | sec<br>sec       |                |
|                          |                              |         | G <sub>(P)</sub>                     | 1          |               |            | rossing                              |           | 5                |                       | GM +           | 7          |                | GM =             | 12              | sec              |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  |                       |                |            |                |                  |                 |                  |                |
| AM Traffic Flow (pcu/hr) | )                            |         | N                                    | PM Traffic | Flow (pcu/hr) |            |                                      |           | N                | S=1940+               | 100(W–3.2      | 25) S=     | 2080+100       | )(W–3.25)        | Note:           |                  |                |
|                          |                              |         | 7                                    |            |               |            |                                      |           | 1                | S <sub>M</sub> =S+(1· |                |            |                | +(1+1.5f/r)      |                 |                  |                |
| 71<br>∱                  | 75                           | + 613   |                                      |            | 131           | 61         | <b></b>                              | 649       |                  |                       |                | ak Hour    |                | ak Hour          |                 |                  |                |
|                          | ► 666                        | 476     |                                      |            | 1             | 686        |                                      | 560       |                  | Sum y                 | 1+2,3<br>0.464 |            | 1+2,3<br>0.498 |                  |                 |                  |                |
|                          | 110                          | )3 ←    |                                      |            |               |            | 979                                  | ┥         |                  | L (s)                 | 13             |            | 13             |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  | C (s)                 | 136            |            | 136            |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  | practical y           | 0.814          |            | 0.814          |                  |                 |                  |                |
|                          |                              |         |                                      |            |               |            |                                      |           |                  | R.C. (%)              | 75%            |            | 64%            |                  |                 |                  |                |
| 1                        | <u>↓</u> ↓                   | 2       |                                      | ĥĻ         | B1            | 3          | B2<br><b>∢</b>                       | .↓        | B1               | 4                     |                |            |                | 5                |                 |                  |                |
|                          | D <sub>(p)</sub>             |         | F <sub>(p)</sub>                     |            |               | <b>_</b>   | E <sub>(p)</sub><br>F <sub>(p)</sub> |           |                  |                       |                |            |                |                  |                 |                  |                |
| *                        | τ                            |         |                                      |            | A3<br>▲       |            |                                      |           | т                |                       |                |            |                |                  |                 |                  |                |
| G <sub>(p)</sub>         | 고<br>고                       | _       |                                      | A2<br>A1   | ÷ 🛨           |            |                                      |           | ╷┸               |                       |                |            |                |                  |                 |                  |                |
| •                        |                              |         |                                      | A1         |               |            |                                      |           | r                |                       |                |            |                |                  |                 |                  |                |
| AM G =                   |                              |         | G =                                  |            | I/G =         |            | G =                                  |           | I/G =            |                       | G =            |            | I/G =          |                  | G =             |                  | I/G =          |
| G =                      |                              |         | G =<br>G =                           |            | I/G =         |            | G =<br>G =                           |           | I/G =            |                       | G =<br>G =     |            | I/G =          |                  | G =<br>G =      |                  | I/G =          |
| PM G =<br>G =            |                              |         | G =<br>G =                           |            | I/G =         |            | G =<br>G =                           |           | I/G =<br>I/G =   |                       | G =<br>G =     |            | I/G =<br>I/G = |                  | G =<br>G =      |                  | I/G =<br>I/G = |
| 0-                       |                              |         | 0.1                                  |            |               |            | 0-                                   |           |                  |                       | 5-             |            |                |                  | 0-              |                  |                |

# **Priority Junction Analysis**



# **Priority Junction Analysis**



| Junction:      |            | Jockey Cl    | ub Road / S | sha Tau Ko | k Road   |            |            | J     | ob Number: | J7204          |          |         |
|----------------|------------|--------------|-------------|------------|----------|------------|------------|-------|------------|----------------|----------|---------|
| Scenario:      |            | Existing C   | ondition    |            |          |            |            |       |            |                | J4 - P.  | 1       |
| Design Ye      | ear:       | 2022         | De          | signed By: | NCL      | CI         | hecked By: | WCH   | -          | Date:          | 13 Decem | ber 202 |
| AM Peak        |            |              |             |            |          |            |            |       |            |                |          |         |
| Arm            | To A       | To B         | To C        | To D       | To E     | To F       | To G       | To H  | Total      | q <sub>c</sub> | 1        |         |
| From A         | 15         | 84           | 794         | 296        |          |            |            |       | 1189       | 410            | 1        |         |
| From B         | 377        | 23           | 76          | 236        |          |            |            |       | 713        | 1265           |          |         |
| From C         | 717        | 115          | 39          | 121        |          |            |            |       | 991        | 1005           |          |         |
| From D         | 233        | 111          | 64          | 58         |          |            |            |       | 465        | 1286           |          |         |
| From E         |            |              |             |            |          |            |            |       |            |                |          |         |
| From F         |            |              |             |            |          |            |            |       |            |                |          |         |
| From G         |            |              |             |            |          |            |            |       |            |                |          |         |
| From H         |            |              |             |            |          |            |            |       |            |                |          |         |
| Total          | 1342       | 333          | 973         | 710        |          |            |            |       | 3357       |                |          |         |
| PM Peak<br>Arm | To A       | To B         | To C        | To D       | To E     | To F       | To G       | To H  | Total      | q <sub>c</sub> | ٦        |         |
| From A         | IUA        | 10.8         | 656         | 261        | IUL      | 101        | 10.0       | 1011  | 1021       | чс<br>471      | -        |         |
| From B         | 505        | 104<br>36    |             | 201<br>64  |          |            |            |       | 666        | 1053           |          |         |
| From C         | 505<br>651 | 30<br>174    | 61<br>39    | 64<br>74   |          |            |            |       | 938        | 897            |          |         |
| From D         | 255        | 174          | 39<br>67    | 74<br>31   |          |            |            |       | 930<br>477 | 097<br>1405    |          |         |
| From E         | 200        | 125          | 07          | 31         |          |            |            |       | 4//        | 1405           |          |         |
| From F         |            |              |             |            |          |            |            |       |            |                |          |         |
| From G         |            |              |             |            |          |            |            |       |            |                |          |         |
| From H         |            |              |             |            |          |            |            |       |            |                |          |         |
| Total          | 1411       | 439          | 822         | 430        |          |            |            |       | 3102       |                | 1        |         |
|                |            |              |             |            |          |            |            |       |            | 1              | 4        |         |
| Legend         |            |              |             |            | Geometri | c Paramete | ers        |       |            |                |          |         |
| Arm            | -          | (in clockwis | /           |            | Arm      | e (m)      | v (m)      | r (m) | L (m)      | D (m)          | Ø (°)    | S       |
| Α              | Sha Tau    | Kok Road -   | East        |            | From A   | 8.0        | 7.5        | 35.0  | 4.0        | 65             | 10       | 0.2     |
| D              | lookov O   | lub Dood     | Couth       |            | Crom D   | 75         | 70         | 25.0  | 10         | CE.            | 10       | 0.0     |

| AIIII | Road (III Clockwise older) |
|-------|----------------------------|
| А     | Sha Tau Kok Road - East    |
| В     | Jockey Club Road - South   |
| С     | Sha Tau Kok Road - West    |
| D     | Jockey Club Road - North   |
| Е     |                            |
| F     |                            |
| G     |                            |
| Н     |                            |

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 8.0   | 7.5   | 35.0  | 4.0   | 65    | 10    | 0.2 |
| From B | 7.5   | 7.0   | 25.0  | 1.0   | 65    | 10    | 0.8 |
| From C | 10.0  | 7.0   | 40.0  | 15.0  | 65    | 40    | 0.3 |
| From D | 8.5   | 8.0   | 60.0  | 2.0   | 65    | 20    | 0.4 |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$          | Entry Capacity                      |
|----------------|-------------------------------------|
| q <sub>c</sub> | Circulating Flow across the Entry   |
| К              | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F              | = 303x <sub>2</sub>                 |
| f <sub>c</sub> | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub> | = 1+0.5/(1+M)                       |
| М              | = exp[(D-60)/10]                    |
| x <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S              | = 1.6(e-v)/L                        |
|                |                                     |
|                |                                     |

#### Limitation

| e Entry Width 4.0 - 15.0 m                |  |
|---|--|
|   |  |
| v Approach Half Width 2.0 - 7.3 m         |  |
| r Entry Radius 6.0 - 100.0 m              |  |
| L Effective Length of Flare 1.0 - 100.0 m |  |
| D Inscribed Circle Diameter 15 - 100 m    |  |
| Ø Entry Angle 10° - 60°                   |  |
| S Sharpness of Flare 0.0 - 3.0            |  |

|        |                       |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|-----------------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | <b>x</b> <sub>2</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.857                 | 1.649 | 1.189          | 1.090 | 2381 | 0.642          | 2309  | 2266 | 1189       | 1021 | 0.515 | 0.450 |
| From B | 7.192                 | 1.649 | 1.189          | 1.079 | 2179 | 0.609          | 1521  | 1660 | 713        | 666  | 0.469 | 0.401 |
| From C | 8.829                 | 1.649 | 1.189          | 0.990 | 2675 | 0.690          | 1961  | 2035 | 991        | 938  | 0.505 | 0.461 |
| From D | 8.278                 | 1.649 | 1.189          | 1.067 | 2508 | 0.663          | 1767  | 1683 | 465        | 477  | 0.263 | 0.284 |
| From E |                       |       |                |       |      |                |       |      |            |      |       |       |
| From F |                       |       |                |       |      |                |       |      |            |      |       |       |
| From G |                       |       |                |       |      |                |       |      |            |      |       |       |
| From H |                       |       |                |       |      |                |       |      |            |      |       |       |

| Junction: |      | Jockey Cl | ub Road / S | Sha Tau Kok | Road |      |            |      |       | Jo             | b Number: J7204  |
|-----------|------|-----------|-------------|-------------|------|------|------------|------|-------|----------------|------------------|
| Scenario: |      | Without P | roposed De  | velopment   |      |      |            |      |       | _              | J4 - P. 2        |
| Design Ye | ar:  | 2034      | _ De        | signed By:  | NCL  | С    | hecked By: | WCH  |       | Date:          | 13 December 2022 |
| AM Peak   |      |           |             |             |      |      |            |      |       |                |                  |
| Arm       | To A | To B      | To C        | To D        | To E | To F | To G       | To H | Total | q <sub>c</sub> | 1                |
| From A    | 21   | 148       | 940         | 366         |      |      |            |      | 1475  | 490            |                  |
| From B    | 313  | 34        | 90          | 323         |      |      |            |      | 759   | 1527           |                  |
| From C    | 822  | 136       | 49          | 144         |      |      |            |      | 1150  | 1133           |                  |
| From D    | 278  | 121       | 74          | 77          |      |      |            |      | 550   | 1373           |                  |
| From E    |      |           |             |             |      |      |            |      |       |                |                  |
| From F    |      |           |             |             |      |      |            |      |       |                |                  |
| From G    |      |           |             |             |      |      |            |      |       |                |                  |
| From H    |      |           |             |             |      |      |            |      |       |                |                  |
| Total     | 1433 | 438       | 1153        | 910         |      |      |            |      | 3934  |                | 1                |
|           |      |           |             |             |      |      |            |      |       |                |                  |
| PM Peak   |      |           |             |             |      |      |            |      |       | -              | -                |
| Arm       | To A | To B      | To C        | To D        | To E | To F | To G       | To H | Total | q <sub>c</sub> |                  |
| From A    | 34   | 141       | 712         | 383         |      |      |            |      | 1270  | 596            |                  |
| From B    | 368  | 55        | 75          | 123         |      |      |            |      | 621   | 1325           |                  |
| From C    | 806  | 209       | 58          | 87          |      |      |            |      | 1160  | 1016           |                  |
| From D    | 282  | 136       | 85          | 52          |      |      |            |      | 555   | 1531           |                  |
| From E    |      |           |             |             |      |      |            |      |       |                |                  |
| From F    |      |           |             |             |      |      |            |      |       |                |                  |
| From G    |      |           |             |             |      |      |            |      |       |                |                  |
| From H    |      |           |             |             |      |      |            |      |       |                | J                |
| Total     | 1490 | 541       | 930         | 646         |      |      |            |      | 3607  |                |                  |

#### Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| А   | Sha Tau Kok Road - East   |
| В   | Jockey Club Road - South  |
| С   | Sha Tau Kok Road - West   |
| D   | Jockey Club Road - North  |
| Е   |                           |
| F   |                           |
| G   |                           |
| н   |                           |

## Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 8.0   | 7.5   | 35.0  | 4.0   | 65    | 10    | 0.2 |
| From B | 7.5   | 7.0   | 25.0  | 1.0   | 65    | 10    | 0.8 |
| From C | 10.0  | 7.0   | 40.0  | 15.0  | 65    | 40    | 0.3 |
| From D | 8.5   | 8.0   | 60.0  | 2.0   | 65    | 20    | 0.4 |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_{c}$               | Circulating Flow across the Entry   |
| К                     | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| f <sub>c</sub>        | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>        | = 1+0.5/(1+M)                       |
| М                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |
|                       |                                     |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |
|---|---------------------------|---------------|
| v | Approach Half Width       | 2.0 - 7.3 m   |
| r | Entry Radius              | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m    |
| Ø | Entry Angle               | 10° - 60°     |
| S | Sharpness of Flare        | 0.0 - 3.0     |

|        |                |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | X <sub>3</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.857          | 1.649 | 1.189          | 1.090 | 2381 | 0.642          | 2253  | 2178 | 1475       | 1270 | 0.655 | 0.583 |
| From B | 7.192          | 1.649 | 1.189          | 1.079 | 2179 | 0.609          | 1349  | 1481 | 759        | 621  | 0.563 | 0.420 |
| From C | 8.829          | 1.649 | 1.189          | 0.990 | 2675 | 0.690          | 1873  | 1953 | 1150       | 1160 | 0.614 | 0.594 |
| From D | 8.278          | 1.649 | 1.189          | 1.067 | 2508 | 0.663          | 1705  | 1594 | 550        | 555  | 0.322 | 0.348 |
| From E |                |       |                |       |      |                |       |      |            |      |       |       |
| From F |                |       |                |       |      |                |       |      |            |      |       |       |
| From G |                |       |                |       |      |                |       |      |            |      |       |       |
| From H |                |       |                |       |      |                |       |      |            |      |       |       |

| Junction:      |      | Jockey Clu | ub Road / S | Job Number: J7204 |      |      |            |      |       |       |                 |
|----------------|------|------------|-------------|-------------------|------|------|------------|------|-------|-------|-----------------|
| Scenario:      |      | With Prop  | osed Devel  | opment            |      |      |            |      |       |       | J4 - P. 3       |
| Design Ye      | ar:  | 2034       | De          | signed By:        | NCL  | C    | necked By: | WCH  |       | Date: | 13 December 202 |
| AM Peak        |      |            |             |                   |      |      |            |      |       |       |                 |
| Arm            | To A | To B       | To C        | To D              | To E | To F | To G       | To H | Total | dc    | 1               |
| From A         | 21   | 148        | 993         | 370               |      |      |            |      | 1532  | 490   |                 |
| From B         | 313  | 34         | 90          | 323               |      |      |            |      | 759   | 1584  |                 |
| From C         | 822  | 136        | 49          | 144               |      |      |            |      | 1150  | 1137  |                 |
| From D         | 278  | 121        | 74          | 77                |      |      |            |      | 550   | 1373  |                 |
| From E         |      |            |             |                   |      |      |            |      |       |       |                 |
| From F         |      |            |             |                   |      |      |            |      |       |       |                 |
| From G         |      |            |             |                   |      |      |            |      |       |       |                 |
| From H         |      |            |             |                   |      |      |            |      |       |       |                 |
| Total          | 1433 | 438        | 1206        | 914               |      |      |            |      | 3991  |       |                 |
| PM Peak<br>Arm | To A | To B       | To C        | To D              | To E | To F | To G       | To H | Total | qc    | 1               |
| From A         | 34   | 141        | 731         | 386               |      |      |            |      | 1292  | 596   |                 |
| From B         | 368  | 55         | 75          | 123               |      |      |            |      | 621   | 1347  |                 |
| From C         | 806  | 209        | 58          | 87                |      |      |            |      | 1160  | 1019  |                 |
| From D         | 282  | 136        | 85          | 52                |      |      |            |      | 555   | 1531  |                 |
| From E         |      |            |             |                   |      |      |            |      |       |       |                 |
| From F         |      |            |             |                   |      |      |            |      |       |       |                 |
| From G         |      |            |             |                   |      |      |            |      |       |       |                 |
| From H         |      |            |             |                   |      |      |            |      |       |       |                 |
|                | 1490 | 541        | 949         | 649               |      |      |            |      | 3629  |       |                 |

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| А   | Sha Tau Kok Road - East   |
| В   | Jockey Club Road - South  |
| С   | Sha Tau Kok Road - West   |
| D   | Jockey Club Road - North  |
| Е   |                           |
| F   |                           |
| G   |                           |
| Н   |                           |

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 8.0   | 7.5   | 35.0  | 4.0   | 65    | 10    | 0.2 |
| From B | 7.5   | 7.0   | 25.0  | 1.0   | 65    | 10    | 0.8 |
| From C | 10.0  | 7.0   | 40.0  | 15.0  | 65    | 40    | 0.3 |
| From D | 8.5   | 8.0   | 60.0  | 2.0   | 65    | 20    | 0.4 |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                                 |
|-----------------------|--|
| q <sub>c</sub>        | Circulating Flow across the Entry              |
| K<br>F                | = 1-0.00347(∅-30)-0.978[(1/r)-0.05]<br>= 303x₂ |
| f <sub>c</sub>        | $= 0.210t_{D}(1+0.2x_{2})$                     |
| t <sub>D</sub>        | = 1+0.5/(1+M)                                  |
| М                     | = exp[(D-60)/10]                               |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                               |
| S                     | = 1.6(e-v)/L                                   |
|                       |  |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |  |
|---|---------------------------|---------------|--|
| v | Approach Half Width       | 2.0 - 7.3 m   |  |
| r | Entry Radius              | 6.0 - 100.0 m |  |
| L | Effective Length of Flare | 1.0 - 100.0 m |  |
| D | Inscribed Circle Diameter | 15 - 100 m    |  |
| Ø | Entry Angle               | 10° - 60°     |  |
| S | Sharpness of Flare        | 0.0 - 3.0     |  |

|        |                |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | x <sub>6</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.857          | 1.649 | 1.189          | 1.090 | 2381 | 0.642          | 2253  | 2178 | 1532       | 1292 | 0.680 | 0.593 |
| From B | 7.192          | 1.649 | 1.189          | 1.079 | 2179 | 0.609          | 1311  | 1467 | 759        | 621  | 0.579 | 0.424 |
| From C | 8.829          | 1.649 | 1.189          | 0.990 | 2675 | 0.690          | 1871  | 1951 | 1150       | 1160 | 0.615 | 0.594 |
| From D | 8.278          | 1.649 | 1.189          | 1.067 | 2508 | 0.663          | 1705  | 1594 | 550        | 555  | 0.322 | 0.348 |
| From E |                |       |                |       |      |                |       |      |            |      |       |       |
| From F |                |       |                |       |      |                |       |      |            |      |       |       |
| From G |                |       |                |       |      |                |       |      |            |      |       |       |
| From H |                |       |                |       |      |                |       |      |            |      |       |       |

|  |                             |                                      |             |               | _          |                       |              |                       |                         |                |            |              |                        |                               |         |            |
|--|-----------------------------|--------------------------------------|-------------|---------------|------------|-----------------------|--------------|-----------------------|-------------------------|----------------|------------|--------------|------------------------|-------------------------------|---------|------------|
|  | key Club Road / Ma          | Sik Roa                              | ad / So I   | Kwun Po       | Road       |                       |              |                       |                         |                |            |              | -                      | Job Nu                        | mber:   |            |
| Scenario: <u>Exis</u><br>Design Year: <u>202</u> | sting Condition<br>2 Design | ed By:                               |             | NCL           |            | <u> </u>              | Checke       | d By:                 | WCH Date:               |                |            |              |                        | J5 - P. 1<br>13 December 2022 |         |            |
|  |                             |                                      |             |               |            |                       |              |                       | AM Peak                 |                |            |              |                        | PM Peak                       |         |            |
| Appr   | roach                       | Phase                                | Stage       | Width (m)     | Radius (m) | % Up-hill<br>Gradient | Turning %    | Sat. Flow<br>(pcu/hr) | Flow<br>(pcu/hr)        | y value        | Critical y | Turning %    | Sat. Flow<br>(pcu/hr)  | Flow<br>(pcu/hr)              | y value | Critical y |
| Jockey Club Road                                 | EB LT                       | A1                                   | 3           | 3.30          | 12.5       |                       | 100          | 1737                  | 90                      | 0.052          |            | 100          | 1737                   | 87                            | 0.050   |            |
| Jockey Club Road                                 | EB LT+SA                    | A2                                   | 3           | 3.30          | 15.0       |                       | 59           | 1969                  | 103                     | 0.052          |            | 87           | 1919                   | 97                            | 0.051   | 0.051      |
| Jockey Club Road                                 | EB SA                       | A3                                   | 3           | 3.30          |            |                       |              | 2085                  | 108                     | 0.052          |            |              | 2085                   | 104                           | 0.050   |            |
| Jockey Club Road                                 |                             | A4                                   | 3           | 3.30          | 27.5       |                       | 100          | 1977                  | 116                     | 0.059          | 0.059      | 100          | 1977                   | 92                            | 0.046   |            |
| Jockey Club Road                                 | EB RT                       | A5                                   | 3           | 3.30          | 25.0       |                       | 100          | 1967                  | 115                     | 0.059          |            | 100          | 1967                   | 91                            | 0.046   |            |
| So Kwun Po Road                                  | NB LT                       | B1                                   | 1, 2        | 4.60          | 45.0       |                       | 100          | 2008                  | 347                     | 0.173          |            | 100          | 2008                   | 417                           | 0.208   |            |
| So Kwun Po Road                                  | NB SA                       | B2                                   | 1           | 3.30          |            |                       |              | 2085                  | 419                     | 0.201          | 0.201      |              | 2085                   | 408                           | 0.195   | 0.195      |
| So Kwun Po Road                                  | NB SA+RT                    | В3                                   | 1           | 3.30          | 27.5       |                       | 0            | 2085                  | 419                     | 0.201          |            | 0            | 2085                   | 407                           | 0.195   |            |
| So Kwun Po Road                                  | NB RT                       | B4                                   | 1           | 3.30          | 25.0       |                       | 100          | 1967                  | 310                     | 0.157          |            | 100          | 1967                   | 291                           | 0.148   |            |
| Jookov Club Road                                 | WB LT                       | C1                                   | 2           | 3.30          | 25.0       |                       | 100          | 1835                  | 139                     | 0.076          |            | 100          | 1835                   | 122                           | 0.067   | 0.067      |
| Jockey Club Road                                 |                             | C1<br>C2                             | 2           | 3.30          | 25.0       |                       | 67           | 2012                  | 154                     | 0.076          | 0.077      | 59           | 2020                   | 122                           | 0.067   | 0.007      |
| Jockey Club Road                                 |                             | C3                                   | 2           | 3.30          | 21.5       |                       | 07           | 2012                  | 154                     | 0.077          | 0.077      | - 59         | 2020                   | 134                           | 0.000   |            |
| Jockey Club Road                                 |                             | C4                                   | 2           | 3.60          | 25.0       |                       | 100          | 1995                  | 121                     | 0.070          |            | 100          | 1995                   | 82                            | 0.007   |            |
| ,  |                             |                                      |             |               |            |                       |              |                       |                         |                |            |              |                        |                               |         |            |
| Ma Sik Road SB                                   | LT                          | D1                                   | 4           | 3.70          | 12.5       |                       | 100          | 1772                  | 68                      | 0.039          |            | 100          | 1772                   | 56                            | 0.031   |            |
| Ma Sik Road SB                                   | SA                          | D2                                   | 4           | 3.80          | 15.0       |                       |              | 2135                  | 388                     | 0.182          | 0.182      |              | 2135                   | 311                           | 0.146   |            |
| Ma Sik Road SB                                   | SA                          | D3                                   | 4           | 3.80          |            |                       |              | 2135                  | 389                     | 0.182          |            |              | 2135                   | 311                           | 0.146   |            |
| Ma Sik Road SB                                   | RT                          | D4                                   | 4           | 3.50          | 2.0        |                       | 100          | 1203                  | 191                     | 0.158          |            | 100          | 1203                   | 193                           | 0.160   | 0.160      |
| n edeetrien ubeen                                |                             | _                                    | 1           |               |            |                       |              | 5                     |                         |                | 10         |              | CM -                   | 15                            |         |            |
| pedestrian phase                                 |                             | E <sub>(p)</sub><br>F <sub>(p)</sub> | 2,3,4       |               |            | rossing               |              | 5<br>7                |                         | GM +<br>GM +   | 9          |              | GM =                   | 16                            | sec     |            |
|  |                             | G <sub>(p)</sub>                     | 2,3,4       |               |            | rossing<br>rossing    |              | 13                    |                         | GM +           | 9<br>14    |              | GM =                   | 27                            | sec     |            |
|  |                             | С <sub>(р)</sub><br>Н <sub>(р)</sub> | 3,4         |               |            | rossing               |              | 7                     |                         | GM +           | 7          |              | GM =                   | 14                            | sec     |            |
|  |                             | AF7                                  |             |               |            | Ţ                     |              |                       |                         |                |            |              |                        |                               |         |            |
|  |                             |                                      |             |               |            |                       |              |                       |                         |                |            |              |                        |                               |         |            |
|  |                             |                                      |             |               |            |                       |              |                       |                         |                |            |              |                        |                               |         |            |
|  |                             |                                      | DV T (* 1   |               |            |                       |              |                       |                         |                |            |              |                        |                               |         |            |
| AM Traffic Flow (pcu/hr)                         |                             | NK                                   | PM Trainc r | flow (pcu/hr) |            |                       |              | N<br>K                |                         | 100(W–3.2      |            | 2080+100     |                        | Note:                         |         |            |
|  |                             | $\backslash$                         |             |               | 100        |                       | 50           | $\setminus$           | S <sub>M</sub> =S÷(1∙   |                |            |              | ⊧(1+1.5f/r)<br>ak Hour |                               |         |            |
| 151  | 191 + 68                    |                                      |             | 171           | 193        | Ì                     | 00           |                       |                         | AM Pe          |            |              |                        |                               |         |            |
| 150  | 777<br>121                  |                                      |             | <u> </u>      | 117        | 622                   | 82           |                       |                         | 1+2+3+4        |            | 1+2+3+4      |                        |                               |         |            |
|  | 38 209                      |                                      |             |               | 815        | 194                   | $\mathbf{+}$ |                       | Sum y                   | 0.518          |            | 0.473        |                        |                               |         |            |
| 231 0  | · · · · •                   |                                      |             | 183           |            | 004                   | Ļ            |                       | L (s)                   | 27             |            | 27           |                        |                               |         |            |
| 347  | → 310 242                   |                                      |             | 417           | $\neg$     | 291                   | 201          |                       | C (s)                   | 116            |            | 116          |                        |                               |         |            |
|  |                             |                                      |             |               |            |                       |              |                       | practical y<br>R.C. (%) | 0.691<br>33%   |            | 0.691<br>46% |                        |                               |         |            |
| 1  | 2                           |                                      |             |               | 3          |                       | 1111         |                       | 4                       | 0070           |            |              | 5                      |                               |         |            |
| ┝╤╷╴╵╵   |                             |                                      | ∣∐կ         |               | -7         |                       | վ∐կ          |                       | ηf                      | D4             | ┥╽╽┕       | D1           | -                      |                               |         |            |
| G(p)   |                             |                                      |             |               |            |                       |              |                       |                         |                | D3 D2      |              |                        |                               |         |            |
|  | ▲<br>★ A5                   |                                      |             | <u> </u>      |            |                       |              | C4                    |                         |                |            | <u> </u>     |                        |                               |         |            |
| B2 B3  |                             | <b>∢</b> Εω∟                         | *           | F             | Hu         | .▼ <b>∢</b> Ē⊮L       | *            |                       | н                       | .▼ <b>∢</b> Ξω | *          | F            | -                      |                               |         |            |
| B1 <b>4</b>   → P B4                             | В1                          | זין                                  |             |               | رون<br>۲   | <u>httr</u>           |              | ▼<br>C1               | <b>*</b>                | <u>'</u> ]     |            |              |                        |                               |         |            |
| AM G =   | I/G =                       | G =                                  |             | I/G =         |            | G =                   |              | I/G =                 |                         | G =            |            | I/G =        |                        | G =                           |         | I/G =      |
| G =  | I/G =                       | G =                                  |             | I/G =         |            | G =                   |              | I/G =                 |                         | G =            |            | I/G =        |                        | G =                           |         | I/G =      |
| PM G =   | I/G =                       | G =                                  |             | I/G =         |            | G =                   |              | I/G =                 |                         | G =            |            | I/G =        |                        | G =                           |         | I/G =      |
| G =  | I/G =                       | G =                                  |             | I/G =         |            | G =                   |              | I/G =                 |                         | G =            |            | I/G =        |                        | G =                           |         | I/G =      |

| <b></b>                   |                      |                          |                        |              |              |                        |                            |           |                       |                       |               |                |             |                       |                  |                               |                |  |  |  |
|---------------------------|----------------------|--------------------------|------------------------|--------------|--------------|------------------------|----------------------------|-----------|-----------------------|-----------------------|---------------|----------------|-------------|-----------------------|------------------|-------------------------------|----------------|--|--|--|
| Junction:                 |                      | Club Road / Ma           |                        |              | Kwun Po      | Road                   |                            |           |                       |                       |               |                |             |                       | Job Nu           | mber:                         |                |  |  |  |
| Scenario:<br>Design Year: | 2034                 | Proposed Deve<br>Designe |                        |              | NCL          |                        | Checked By: WCH Date       |           |                       |                       |               |                |             |                       |                  | J5 - P. 2<br>13 December 2022 |                |  |  |  |
|                           |                      |                          |                        |              |              | 1                      | AM Peak                    |           |                       |                       |               |                |             |                       | PM Peak          |                               |                |  |  |  |
|                           | Approach             |                          | Phase                  | Stage        | Width (m)    | Radius (m)             | % Up-hill<br>Gradient      | Turning % | Sat. Flow<br>(pcu/hr) | Flow<br>(pcu/hr)      | y value       | Critical y     | Turning %   | Sat. Flow<br>(pcu/hr) | Flow<br>(pcu/hr) | y value                       | Critical y     |  |  |  |
| Jockey Club Ro            | oad EB               | LT                       | A1                     | 3            | 3.30         | 12.5                   |                            | 100       | 1737                  | 113                   | 0.065         | 0.065          | 100         | 1737                  | 102              | 0.059                         | 0.059          |  |  |  |
| Jockey Club Re            | oad EB               | LT+SA                    | A2                     | 3            | 3.30         | 15.0                   |                            | 55        | 1976                  | 129                   | 0.065         |                | 98          | 1899                  | 112              | 0.059                         |                |  |  |  |
| Jockey Club Re            | oad EB               | SA                       | A3                     | 3            | 3.30         |                        |                            |           | 2085                  | 135                   | 0.065         |                |             | 2085                  | 123              | 0.059                         |                |  |  |  |
| Jockey Club Ro            | oad EB               | RT                       | A4                     | 3            | 3.30         | 27.5                   |                            | 100       | 1977                  | 126                   | 0.064         |                | 100         | 1977                  | 100              | 0.050                         |                |  |  |  |
| Jockey Club Ro            | oad EB               | RT                       | A5                     | 3            | 3.30         | 25.0                   |                            | 100       | 1967                  | 125                   | 0.064         |                | 100         | 1967                  | 99               | 0.050                         |                |  |  |  |
| So Kwun Po R              | load NB              | LT                       | B1                     | 1, 2         | 4.60         | 45.0                   |                            | 100       | 2008                  | 387                   | 0.193         |                | 100         | 2008                  | 466              | 0.232                         |                |  |  |  |
| So Kwun Po R              | load NB              | SA                       | B2                     | 1            | 3.30         |                        |                            |           | 2085                  | 382                   | 0.183         | 0.183          |             | 2085                  | 386              | 0.185                         | 0.185          |  |  |  |
| So Kwun Po R              | load NB              | SA                       | B3                     | 1            | 3.30         |                        |                            |           | 2085                  | 382                   | 0.183         |                |             | 2085                  | 386              | 0.185                         |                |  |  |  |
| So Kwun Po R              | load NB              | SA+RT                    | B4                     | 1            | 3.30         | 27.5                   |                            | 0         | 2085                  | 382                   | 0.183         |                | 0           | 2085                  | 386              | 0.185                         |                |  |  |  |
| So Kwun Po R              | load NB              | RT                       | B5                     | 1            | 3.30         | 25.0                   |                            | 100       | 1967                  | 356                   | 0.181         |                | 100         | 1967                  | 348              | 0.177                         |                |  |  |  |
| Jockey Club Ro            | load WB              | LT                       | C1                     | 2            | 3.30         | 25.0                   |                            | 100       | 1835                  | 182                   | 0.099         |                | 100         | 1835                  | 163              | 0.089                         | 0.089          |  |  |  |
| Jockey Club Ro            |                      | LT+SA                    | C2                     | 2            | 3.30         | 27.5                   |                            | 73        | 2005                  | 200                   | 0.100         | 0.100          | 63          | 2016                  | 179              | 0.089                         | 0.000          |  |  |  |
| Jockey Club Ro            |                      | SA                       | C3                     | 2            | 3.30         |                        |                            |           | 2085                  | 207                   | 0.099         |                |             | 2085                  | 186              | 0.089                         |                |  |  |  |
| Jockey Club Ro            |                      | RT                       | C4                     | 2            | 3.60         | 25.0                   |                            | 100       | 1995                  | 135                   | 0.068         |                | 100         | 1995                  | 92               | 0.046                         |                |  |  |  |
|                           |                      |                          |                        |              |              |                        |                            |           |                       |                       |               |                |             |                       |                  |                               |                |  |  |  |
| Ma Sik Road S             |                      | LT                       | D1                     | 4            | 3.70         | 12.5                   |                            | 100       | 1772                  | 77                    | 0.044         |                | 100         | 1772                  | 63               | 0.035                         |                |  |  |  |
| Ma Sik Road S             |                      | LT+SA                    | D2                     | 4            | 3.80         | 15.0                   |                            | 0         | 2135                  | 518                   | 0.242         | 0.242          |             | 2135                  | 396              | 0.185                         | 0.185          |  |  |  |
| Ma Sik Road S             |                      | SA                       | D3                     | 4            | 3.80         |                        |                            |           | 2135                  | 518                   | 0.242         |                | 400         | 2135                  | 396              | 0.185                         |                |  |  |  |
| Ma Sik Road S             |                      | SA+RT                    | D4<br>E <sub>(p)</sub> | 4            | 3.50         | 2.0                    | roccing                    | 66        | 1407<br>5             | 341                   | 0.242<br>GM + | 10             | 103         | 1186<br>GM =          | 220<br>15        | 0.185<br>sec                  |                |  |  |  |
| pedestrian pha            | 150                  |                          | F <sub>(p)</sub>       | 2,3,4        |              |                        | rossing<br>rossing         |           | 7                     |                       | GM +          | 9              |             | GM =                  | 16               | sec                           |                |  |  |  |
|                           |                      |                          | G <sub>(p)</sub>       | 1            |              |                        | rossing                    |           | 13                    |                       | GM +          | 14             |             | GM =                  | 27               | sec                           |                |  |  |  |
|                           |                      |                          | H <sub>(p)</sub>       | 3,4          |              |                        | rossing                    |           | 7                     |                       | GM +          | 7              |             | GM =                  | 14               | sec                           |                |  |  |  |
|                           |                      |                          | (P)                    | - ,          |              |                        | 5                          |           |                       |                       | -             |                |             | -                     |                  |                               |                |  |  |  |
|                           |                      |                          |                        |              |              |                        |                            |           |                       |                       |               |                |             |                       |                  |                               |                |  |  |  |
|                           |                      |                          |                        |              |              |                        |                            |           |                       |                       |               |                |             |                       |                  |                               |                |  |  |  |
|                           |                      |                          |                        |              |              |                        |                            |           |                       |                       |               |                |             |                       |                  |                               |                |  |  |  |
| AM Traffic Flow (pcu/hr)  | .)                   |                          | N                      | PM Traffic F | low (pcu/hr) |                        |                            |           | N                     | S=1940+               | 100(W–3.2     | 25) S=         | 2080+100    | (W–3.25)              | Note:            |                               |                |  |  |  |
|                           |                      | 1                        | 5                      |              |              |                        | 1                          |           | 5                     | S <sub>M</sub> =S÷(1∙ | +1.5f/r)      | S <sub>M</sub> | =(S–230)+   | +(1+1.5f/r)           |                  |                               |                |  |  |  |
|                           | 225 🕈                |                          |                        |              |              | 227                    | ← →                        | 63        |                       |                       | AM Pe         | ak Hour        | PM Pe       | ak Hour               |                  |                               |                |  |  |  |
| 184<br><b>†</b>           |                      | 1151                     |                        |              | 212<br>1     |                        | 784                        |           |                       |                       | 1+2+3+4       |                | 1+2+3+4     |                       |                  |                               |                |  |  |  |
| │                         | ▶ 193                | 135<br>1                 |                        |              |              | 125                    |                            | 92<br>1   |                       | Sum y                 | 0.590         |                | 0.518       |                       |                  |                               |                |  |  |  |
| ¥<br>251                  | 1152<br>1            | 261                      |                        |              | <b>1</b> 99  | 1157<br><b>†</b>       | 252                        | +         |                       | L (s)                 | 27            |                | 27          |                       |                  |                               |                |  |  |  |
| 387                       | / ← 🔶 3              | 356 328                  |                        |              | 466          | ←   →                  | 348                        | 276       |                       | C (s)                 | 116           |                | 116         |                       |                  |                               |                |  |  |  |
|                           | I                    |                          |                        |              |              | I                      |                            |           |                       | practical y           | 0.691         |                | 0.691       |                       |                  |                               |                |  |  |  |
|                           |                      |                          |                        |              |              |                        |                            |           |                       | R.C. (%)              | 17%           |                | 33%         |                       |                  |                               |                |  |  |  |
| 1                         | 7114                 | 2                        |                        | ,   կ        |              | 3                      |                            | վ∐կ       |                       | 4                     | D4            |                | D1          | 5                     |                  |                               |                |  |  |  |
|                           |                      | A1                       |                        |              |              | Η                      |                            |           |                       | Ц                     |               |                |             |                       |                  |                               |                |  |  |  |
| G <sub>(p)</sub>          |                      | → A3                     |                        |              |              |                        |                            |           | C4                    |                       |               |                |             |                       |                  |                               |                |  |  |  |
|                           |                      | ▲ ★ A5                   |                        |              | ļ            | 1                      |                            |           | сз 📥                  | 1                     |               |                | Ļ           |                       |                  |                               |                |  |  |  |
| B2 B3                     | < <sup>E</sup> (p)-→ | 4                        | 4 <u></u> Γω           | *            | Ę.           | H <sub>@F</sub>        | .▼ <u>4</u> <sup>F</sup> ∞ | *         | C2                    | H <sub>(p)</sub> .    | .▼ <u></u>    | •              | -<br>-      |                       |                  |                               |                |  |  |  |
| B1 <b>4</b>               | ▶ B4                 | B1                       | ┑┦╿┍                   |              |              | <b>*</b> <sup>**</sup> | 'nיּדןי                    |           | C1                    | <b>*</b> -*           | 'nקני         |                |             |                       |                  |                               |                |  |  |  |
| AM G =                    |                      | I/G =                    | G =                    |              | I/G =        |                        | G =                        |           | I/G =                 |                       | G =           |                | I/G =       |                       | G =              |                               | I/G =          |  |  |  |
| G =                       |                      | I/G =                    | G =                    |              | I/G =        |                        | G =                        |           | I/G =                 |                       | G =           |                | I/G =       |                       | G =              |                               | I/G =          |  |  |  |
| PM G =<br>G =             |                      | I/G =                    | G =<br>G =             |              | I/G =        |                        | G =<br>G =                 |           | I/G =<br>I/G =        |                       | G =<br>G =    |                | I/G =       |                       | G =<br>G =       |                               | I/G =<br>I/G = |  |  |  |
| 0-                        |                      |                          | 0-                     |              | 10-          |                        | 0-                         |           | 10-                   |                       | 0-            |                | <i>"</i> 0- |                       | 0-               |                               |                |  |  |  |

| r                         |                  |                          |                  |              |                 | -                |                 |           |                  |                       |                             |                |           |                  |                 |                               |            |  |  |
|---------------------------|------------------|--------------------------|------------------|--------------|-----------------|------------------|-----------------|-----------|------------------|-----------------------|-----------------------------|----------------|-----------|------------------|-----------------|-------------------------------|------------|--|--|
| Junction:                 |                  | Club Road / Ma           |                  | ad / So I    | Kwun Po         | Road             |                 |           |                  |                       |                             |                |           |                  | Job Nu          | mber:                         |            |  |  |
| Scenario:<br>Design Year: |                  | posed Develop<br>Designe |                  |              | NCL             |                  |                 | Checke    | d Bv             |                       | WCH Date:                   |                |           |                  |                 | J5 - P. 3<br>13 December 2022 |            |  |  |
| Dooigit Four              |                  | Doolgin                  | <i></i>          |              |                 |                  |                 |           |                  |                       |                             |                |           |                  |                 |                               |            |  |  |
|                           | Approach         |                          | Phase            | Stage        | Width (m)       | Radius (m)       | % Up-hill       | Turning % | Sat. Flow        | AM Peak<br>Flow       | y value                     | Critical y     | Turning % | Sat. Flow        | PM Peak<br>Flow | y value                       | Critical y |  |  |
| Jockey Club R             |                  | LT                       | A1               | 3            | 3.30            | 12.5             | Gradient        | 100       | (pcu/hr)<br>1737 | (pcu/hr)<br>114       | 0.066                       |                | 100       | (pcu/hr)<br>1737 | (pcu/hr)<br>104 | 0.060                         |            |  |  |
| Jockey Club R             |                  | LT+SA                    | A1<br>A2         | 3            | 3.30            | 12.5             |                 | 57        | 1973             | 131                   | 0.066                       |                | 100       | 1895             | 114             | 0.060                         |            |  |  |
| Jockey Club R             |                  | SA                       | A2<br>A3         | 3            | 3.30            | 15.0             |                 | 57        | 2085             | 137                   | 0.066                       |                | 100       | 2085             | 125             | 0.060                         |            |  |  |
| Jockey Club R             |                  | RT                       | A4               | 3            | 3.30            | 27.5             |                 | 100       | 1977             | 126                   | 0.064                       |                | 100       | 1977             | 100             | 0.050                         |            |  |  |
| Jockey Club R             |                  | RT                       | A5               | 3            | 3.30            | 25.0             |                 | 100       | 1967             | 125                   | 0.064                       |                | 100       | 1967             | 99              | 0.050                         |            |  |  |
|                           |                  |                          | 7.0              |              | 0.00            | 20.0             |                 |           |                  | .20                   | 0.001                       |                |           |                  |                 | 0.000                         |            |  |  |
| So Kwun Po R              | Road NB          | LT                       | B1               | 1, 2         | 4.60            | 45.0             |                 | 100       | 2008             | 387                   | 0.193                       |                | 100       | 2008             | 466             | 0.232                         |            |  |  |
| So Kwun Po R              |                  | SA                       | B2               | 1            | 3.30            |                  |                 |           | 2085             | 389                   | 0.187                       |                |           | 2085             | 399             | 0.191                         |            |  |  |
| So Kwun Po R              |                  | SA                       | B3               | 1            | 3.30            |                  |                 |           | 2085             | 389                   | 0.187                       |                |           | 2085             | 399             | 0.191                         |            |  |  |
| So Kwun Po R              | Road NB          | SA+RT                    | B4               | 1            | 3.30            | 27.5             |                 | 0         | 2085             | 389                   | 0.187                       |                | 0         | 2085             | 399             | 0.191                         |            |  |  |
| So Kwun Po R              | Road NB          | RT                       | B5               | 1            | 3.30            | 25.0             |                 |           | 1967             | 356                   | 0.181                       |                |           | 1967             | 348             | 0.177                         |            |  |  |
|                           |                  |                          |                  |              |                 |                  |                 |           |                  |                       |                             |                |           |                  |                 |                               |            |  |  |
| Jockey Club R             | Road WB          | LT                       | C1               | 2            | 3.30            | 25.0             |                 | 100       | 1835             | 184                   | 0.100                       |                | 100       | 1835             | 164             | 0.089                         |            |  |  |
| Jockey Club R             | Road WB          | LT+SA                    | C2               | 2            | 3.30            | 27.5             |                 |           | 2006             | 200                   | 0.100                       |                |           | 2016             | 180             | 0.089                         |            |  |  |
| Jockey Club R             | Road WB          | SA                       | C3               | 2            | 3.30            |                  |                 | 0         | 2085             | 209                   | 0.100                       |                | 0         | 2085             | 187             | 0.089                         |            |  |  |
| Jockey Club R             | Road WB          | RT                       | C4               | 2            | 3.60            | 25.0             |                 |           | 1995             | 135                   | 0.068                       |                |           | 1995             | 92              | 0.046                         |            |  |  |
|                           |                  |                          |                  |              |                 |                  |                 | 0         |                  |                       |                             |                | 0         |                  |                 |                               |            |  |  |
| Ma Sik Road S             | SB               | LT                       | D1               | 4            | 3.70            | 12.5             |                 |           | 1772             | 77                    | 0.044                       |                |           | 1772             | 63              | 0.035                         |            |  |  |
| Ma Sik Road S             | SB               | LT+SA                    | D2               | 4            | 3.80            | 15.0             |                 |           | 2135             | 518                   | 0.242                       |                |           | 2135             | 396             | 0.185                         |            |  |  |
| Ma Sik Road S             | SB               | SA                       | D3               | 4            | 3.80            |                  |                 | 0         | 2135             | 518                   | 0.242                       |                | 0         | 2135             | 396             | 0.185                         |            |  |  |
| Ma Sik Road S             | SB               | SA+RT                    | D4               | 4            | 3.50            | 2.0              |                 |           | 1408             | 341                   | 0.242                       |                |           | 1186             | 220             | 0.185                         |            |  |  |
| pedestrian pha            | ase              |                          | E <sub>(p)</sub> | 1            |                 | min c            | rossing         | time =    | 5                | sec                   | GM +                        | 10             | sec F     | GM =             | 15              | sec                           |            |  |  |
|                           |                  |                          | F <sub>(p)</sub> | 2,3,4        |                 | min c            | rossing         | time =    | 7                | sec                   | GM +                        | 9              | sec F     | GM =             | 16              | sec                           |            |  |  |
|                           |                  |                          | G <sub>(p)</sub> | 1            |                 | min c            | rossing         | time =    | 13               | sec                   | GM +                        | 14             | sec F     | GM =             | 27              | sec                           |            |  |  |
|                           |                  |                          | H <sub>(p)</sub> | 3,4          |                 | min c            | rossing         | time =    | 7                | sec                   | GM +                        | 7              | sec F     | GM =             | 14              | sec                           |            |  |  |
|                           |                  |                          |                  |              |                 |                  |                 |           |                  |                       |                             |                |           |                  |                 |                               |            |  |  |
|                           |                  |                          |                  |              |                 |                  |                 |           |                  |                       |                             |                |           |                  |                 |                               |            |  |  |
|                           |                  |                          |                  |              |                 |                  |                 |           |                  |                       |                             |                |           |                  |                 |                               |            |  |  |
|                           |                  |                          |                  |              |                 |                  |                 |           |                  |                       |                             |                |           |                  |                 |                               |            |  |  |
| AM Traffic Flow (pcu/hr   | r)               |                          | N                | PM Traffic F | flow (pcu/hr)   |                  |                 |           | N                | S=1940+               | 100(W–3.2                   | 25) S=         | 2080+100  | (W–3.25)         | Note:           |                               |            |  |  |
|                           |                  | I                        | 5                |              |                 |                  | I.              |           | $\overline{\}$   | S <sub>M</sub> =S÷(1∙ | +1.5f/r)                    | S <sub>M</sub> | =(S–230)+ | +(1+1.5f/r)      |                 |                               |            |  |  |
|                           | 225 <            | 77                       |                  |              |                 | 227              |                 | 63        | -                |                       | AM Pe                       | ak Hour        | PM Pe     | ak Hour          |                 |                               |            |  |  |
| 189<br><b>†</b>           |                  | <b>♦</b><br>1151         |                  |              | 217<br>1        |                  | <b>♦</b><br>784 |           |                  |                       | 1+2+3+4                     |                | 1+2+3+4   |                  |                 |                               |            |  |  |
| │ — <del> </del> →        | ▶ 193            | 135<br>†                 |                  |              | $\rightarrow$   | 125              |                 | 92<br>1   |                  | Sum y                 | 0.596                       |                | 0.526     |                  |                 |                               |            |  |  |
| <b>♦</b><br>251           | 1180<br>•        | 265 🗲 🗕                  |                  |              | <b>♦</b><br>199 | 1197<br><b>†</b> | 255             | -         |                  | L (s)                 | 27                          |                | 27        |                  |                 |                               |            |  |  |
| 387                       | 7 ← 🔶 3          | <b>♦</b><br>356 328      |                  |              | 466             | ←                | 348             | ¥<br>276  |                  | C (s)                 | 116                         |                | 116       |                  |                 |                               |            |  |  |
|                           | I                |                          |                  |              |                 | I                |                 |           |                  | practical y           | 0.691                       |                | 0.691     |                  |                 |                               |            |  |  |
|                           |                  |                          |                  |              |                 |                  |                 |           |                  | R.C. (%)              | 16%                         |                | 31%       |                  |                 |                               |            |  |  |
| 1                         |                  | 2                        |                  |              |                 | 3                |                 | վկ        |                  | 4                     |                             |                |           | 5                |                 |                               |            |  |  |
| 노                         | PTT 4            | A1 43                    |                  | ۲T ۹         |                 | Η                |                 | PILA      |                  | ЪЧ                    | D4                          | ₄↓↓↓           | D1        |                  |                 |                               |            |  |  |
| G <sub>(p)</sub>          |                  |                          |                  |              |                 | -i               |                 |           | 64               | Ľ,                    |                             | D3 D2          |           |                  |                 |                               |            |  |  |
|                           |                  | ¥Ã5                      |                  |              | F               | -                |                 |           | c3 €             | -                     |                             |                | F         |                  |                 |                               |            |  |  |
| B2 B3<br>▲ ▲              | E <sub>(p)</sub> | μ                        | <b>∢</b> Е́µ∟    | *            | μ               |                  | .▼ <b>∢</b> Fωι | *         |                  |                       | . <b>ν 4</b> <sup>F</sup> ω | *              | Н         |                  |                 |                               |            |  |  |
| B1◀┃┝▶ſ                   | ► B4             | B1                       | 'nſŤſ⁺           |              |                 | ¤ <sup>(p)</sup> | 'nיּדָׂדָי      |           | ♥<br>C1          | <b>▲</b>              | ካቸፐ                         |                |           |                  |                 |                               |            |  |  |
| AM G=                     |                  | I/G =                    | G =              |              | I/G =           |                  | G =             |           | I/G =            |                       | G =                         |                | I/G =     |                  | G =             |                               | I/G =      |  |  |
| G =                       |                  | 1/G =                    | G =              |              | I/G =           |                  | G =             |           | 1/G =            |                       | G =                         |                | I/G =     |                  | G =             |                               | I/G =      |  |  |
| PM G=                     |                  | I/G =                    | G =              |              | I/G =           |                  | G =             |           | /G =             |                       | G =                         |                | I/G =     |                  | G =             |                               | I/G =      |  |  |
| G =                       |                  | 1/G =                    | G =              |              | I/G =           |                  | G =             |           | /G =             |                       | G =                         |                | I/G =     |                  | G =             |                               | I/G =      |  |  |
| Ű                         |                  |                          | -                |              |                 |                  | -               |           |                  |                       | -                           |                |           |                  | -               |                               | -          |  |  |

| Junction:    |      | So Kwun I        | Po Road / F | Job Number: <u>J7204</u><br>J6 - P. 1 |                     |      |      |       |                  |                |  |
|--------------|------|------------------|-------------|---------------------------------------|---------------------|------|------|-------|------------------|----------------|--|
| Scenario:    |      | Existing C       | ondition    |                                       |                     |      |      |       |                  |                |  |
| Design Year: |      | 2022 Designed By |             | esigned By:                           | NCL Checked By: WCH |      | -    | Date: | 13 December 2022 |                |  |
| AM Peak      |      |                  |             |                                       |                     |      |      |       |                  |                |  |
| Arm          | To A | To B             | To C        | To D                                  | To E                | To F | To G | To H  | Total            | q <sub>c</sub> |  |
| From A       | 59   |                  | 359         | 1144                                  |                     |      |      |       | 1561             | 550            |  |
| From B       | 427  |                  |             |                                       |                     |      |      |       | 427              | 1812           |  |
| From C       | 396  | 299              |             |                                       |                     |      |      |       | 695              | 1630           |  |
| From D       |      |                  | 251         |                                       |                     |      |      |       | 251              | 1181           |  |
| From E       |      |                  |             |                                       |                     |      |      |       |                  |                |  |
| From F       |      |                  |             |                                       |                     |      |      |       |                  |                |  |
| From G       |      |                  |             |                                       |                     |      |      |       |                  |                |  |
| From H       |      |                  |             |                                       |                     |      |      |       |                  |                |  |
| Total        | 882  | 299              | 609         | 1144                                  |                     |      |      |       | 2934             |                |  |

#### PM Peak

| Arm    | To A | To B | To C | To D | To E | To F | To G | To H | Total | q <sub>c</sub> |
|--------|------|------|------|------|------|------|------|------|-------|----------------|
| From A | 3    |      | 567  | 981  |      |      |      |      | 1550  | 575            |
| From B | 572  |      |      |      |      |      |      |      | 572   | 1863           |
| From C | 476  | 261  |      |      |      |      |      |      | 738   | 1556           |
| From D |      |      | 313  |      |      |      |      |      | 313   | 1313           |
| From E |      |      |      |      |      |      |      |      |       |                |
| From F |      |      |      |      |      |      |      |      |       |                |
| From G |      |      |      |      |      |      |      |      |       |                |
| From H |      |      |      |      |      |      |      |      |       |                |
| Total  | 1051 | 261  | 880  | 981  |      |      |      |      | 3173  |                |

#### Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| А   | So Kwun Po Road - North   |
| В   | Fanling Highway - East    |
| С   | So Kwun Po Road - South   |
| D   | Fanling Highway - West    |
| Е   |                           |
| F   |                           |
| G   |                           |
| н   |                           |

## Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 9.5   | 6.0   | 20.0  | 12.0  | 65    | 55    | 0.5 |
| From B | 7.0   | 3.5   | 90.0  | 34.0  | 65    | 25    | 0.2 |
| From C | 9.0   | 6.9   | 30.0  | 17.0  | 65    | 35    | 0.2 |
| From D | 7.5   | 3.5   | 55.0  | 19.0  | 65    | 30    | 0.3 |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_{c}$               | Circulating Flow across the Entry   |
| К                     | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| $f_{c}$               | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>        | = 1+0.5/(1+M)                       |
| М                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |
|                       |                                     |

#### Limitation

| e Entry Width 4.0 - 15.0 m                |  |
|---|--|
|   |  |
| v Approach Half Width 2.0 - 7.3 m         |  |
| r Entry Radius 6.0 - 100.0 m              |  |
| L Effective Length of Flare 1.0 - 100.0 m |  |
| D Inscribed Circle Diameter 15 - 100 m    |  |
| Ø Entry Angle 10° - 60°                   |  |
| S Sharpness of Flare 0.0 - 3.0            |  |

|        |                       |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|-----------------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | <b>x</b> <sub>2</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.810                 | 1.649 | 1.189          | 0.913 | 2367 | 0.640          | 1840  | 1826 | 1561       | 1550 | 0.848 | 0.849 |
| From B | 6.133                 | 1.649 | 1.189          | 1.055 | 1858 | 0.556          | 898   | 868  | 427        | 572  | 0.476 | 0.659 |
| From C | 8.405                 | 1.649 | 1.189          | 0.999 | 2547 | 0.669          | 1454  | 1504 | 695        | 738  | 0.478 | 0.491 |
| From D | 5.890                 | 1.649 | 1.189          | 1.031 | 1785 | 0.544          | 1178  | 1104 | 251        | 313  | 0.213 | 0.284 |
| From E |                       |       |                |       |      |                |       |      |            |      |       |       |
| From F |                       |       |                |       |      |                |       |      |            |      |       |       |
| From G |                       |       |                |       |      |                |       |      |            |      |       |       |
| From H |                       |       |                |       |      |                |       |      |            |      |       |       |

| Junction:    |      | So Kwun I         | Po Road / F | Job Number: <u>J7204</u><br>J6 - P. 2 |      |                     |      |      |       |                |                  |
|--------------|------|-------------------|-------------|---------------------------------------|------|---------------------|------|------|-------|----------------|------------------|
| Scenario:    |      | Without Pr        | roposed De  |                                       |      |                     |      |      |       |                |                  |
| Design Year: |      | 2034 Designed By: |             | signed By:                            | NCL  | NCL Checked By: WCH |      |      |       |                | 13 December 2022 |
| AM Peak      |      |                   |             |                                       |      |                     |      |      |       |                |                  |
| Arm          | To A | To B              | To C        | To D                                  | To E | To F                | To G | To H | Total | q <sub>c</sub> |                  |
| From A       | 24   |                   | 128         | 1228                                  |      |                     |      |      | 1380  | 631            |                  |
| From B       | 491  |                   |             |                                       |      |                     |      |      | 491   | 1693           |                  |
| From C       | 172  | 318               |             |                                       |      |                     |      |      | 490   | 1743           |                  |
| From D       |      |                   | 313         |                                       |      |                     |      |      | 313   | 1005           |                  |
| From E       |      |                   |             |                                       |      |                     |      |      |       |                |                  |
| From F       |      |                   |             |                                       |      |                     |      |      |       |                |                  |
| From G       |      |                   |             |                                       |      |                     |      |      |       |                |                  |
| From H       |      |                   |             |                                       |      |                     |      |      |       |                |                  |
| Total        | 687  | 318               | 441         | 1228                                  |      |                     |      |      | 2674  |                |                  |

## PM Peak

| Arm    | To A | To B | To C | To D | To E | To F | To G | To H | Total | q <sub>c</sub> |
|--------|------|------|------|------|------|------|------|------|-------|----------------|
| From A | 27   |      | 273  | 1070 |      |      |      |      | 1369  | 638            |
| From B | 654  |      |      |      |      |      |      |      | 654   | 1739           |
| From C | 207  | 268  |      |      |      |      |      |      | 475   | 1750           |
| From D |      |      | 370  |      |      |      |      |      | 370   | 1155           |
| From E |      |      |      |      |      |      |      |      |       |                |
| From F |      |      |      |      |      |      |      |      |       |                |
| From G |      |      |      |      |      |      |      |      |       |                |
| From H |      |      |      |      |      |      |      |      |       |                |
| Total  | 887  | 268  | 643  | 1070 |      |      |      |      | 2868  |                |

#### Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| Α   | So Kwun Po Road - North   |
| В   | Fanling Highway - East    |
| С   | So Kwun Po Road - South   |
| D   | Fanling Highway - West    |
| Е   |                           |
| F   |                           |
| G   |                           |
| Н   |                           |

## Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
|--------|-------|-------|-------|-------|-------|-------|-----|
| From A | 9.5   | 6.0   | 20.0  | 12.0  | 65    | 55    | 0.5 |
| From B | 7.0   | 3.5   | 90.0  | 34.0  | 65    | 25    | 0.2 |
| From C | 9.0   | 6.9   | 30.0  | 17.0  | 65    | 35    | 0.2 |
| From D | 7.5   | 3.5   | 55.0  | 19.0  | 65    | 30    | 0.3 |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_{c}$               | Circulating Flow across the Entry   |
| К                     | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| f <sub>c</sub>        | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>        | = 1+0.5/(1+M)                       |
| М                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |
|                       |                                     |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |  |
|---|---------------------------|---------------|--|
| v | Approach Half Width       | 2.0 - 7.3 m   |  |
| r | Entry Radius              | 6.0 - 100.0 m |  |
| L | Effective Length of Flare | 1.0 - 100.0 m |  |
| D | Inscribed Circle Diameter | 15 - 100 m    |  |
| Ø | Entry Angle               | 10° - 60°     |  |
| S | Sharpness of Flare        | 0.0 - 3.0     |  |

|        |                |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | x <sub>3</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.810          | 1.649 | 1.189          | 0.913 | 2367 | 0.640          | 1793  | 1789 | 1380       | 1369 | 0.770 | 0.766 |
| From B | 6.133          | 1.649 | 1.189          | 1.055 | 1858 | 0.556          | 968   | 941  | 491        | 654  | 0.507 | 0.695 |
| From C | 8.405          | 1.649 | 1.189          | 0.999 | 2547 | 0.669          | 1379  | 1374 | 490        | 475  | 0.355 | 0.346 |
| From D | 5.890          | 1.649 | 1.189          | 1.031 | 1785 | 0.544          | 1277  | 1193 | 313        | 370  | 0.245 | 0.310 |
| From E |                |       |                |       |      |                |       |      |            |      |       |       |
| From F |                |       |                |       |      |                |       |      |            |      |       |       |
| From G |                |       |                |       |      |                |       |      |            |      |       |       |
| From H |                |       |                |       |      |                |       |      |            |      |       |       |

| Junction: |      |           | Po Road / F |            | Job Number: J7204 |      |            |      |       |       |                  |
|-----------|------|-----------|-------------|------------|-------------------|------|------------|------|-------|-------|------------------|
| Scenario: |      | With Prop | osed Devel  |            | J6 - P. 3         |      |            |      |       |       |                  |
| Design Ye | ear: | 2034      | _ De        | signed By: | NCL               | C    | hecked By: | WCH  |       | Date: | 13 December 2022 |
| AM Peak   |      |           |             |            |                   |      |            |      |       |       |                  |
| Arm       | To A | To B      | To C        | To D       | To E              | To F | To G       | To H | Total | qc    | 1                |
| From A    | 24   |           | 128         | 1281       |                   |      |            |      | 1433  | 631   |                  |
| From B    | 491  |           |             |            |                   |      |            |      | 491   | 1746  |                  |
| From C    | 172  | 318       |             |            |                   |      |            |      | 490   | 1796  |                  |
| From D    |      |           | 313         |            |                   |      |            |      | 313   | 1005  |                  |
| From E    |      |           |             |            |                   |      |            |      |       |       |                  |
| From F    |      |           |             |            |                   |      |            |      |       |       |                  |
| From G    |      |           |             |            |                   |      |            |      |       |       |                  |
| From H    |      |           |             |            |                   |      |            |      |       |       |                  |
| Total     | 687  | 318       | 441         | 1281       |                   |      |            |      | 2727  |       |                  |

| РМ | Peak |
|----|------|
|    |      |

| Arm    | To A | To B | To C | To D | To E | To F | To G | To H | Total | qc   |
|--------|------|------|------|------|------|------|------|------|-------|------|
| From A | 27   |      | 273  | 1089 |      |      |      |      | 1388  | 638  |
| From B | 654  |      |      |      |      |      |      |      | 654   | 1758 |
| From C | 207  | 268  |      |      |      |      |      |      | 475   | 1769 |
| From D |      |      | 370  |      |      |      |      |      | 370   | 1155 |
| From E |      |      |      |      |      |      |      |      |       |      |
| From F |      |      |      |      |      |      |      |      |       |      |
| From G |      |      |      |      |      |      |      |      |       |      |
| From H |      |      |      |      |      |      |      |      |       |      |
| Total  | 887  | 268  | 643  | 1089 |      |      |      |      | 2887  |      |

## Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| А   | So Kwun Po Road - North   |
| В   | Fanling Highway - East    |
| С   | So Kwun Po Road - South   |
| D   | Fanling Highway - West    |
| Е   |                           |
| F   |                           |
| G   |                           |
| н   |                           |

## Geometric Parameters

|        |       | -     |       |       |       |       |     |
|--------|-------|-------|-------|-------|-------|-------|-----|
| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
| From A | 9.5   | 6.0   | 20.0  | 12.0  | 65    | 55    | 0.5 |
| From B | 7.0   | 3.5   | 90.0  | 34.0  | 65    | 25    | 0.2 |
| From C | 9.0   | 6.9   | 30.0  | 17.0  | 65    | 35    | 0.2 |
| From D | 7.5   | 3.5   | 55.0  | 19.0  | 65    | 30    | 0.3 |
| From E |       |       |       |       |       |       |     |
| From F |       |       |       |       |       |       |     |
| From G |       |       |       |       |       |       |     |
| From H |       |       |       |       |       |       |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_{c}$               | Circulating Flow across the Entry   |
| К                     | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| $f_{c}$               | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>        | = 1+0.5/(1+M)                       |
| М                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |
|                       |                                     |

#### Limitation

| e Entry Width 4.0 - 15.0 m                |  |
|---|--|
|   |  |
| v Approach Half Width 2.0 - 7.3 m         |  |
| r Entry Radius 6.0 - 100.0 m              |  |
| L Effective Length of Flare 1.0 - 100.0 m |  |
| D Inscribed Circle Diameter 15 - 100 m    |  |
| Ø Entry Angle 10° - 60°                   |  |
| S Sharpness of Flare 0.0 - 3.0            |  |

|        |                |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | x <sub>6</sub> | Μ     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 7.810          | 1.649 | 1.189          | 0.913 | 2367 | 0.640          | 1793  | 1789 | 1433       | 1388 | 0.799 | 0.776 |
| From B | 6.133          | 1.649 | 1.189          | 1.055 | 1858 | 0.556          | 937   | 930  | 491        | 654  | 0.524 | 0.703 |
| From C | 8.405          | 1.649 | 1.189          | 0.999 | 2547 | 0.669          | 1343  | 1361 | 490        | 475  | 0.365 | 0.349 |
| From D | 5.890          | 1.649 | 1.189          | 1.031 | 1785 | 0.544          | 1277  | 1193 | 313        | 370  | 0.245 | 0.310 |
| From E |                |       |                |       |      |                |       |      |            |      |       |       |
| From F |                |       |                |       |      |                |       |      |            |      |       |       |
| From G |                |       |                |       |      |                |       |      |            |      |       |       |
| From H |                |       |                |       |      |                |       |      |            |      |       |       |

| Junction: |      | Sha Tau Kok Road / Fanling Bypass Interchange |            |            |      |           |            |      | Job Number: J7204 |                |                  |
|-----------|------|---|------------|------------|------|-----------|------------|------|-------------------|----------------|------------------|
| Scenario: |      | Without Pr                                    | roposed De | velopment  |      | J7 - P. 1 |            |      |                   |                |                  |
| Design Ye | ar:  | 2034  | De         | signed By: | NCL  | C         | hecked By: | WCH  |                   | Date:          | 13 December 2022 |
| AM Peak   |      |   |            |            |      |           |            |      |                   |                |                  |
| Arm       | To A | To B  | To C       | To D       | To E | To F      | To G       | To H | Total             | q <sub>c</sub> | 1                |
| From A    |      |   | 937        | 132        |      |           |            |      | 1069              | 841            |                  |
| From B    | 659  |   |            | 55         |      |           |            |      | 714               | 1263           |                  |
| From C    | 807  | 647   | 93         | 4          |      |           |            |      | 1551              | 850            |                  |
| From D    | 174  |   | 97         | 4          |      |           |            |      | 275               | 2206           |                  |
| From E    |      |   |            |            |      |           |            |      |                   |                |                  |
| From F    |      |   |            |            |      |           |            |      |                   |                |                  |
| From G    |      |   |            |            |      |           |            |      |                   |                |                  |
| From H    |      |   |            |            |      |           |            |      |                   |                |                  |
| Total     | 1640 | 647   | 1127       | 194        |      |           |            |      | 3609              |                |                  |
|           |      |   |            |            |      |           |            |      |                   |                | -                |
| PM Peak   |      |   |            |            |      |           |            |      |                   |                | _                |
| Arm       | To A | To B  | To C       | To D       | To E | To F      | To G       | To H | Total             | q <sub>c</sub> |                  |
| From A    |      |   | 789        | 114        |      |           |            |      | 904               | 731            |                  |
| From B    | 850  |   |            | 60         |      |           |            |      | 910               | 1013           |                  |
| From C    | 622  | 622   | 68         | 2          |      |           |            |      | 1313              | 1027           |                  |
| From D    | 191  |   | 38         | 3          |      |           |            |      | 233               | 2160           |                  |
| From E    |      |   |            |            |      |           |            |      |                   |                |                  |
| From F    |      |   |            |            |      |           |            |      |                   |                |                  |
| From G    |      |   |            |            |      |           |            |      |                   |                |                  |
| From H    |      |   |            |            |      |           |            |      |                   |                |                  |
| Total     | 1663 | 622   | 896        | 180        |      |           |            |      | 3360              |                | 1                |

## Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| Α   | Sha Tau Kok Road - North  |
| В   | Fanling Bypass - East     |
| С   | Sha Tau Kok Road - South  |
| D   | Fanling Bypass - West     |
| Е   |                           |
| F   |                           |
| G   |                           |
| Н   |                           |

## Geometric Parameters

| A      | . ()  |       |       | 1 ()  | D ()  | <i>a</i> (0) | 0   |
|--------|-------|-------|-------|-------|-------|--------------|-----|
| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°)        | S   |
| From A | 9.0   | 7.0   | 25.0  | 18.0  | 75    | 40           | 0.2 |
| From B | 6.0   | 5.5   | 45.0  | 34.0  | 75    | 25           | 0.0 |
| From C | 9.5   | 9.0   | 35.0  | 10.0  | 75    | 30           | 0.1 |
| From D | 8.5   | 4.5   | 40.0  | 19.0  | 75    | 45           | 0.3 |
| From E |       |       |       |       |       |              |     |
| From F |       |       |       |       |       |              |     |
| From G |       |       |       |       |       |              |     |
| From H |       |       |       |       |       |              |     |

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity   |
|-----------------------|--|
| $q_{c}$               | Circulating Flow across the Entry                          |
| K<br>F                | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05]<br>= 303x <sub>2</sub> |
| $f_{c}$               | $= 0.210t_{D}(1+0.2x_{2})$                                 |
| t <sub>D</sub>        | = 1+0.5/(1+M)  |
| М                     | = exp[(D-60)/10]   |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)   |
| S                     | = 1.6(e-v)/L   |
|                       |  |

#### Limitation

| eEntry Width4.0 - 15.0 mvApproach Half Width2.0 - 7.3 mrEntry Radius6.0 - 100.0 mLEffective Length of Flare1.0 - 100.0 mDInscribed Circle Diameter15 - 100 m |   |                           |               |
|--|---|---------------------------|---------------|
| r Entry Radius 6.0 - 100.0 m<br>L Effective Length of Flare 1.0 - 100.0 m  | е | Entry Width               | 4.0 - 15.0 m  |
| L Effective Length of Flare 1.0 - 100.0 m  | v | Approach Half Width       | 2.0 - 7.3 m   |
| 5  | r | Entry Radius              | 6.0 - 100.0 m |
| D Inscribed Circle Diameter 15 - 100 m   | L | Effective Length of Flare | 1.0 - 100.0 m |
|  | D | Inscribed Circle Diameter | 15 - 100 m    |
| $\varnothing$ Entry Angle 10° - 60°  | Ø | Entry Angle               | 10° - 60°     |
| S Sharpness of Flare 0.0 - 3.0   | S | Sharpness of Flare        | 0.0 - 3.0     |

|        |                |       |                |       |      |                | $Q_E$ |      | Entry Flow | ,    | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | x <sub>3</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 8.475          | 4.482 | 1.091          | 0.975 | 2568 | 0.618          | 1998  | 2064 | 1069       | 904  | 0.535 | 0.438 |
| From B | 5.978          | 4.482 | 1.091          | 1.045 | 1811 | 0.503          | 1228  | 1360 | 714        | 910  | 0.581 | 0.669 |
| From C | 9.431          | 4.482 | 1.091          | 1.021 | 2858 | 0.661          | 2344  | 2224 | 1551       | 1313 | 0.662 | 0.590 |
| From D | 6.890          | 4.482 | 1.091          | 0.972 | 2088 | 0.545          | 861   | 885  | 275        | 233  | 0.319 | 0.263 |
| From E |                |       |                |       |      |                |       |      |            |      |       |       |
| From F |                |       |                |       |      |                |       |      |            |      |       |       |
| From G |                |       |                |       |      |                |       |      |            |      |       |       |
| From H |                |       |                |       |      |                |       |      |            |      |       |       |

| Junction: |      | Sha Tau k | Kok Road / | Job Number: J7204 |      |      |            |      |       |           |                 |  |  |
|-----------|------|-----------|------------|-------------------|------|------|------------|------|-------|-----------|-----------------|--|--|
| Scenario: |      | With Prop | osed Devel | opment            |      |      |            |      |       | J7 - P. 2 |                 |  |  |
| Design Ye | ar:  | 2034      | De         | signed By:        | NCL  | C    | hecked By: | WCH  | _     | Date:     | 13 December 202 |  |  |
| AM Peak   |      |           |            |                   |      |      |            |      |       |           |                 |  |  |
| Arm       | To A | To B      | To C       | To D              | To E | To F | To G       | To H | Total | qc        | 7               |  |  |
| From A    |      |           | 1003       | 132               |      |      |            |      | 1135  | 841       |                 |  |  |
| From B    | 759  |           |            | 55                |      |      |            |      | 814   | 1329      |                 |  |  |
| From C    | 850  | 647       | 93         | 4                 |      |      |            |      | 1594  | 950       |                 |  |  |
| From D    | 174  |           | 97         | 4                 |      |      |            |      | 275   | 2349      |                 |  |  |
| From E    |      |           |            |                   |      |      |            |      |       |           |                 |  |  |
| From F    |      |           |            |                   |      |      |            |      |       |           |                 |  |  |
| From G    |      |           |            |                   |      |      |            |      |       |           |                 |  |  |
| From H    |      |           |            |                   |      |      |            |      |       |           |                 |  |  |
| Total     | 1783 | 647       | 1193       | 194               |      |      |            |      | 3818  |           |                 |  |  |
|           |      |           |            |                   |      |      |            |      |       |           | -               |  |  |
| PM Peak   |      |           | <b></b>    | <del></del>       |      |      | <b></b>    |      |       | 1         | -               |  |  |
| Arm       | To A | To B      | To C       | To D              | To E | To F | To G       | To H | Total | qc        | _               |  |  |
| From A    |      |           | 817        | 114               |      |      |            |      | 932   | 731       |                 |  |  |
| From B    | 937  |           |            | 60                |      |      |            |      | 997   | 1041      |                 |  |  |
| From C    | 671  | 622       | 68         | 2                 |      |      |            |      | 1362  | 1114      |                 |  |  |
| From D    | 191  |           | 38         | 3                 |      |      |            |      | 233   | 2296      |                 |  |  |
| From E    |      |           |            |                   |      |      |            |      |       |           |                 |  |  |
| From F    |      |           |            |                   |      |      |            |      |       |           |                 |  |  |
| From G    |      |           |            |                   |      |      |            |      |       |           |                 |  |  |
| From H    |      |           |            |                   |      |      |            |      |       |           |                 |  |  |

#### Legend

Total

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| А   | Sha Tau Kok Road - North  |
| В   | Fanling Bypass - East     |
| С   | Sha Tau Kok Road - South  |
| D   | Fanling Bypass - West     |
| Е   |                           |
| F   |                           |
| G   |                           |
| н   |                           |

622

924

180

1799

## Geometric Parameters

| Arm    | e (m) | v (m) | r (m) | L (m) | D (m) | Ø(°) | S   |
|--------|-------|-------|-------|-------|-------|------|-----|
| From A | 9.0   | 7.0   | 25.0  | 18.0  | 75    | 40   | 0.2 |
| From B | 6.0   | 5.5   | 45.0  | 34.0  | 75    | 25   | 0.0 |
| From C | 9.5   | 9.0   | 35.0  | 10.0  | 75    | 30   | 0.1 |
| From D | 8.5   | 4.5   | 40.0  | 19.0  | 75    | 45   | 0.3 |
| From E |       |       |       |       |       |      |     |
| From F |       |       |       |       |       |      |     |
| From G |       |       |       |       |       |      |     |
| From H |       |       |       |       |       |      |     |

3524

#### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_E$                 | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_{c}$               | Circulating Flow across the Entry   |
| К                     | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| f <sub>c</sub>        | $= 0.210t_{D}(1+0.2x_{2})$          |
| t <sub>D</sub>        | = 1+0.5/(1+M)                       |
| М                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |
|                       |                                     |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |
|---|---------------------------|---------------|
| v | Approach Half Width       | 2.0 - 7.3 m   |
| r | Entry Radius              | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m    |
| Ø | Entry Angle               | 10° - 60°     |
| S | Sharpness of Flare        | 0.0 - 3.0     |

|        |                |       |                |       |      |                | $Q_E$ |      | Entry Flow |      | RFC   |       |
|--------|----------------|-------|----------------|-------|------|----------------|-------|------|------------|------|-------|-------|
| Arm    | x <sub>6</sub> | М     | t <sub>D</sub> | К     | F    | f <sub>c</sub> | AM    | PM   | AM         | PM   | AM    | PM    |
| From A | 8.475          | 4.482 | 1.091          | 0.975 | 2568 | 0.618          | 1998  | 2064 | 1135       | 932  | 0.568 | 0.451 |
| From B | 5.978          | 4.482 | 1.091          | 1.045 | 1811 | 0.503          | 1194  | 1345 | 814        | 997  | 0.682 | 0.741 |
| From C | 9.431          | 4.482 | 1.091          | 1.021 | 2858 | 0.661          | 2276  | 2165 | 1594       | 1362 | 0.700 | 0.629 |
| From D | 6.890          | 4.482 | 1.091          | 0.972 | 2088 | 0.545          | 785   | 813  | 275        | 233  | 0.350 | 0.287 |
| From E |                |       |                |       |      |                |       |      |            |      |       |       |
| From F |                |       |                |       |      |                |       |      |            |      |       |       |
| From G |                |       |                |       |      |                |       |      |            |      |       |       |
| From H |                |       |                |       |      |                |       |      |            |      |       |       |