

Drainage Impact Assessment for Proposed Residential Care Home for the Elderly (RCHE) Development at Tung Tsz, Tai Po

C241003W-02-A

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27 December 2024

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Contents

		Pages
1.	Background	3
2.	Objective	3
3.	Site Information	3
4.	Drainage Impact Assessment	5
5.	Conclusion	10



1. Background

The applicant, R Lee Architect, intends to develop one 10-storey building block situated at Tung Tyz, Tai Po, New Territories for the Proposed Residential Care Home for the Elderly (RCHE) Development.

The purpose of this report is to conduct a Drainage Impact Assessment (DIA) to assess the potential sewerage impact arising from the proposed development.

2. Objective

These DIA objectives are to assess the potential sewerage impact arising from the proposed development and recommend mitigation measures, if necessary, to alleviate the impacts.

3. Site Information

The D.D.23, Lot 232RP, 232 S.A. RP, 232 S.A.ss. 1 to 14, 232 S.B. RP, 232

Premise: S.B. ss 1 to 2, 232 S.C. to 232 S.E., 233 RP, 233 S.A to 233 S.M., 237

S.R. 238, 239 RP, 239 SG.

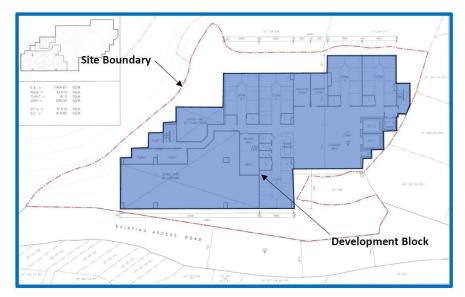
Address: Tung Tsz, Tai Po

Location Plan:





Development Plan:



Development Proposed Residential Care Home for the Elderly (RCHE) Development **Schedule:**

Site Area: 1,494.67m²

Class of Site: A

Proposed Plot Ratio for Non- 5.57 < 9.5

domestic:

Proposed Site Coverage above 61.09% < 80%

for Non-domestic (Above 15m):

Proposed Building Height: 34.50mPD

Absolute Height: 31.0m

Proposed No. of storey: 10 storeys

Proposed Gross Floor Area

LG/F (ENTRANCE & CARPARK) 606.13m²
UG/F (RCHE) 613.16 m²

1/F-5/F (RCHE) 916.89m² x 5 storeys (45 no. of beds

= 4584.45 m² x 5 storey)

6/F (RCHE) : 886.14 m² (17 no. of suites) 7/F (RCHE) : 759.44 m² (11 no. of suites)

8/F (MANAGEMENT OFFICE) : 764.44 m² R/F (SKY GARDEN) : 110.07 m²

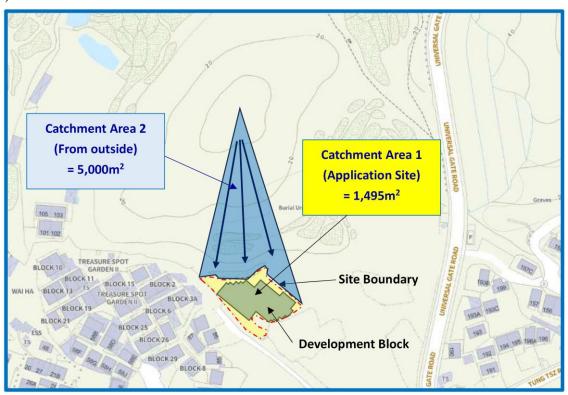
TOTAL : 8323.83 m² (89597 ft²)

(28 no. of suites & 225 no. of beds)



4. Drainage Impact Assessment

i) Catchment Areas



Catchment Area 1 (Application Site) = 1,495m² Catchment Area 2 (From the adjacent hillside) = 5,000m²

Drainage Impact Assessment for Proposed Residential Care Home for the Elderly (RCHE) Development at Tung Tyz, Tai Po



ii) Design Manuel

DSD - STORMWATER DRAINAGE MANUAL

iii) Design Method

a) Rational Method (DSD STORMWATER DRAINAGE MANUAL 7.5.2)

Qp = 0.278CiA

Where

 $Qp = peak runoff in m^3/s$

C = runoff coefficient (dimensionless)

i = rainfall intensity in mm/hr

 $A = \text{catchment area in km}^2$

b) Runoff Coefficient

In Hong Kong, a value of C = 1.0 is commonly used in developed urban areas. In less developed areas, appropriate C values in order to ensure that the design would be fully cost-effective.

Surface Characteristics	Runoff coefficient, C*
Asphalt	0.70-0.95
Concrete	0.80-0.95
Brick	0.70-0.85
Grassland (heavy soil**)	
Flat	0.13-0.25
Steep	0.25-0.35
Grassland (sandy soil)	
Flat	0.05-0.15
Steep	0.15-0.20

The surface of the site will be covered by Asphalt, the C1 should be 0.85 (Mid value) and the surface of the adjacent hill side is Grassland (heavy soil, the C2 should be 0.15.

Drainage Impact Assessment for Proposed Residential Care Home for the Elderly (RCHE) Development at Tung Tyz, Tai Po



c) 6.6.1 Village Drainage and Main Rural Catchment Drainage Channels

'Village Drainage' refers to the local stormwater drainage system within a village. A stormwater drain conveying stormwater runoff from an upstream catchment but happens to pass through a village may need to be considered as either a 'Main Rural Catchment Drainage Channel' or 'Village Drainage', depending on the nature and size of the upstream catchment. In any case, the impact of a 50-year event should be assessed in the planning and design of village drainage system to check whether a higher standard than 10 years is justified. (50 Years is used.)

d) Rainfall Intensity

Table 2d – Intensity-Duration-Frequency (IDF) Relationship of North District Area for durations not exceeding 240 minutes

Duration (min)		Extre	me Intensity x	(mm/h) for val	rious Return P	eriods	
	2	5	10	20	50	100	200
240	28.5	37.7	43.4	48.6	54.9	59.4	63.6
120	42.2	54.7	62.5	69.6	78.4	84.7	90.8
60	61.0	75.7	84.3	92.0	101	108	114
30	84.0	100	110	118	128	135	142
15	106	127	139	150	163	173	182
10	119	141	155	168	184	196	208
5	138	161	177	193	216	234	254

i (rainfall intensity) = 101mm/hr (Duration of 60min is used)



e) Calculations of Water Flow

Qp = 0.278CiA

C1 = 0.85 (Asphalt)(mid value) (Application Site)

C2 = 0.15 (Grass Land (Sandy Soil) (Adjacent Area)

i = 101 mm/hr

 $A1 = 1,495m^2 (0.001495km^2)$ (Application Site)

 $A2 = 1,200 \text{m}^2 (0.001200 \text{km}^2)$ (Adjacent Hill Side)

 $Qp = 0.278 \times 101 \times ((0.85 \times 0.001495) + (0.15 \times 0.005000))$

 $Qp = 0.0567 \text{ m}^3/\text{s} \text{ or } 3,404 \text{ l/min}$

For conservative calculations, all catchment areas are combined for all U-Channels.

f) Design of U-channel

GEO Technical Guidance Note No. 43 (TGN 43) Guidelines on Hydraulic

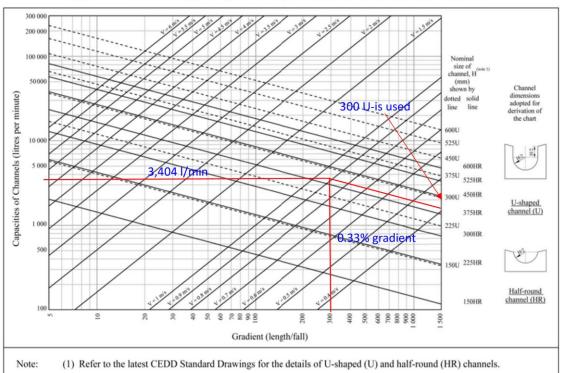
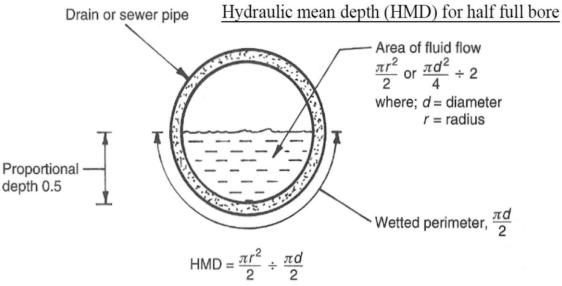


Figure 1 - Chart for the rapid design of U-shaped and half-round channels up to 600 mm

For 3,404 l/min, 300 U-channel is used



f) Design of Pipe



Depth of flow	HMD
0.25	Pipe dia. (m) / 6.67
0.33	Pipe dia. (m) / 5.26
0.50	Pipe dia. (m) / 4.00
0.66	Pipe dia. (m) / 3.45
0.75	Pipe dia. (m) / 3.33
Full	Pipe dia. (m) / 4.00

The 0.5 full bore, velocity of 1.5m/s and 375mm pipe is used.

The capacity of the pipe:

$$Q = V \times A = 1.5 \times \pi \times (0.375)2/4 \times 0.5 = 0.0828 \text{m}^3/\text{s} > 0.0567 \text{m}^3/\text{s}, \text{ OK}$$

Chezy"s formula:

where

V = velocity of flow = 1.5 m/s

m = hydraulic mean depth (HMD) \rightarrow HMD = 0.375 / 4.00 = 0.09375

C = Chezy coefficient = (0.09375)1/6/(0.015(concrete pipe))= 44.94

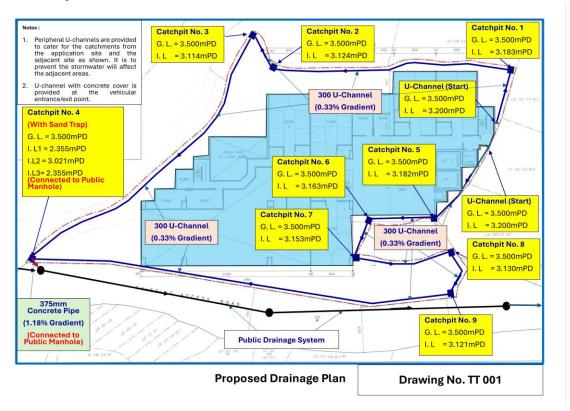
1.5 = 44.94 x (0.09375 x i)0.5

(1.5/44.94)2 = 0.09375 x i

Thus i = 0.01188 or 1.18% (i = inclination or gradient as <math>1/X)



iv) Drainage Plan





5. Conclusion

Since there is no change of total catchment areas and the total Stormwater flow (0.057m³/s) from this developing area is considered small in quantity and therefore the impact is negligible.



Sewerage Impact Assessment for Proposed Residential Care Home for the Elderly (RCHE) Development at Tung Tsz, Tai Po

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3.	Site Information	3
4.	Sewage Impact Assessment	5
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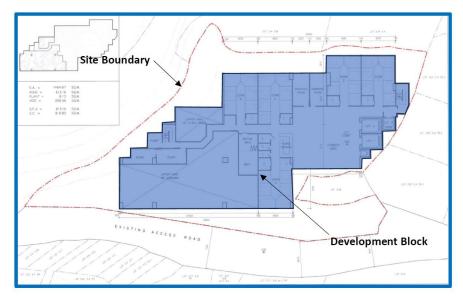
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8/F (MANAGEMENT OFFICE) : 764.44 m² R/F (SKY GARDEN) : 110.07 m²

TOTAL : 8323.83 m² (89597 ft²)

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4. Sewage Impact Assessment

- i) No. of Residents/Employees
- a) No. of Residents = 253 beds
- b) No. of Employees = 120 Nos. (About 2 times as recommended by Code of Practice for Resident Care Home)

ii) Estimated Sewage Flows:

EPD Technical Paper Report No. EPD/TP1/05 – Table T-2 (Unit Flow Rate Factor of Commercial Flows and Student Flows)

8. UNIT FLOW FACTORS – COMMERCIAL AND INSTITUTIONAL FLOWS

8.1 Commercial flows comprise flows due to commercial activities and due to employees. Flows from Job types J2 – J12 are classified as commercial flows. The unit flow factors of the 11 Job types are provided in Table T-2 below. The derivation of the UFFs of employees and students were presented in Appendix III.

Table T-2: Unit Flow Factors of Commercial Flows and Student Flows

		Unit (per)	Datum (2002) (m³/day)	Increase per Annum (m³/day)	Planning for Future (m³/day)
Commer	cial Employee	employee	0.080	-	0.080
Commer	cial activities				
(a) Spec	cific trades:				
J2	Electricity Gas & Water	employee	0.250	-	0.250
Ј3	Transport, Storage & Communication	employee	0.100	-	0.100
J4	Wholesale & Retail	employee	0.200	-	0.200
J5	Import & Export	employee	-		-
J6	Finance, Insurance, Real Estate & Business Services	employee	2	-	-
J7	Agriculture & Fishing	employee	-	-	-
J8	Mining & Quarrying	employee	-	-	-
J9	Construction	employee	0.150	-	0.150
110	Restaurants & Hotels	employee	1.500	_	1.500
J11	Community, Social & Personal Services	employee	0.200	-	0.200
J12	Public Administration	employee	-	-	-
(b) Gen	eral -territorial average	employee	0.200	<u>-</u>	0.200
School st	tudent	person	0.040	-	0.040

Notes of Table T-2:

- (1) For planning of a new sewerage system, the planning unit flow factors should be used and the worst possible combination of commercial flows for the future development scenarios should be considered to ensure that the sewerage system under planning will be sustainable.
- (2) For job types J10 and J11, the "per-employee" unit flow factor takes into account the flows of customers and/or tenants.
- (3) The total unit flow generated from an employee in a particular trade is the sum of the unit flow factor of employee and the unit flow factor of commercial activities of a particular trade under consideration.

EPD/TP 1/05 Guidelines for Estimating Sewage Flows for Sewage Infrastructure Planning

Page 9 of 14

Sewerage Impact Assessment for Proposed Residential Care Home for the Elderly (RCHE) Development at Tung Tyz, Tai Po



Site	Use	Global Unit	No. of	ADWF
		Flow Factor	Residents/Employees	(m3/day)
		(m3/person/day)		
Tung	RCHE	0.200	253 residents + 120	74.6
Tyz, Tai	J11		staff = 373	
Po	(Community,			
	Social &			
	Personal			
	Service)			

iii) Sewer Pipe Design:

For sewer pipe, one quarter (1/4) full bore is used to allow space for a core of air in centre of the stack and the air keeps fluctuations to a minimum.

Minimum velocity of 0.7m/s (smaller than 300mm diameter) is used for maintaining self-cleansing purpose.

To facilitate inspection and cleaning, pipe should not be less than 200mm diameter.

Design Flow = 74.6m³/day or 0.000863m³/s

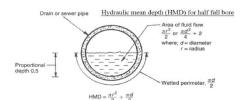
1/4 full bore, velocity of 0.7m/s and 225mm pipe is used.

The capacity of the pipe:

 $Q = V \times A = 0.7 \times \pi \times (0.225)^2 / 4 \times 0.25 = 0.00695 \text{m}^3 / \text{s} \ 0.000863 \text{m}^3 / \text{s}, \mathbf{OK}$

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Depth of flow	HMD
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0.50	Pipe dia. (m) / 4.00
0.66	Pipe dia. (m) / 3.45
0.75	Pipe dia. (m) / 3.33
Full	Pipe dia. (m) / 4.00

Chezy"s formula: $V = C\sqrt{m \times i}$

where V = velocity of flow = 0.7 m/s

m = hydraulic mean depth (HMD) \rightarrow HMD = 0.225 / 6.67 = 0.0337

C = Chezy coefficient = $(0.0337)^{1/6}/(0.015)$ (concrete pipe) = 37.89

 $0.7 = 37.89 \text{ x } (0.0337 \text{ x i})^{0.5}$

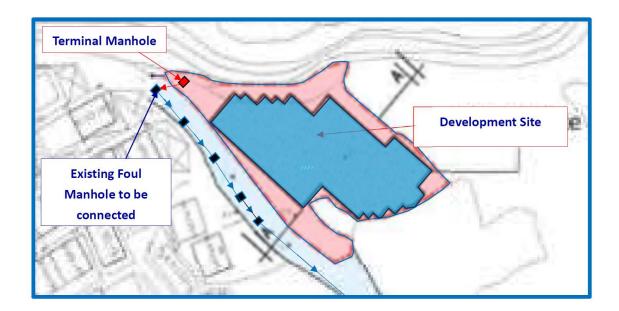
 $(0.7/37.89)^2 = 0.0337 \text{ x i}$

Thus i = 0.0101 or 1.01% (i = inclination)



iv) Connection to Public Foul System:

The foul water from the developing site will be discharged into the nearby existing Foul Manhole (as shown below).





5. Conclusion:

The total foul water flow (0.000863m3/s) from this developing area is considered small in quantity and therefore the impact is negligible.